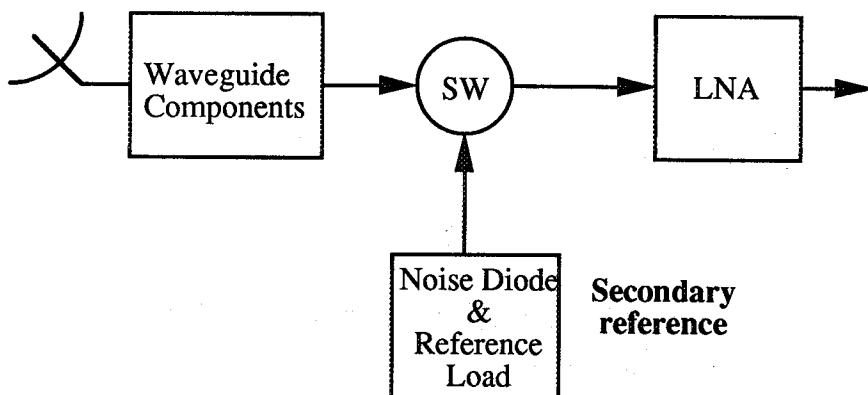


**Radiometer Calibration Procedure  
and  
Beacon Attenuation Estimation  
Reference Level**

by  
**Robert K. Crane**  
**University of Oklahoma**

## RADIOMETER SYSTEM



- **VSWR through switch is high (~ 2:1)**
- **Match secondary reference to LNA not the same as match antenna to LNA**
- **Hot/Cold load measurements not necessary match probably different from other loads**
- **No absolute calibration possible using loads and secondary reference**

## **RADIOMETER CALIBRATION**

### **PRIMARY:**

- Compare Radiometer Attenuation with Beacon Attenuation
- Compare Sky Temperature Estimates with Calculations Using Simultaneous Meteorological Data

### **SECONDARY:**

- Noise Diode and Reference Load Measurements
- Adjust for Outside Temperature and Component Temperature Changes

## **RADIOMETER CALIBRATION MODEL**

$$\mathbf{T_r} = \mathbf{A} + \mathbf{B} \mathbf{V}$$

$$\mathbf{T_s} = \mathbf{C} \mathbf{T_r} + \mathbf{D} \mathbf{T_o} + \mathbf{E}$$

$$\mathbf{A_r} = -4.343 \ln ((\mathbf{T_m} - \mathbf{T_s}) / (\mathbf{T_m} - \mathbf{T_b}))$$

**A, B from noise diode, reference load measurements**

**C from beacon attenuation vs radiometer attenuation measurements**

**D, E from radiometer estimates of sky temperature vs calculated sky temperature**

**T<sub>m</sub> from calculations**

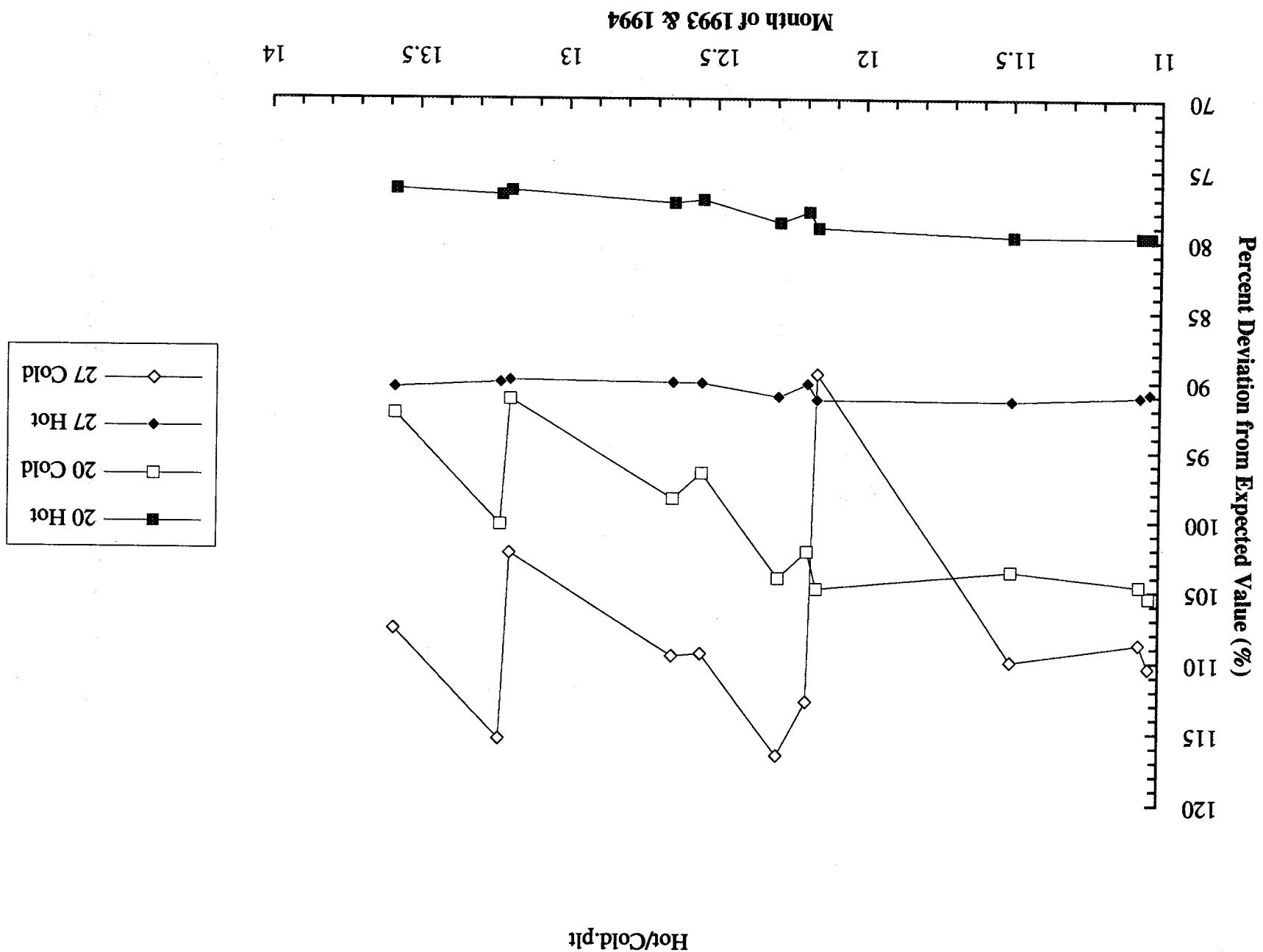
**T<sub>b</sub> from theory**

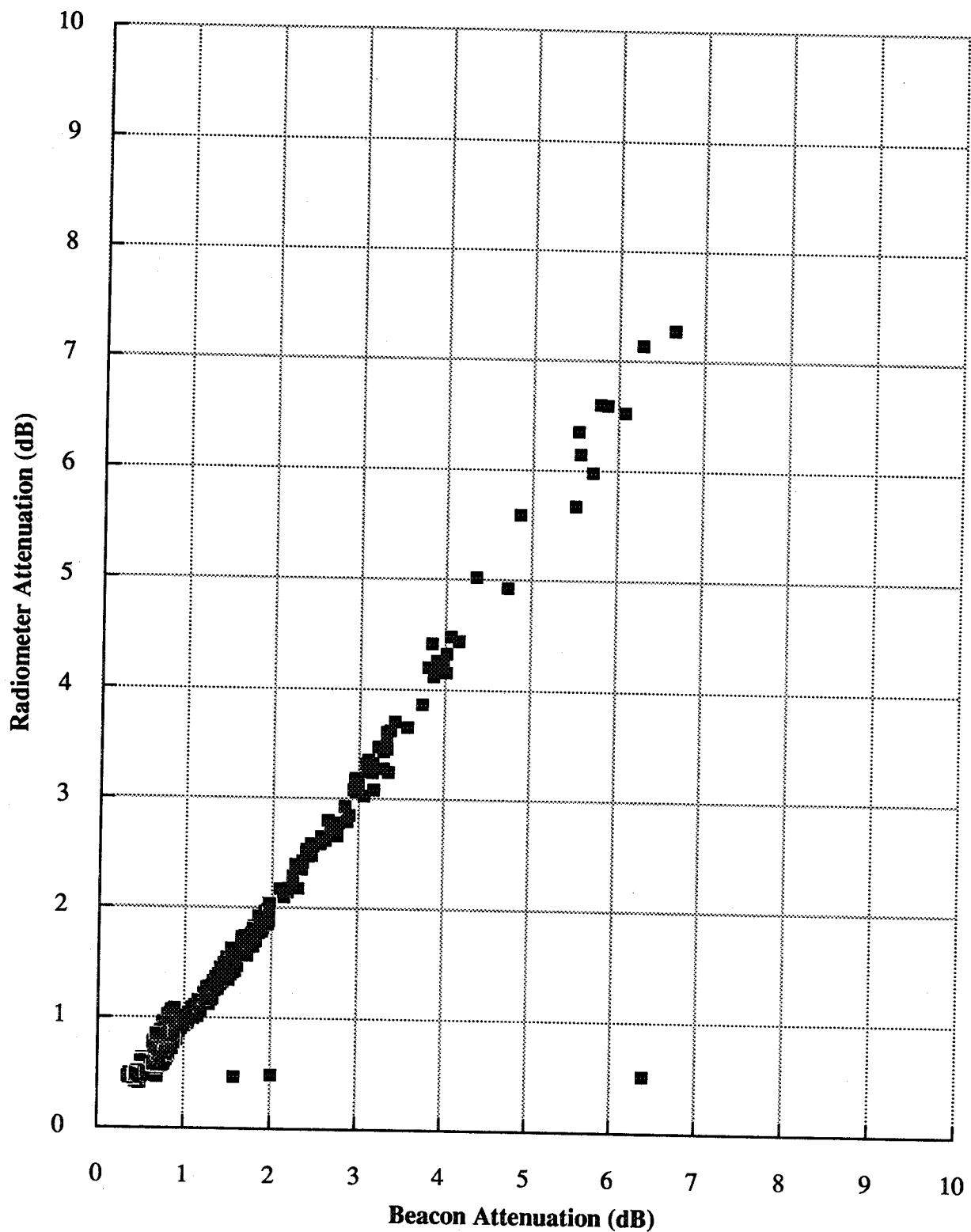
## **SYSTEM CALIBRATION IS ITERATIVE**

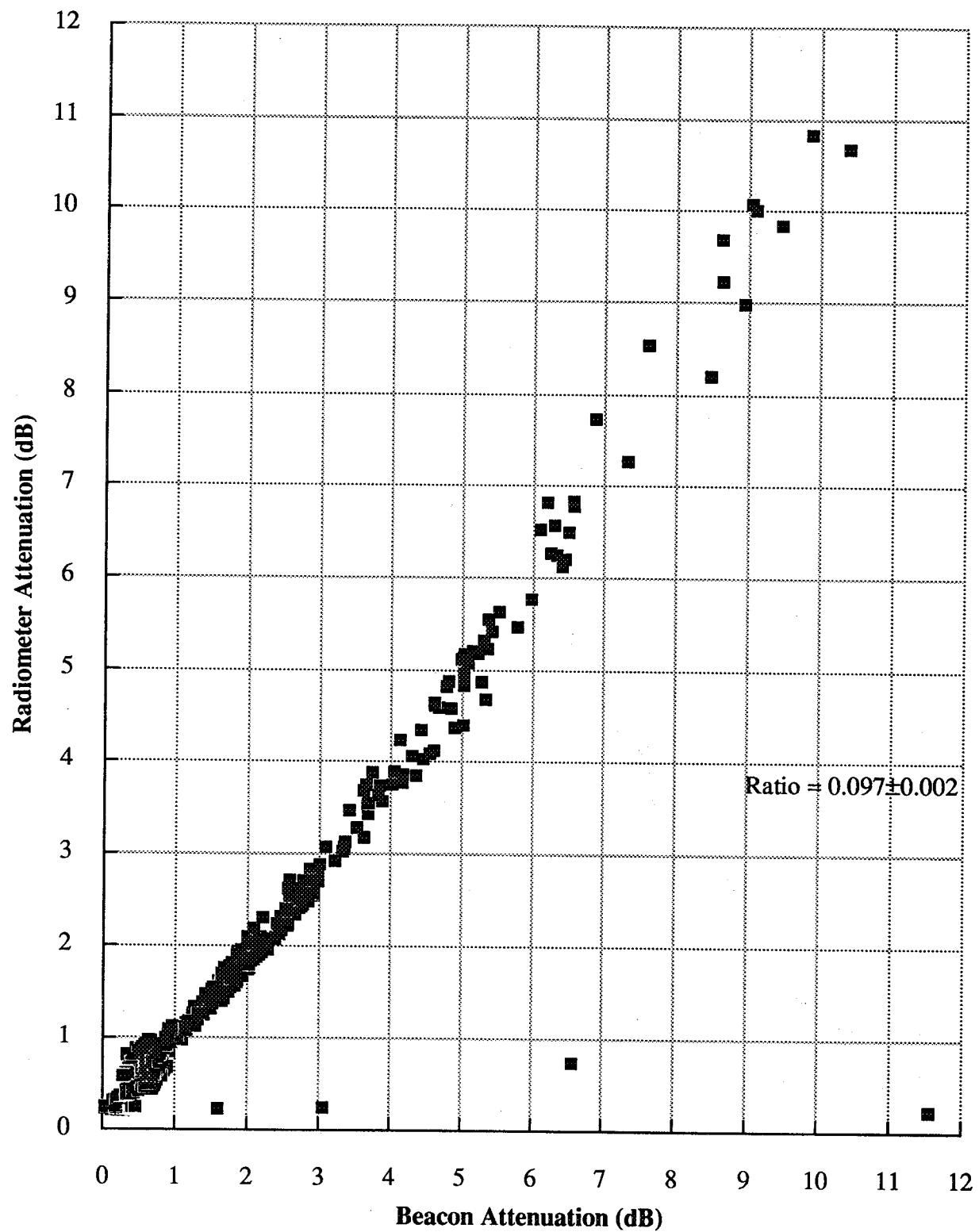
- **Need beacon attenuation to compare to radiometer**
- **Need radiometer attenuation to set beacon reference level**

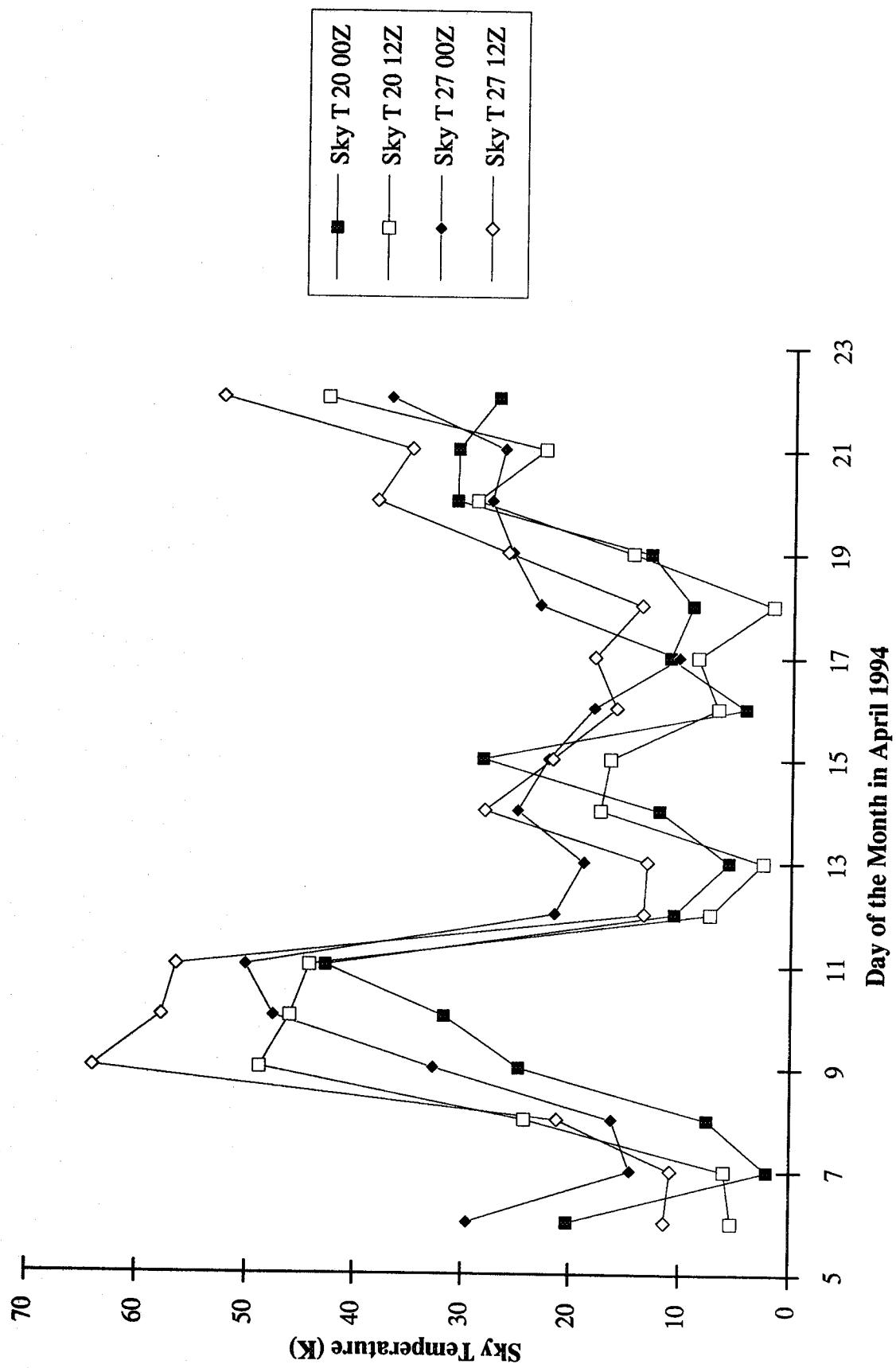
### **Assumptions**

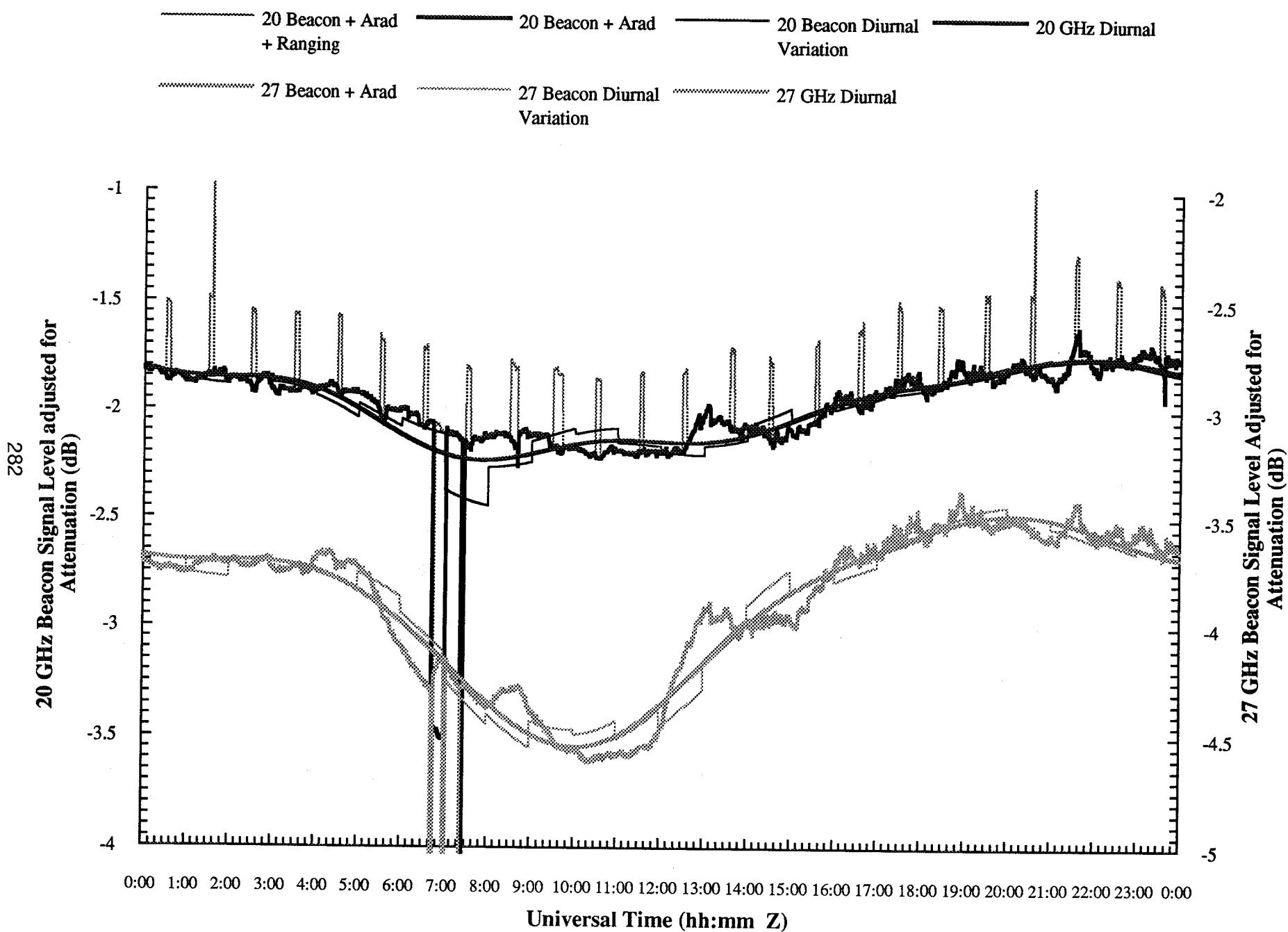
- **Beacon receiver is linear, need only find reference level to estimate beacon attenuation**
- **Radiometer receiver temperature is a linear function of radiometer output voltage, need only estimate gain and offset**
- **Sky temperature is a linear function of radiometer receiver temperature, need only estimate efficiency and background temperature**
- **Radiometer attenuation may be estimated from sky temperature if the medium temperature is known**











Atten 20 GHz  
Beacon

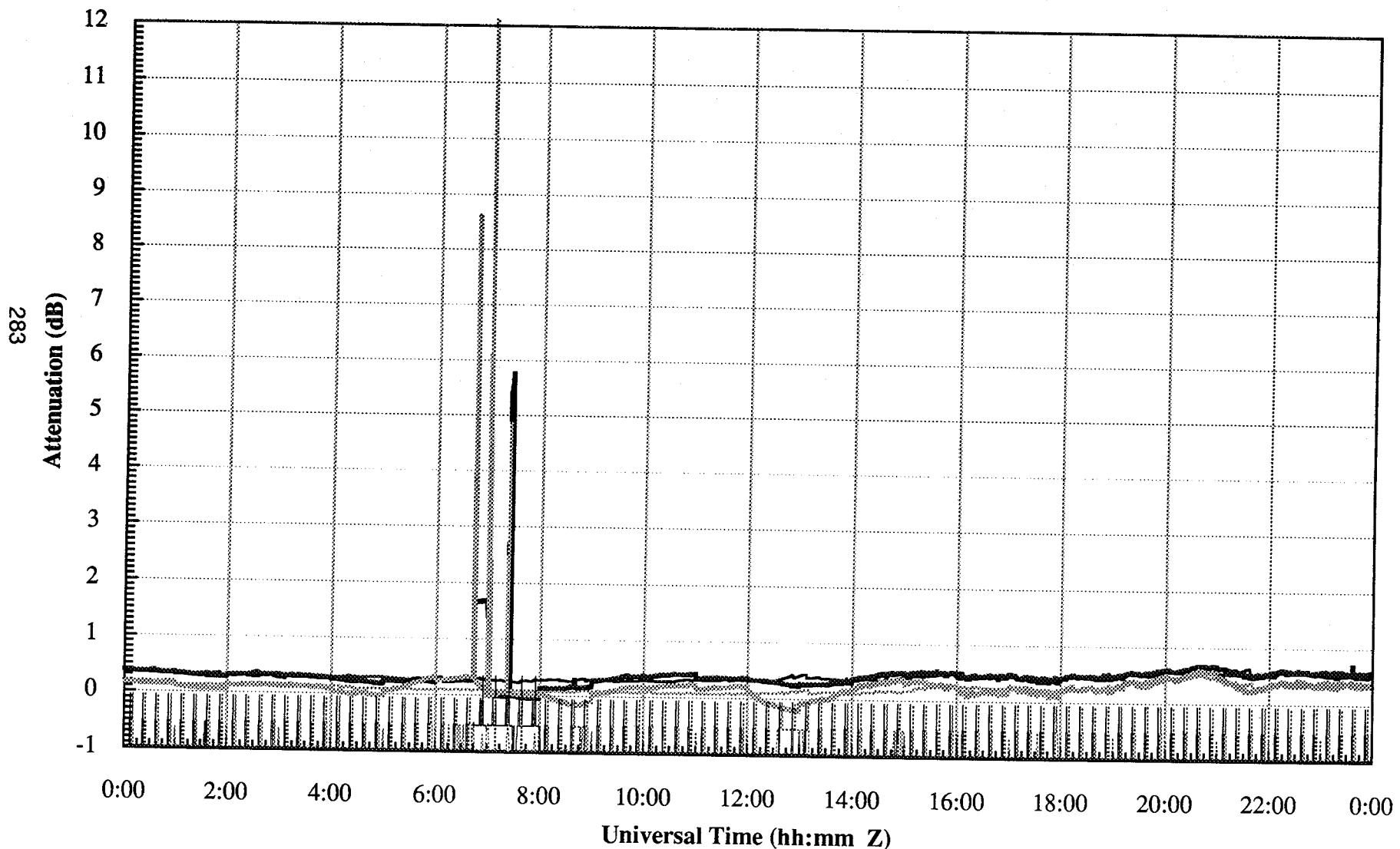
Atten 20 GHz  
Radiometer

Atten 27 GHz  
Beacon

Atten 27 GHz  
Radiometer

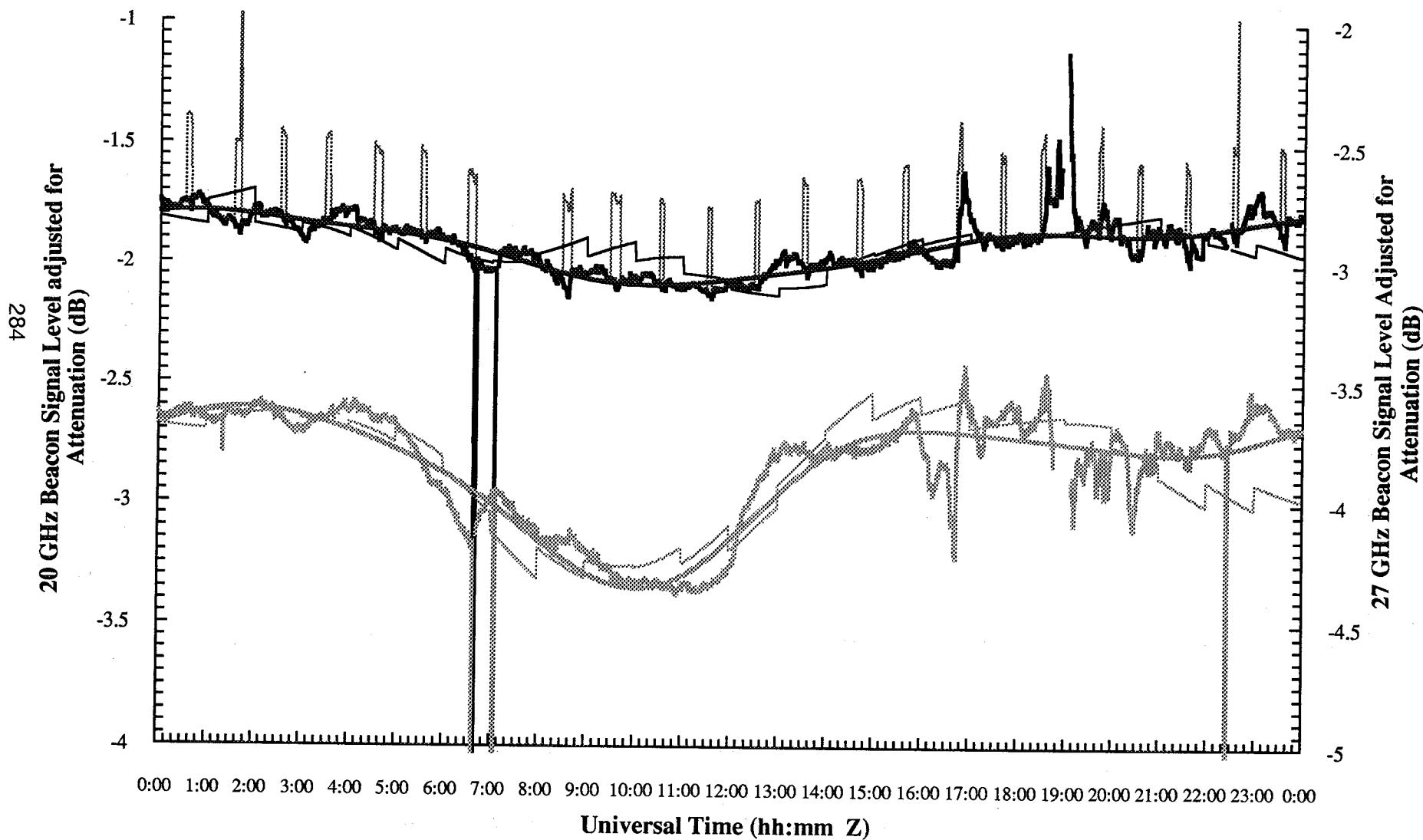
20 Beacon Flag

27 Beacon Flag

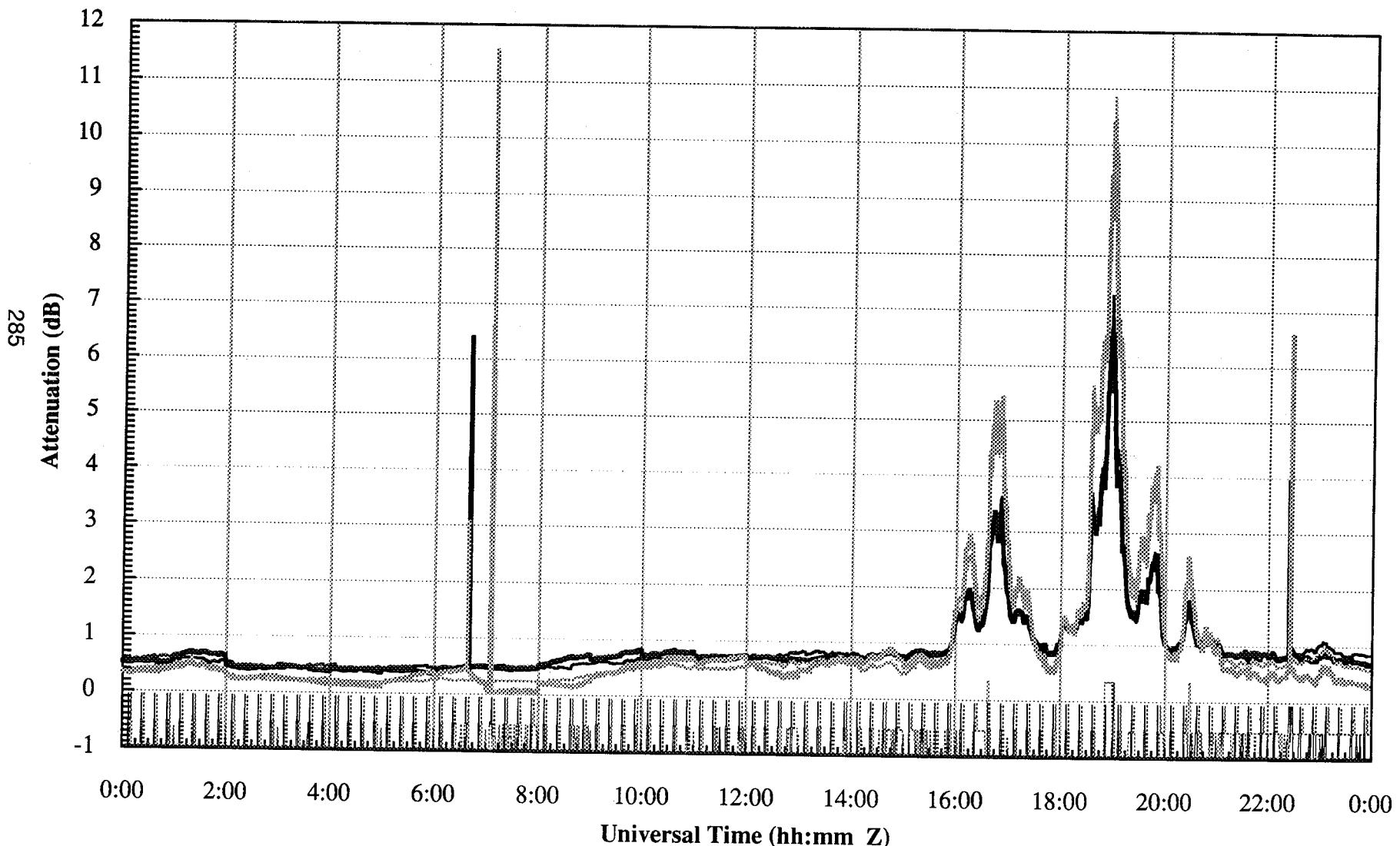


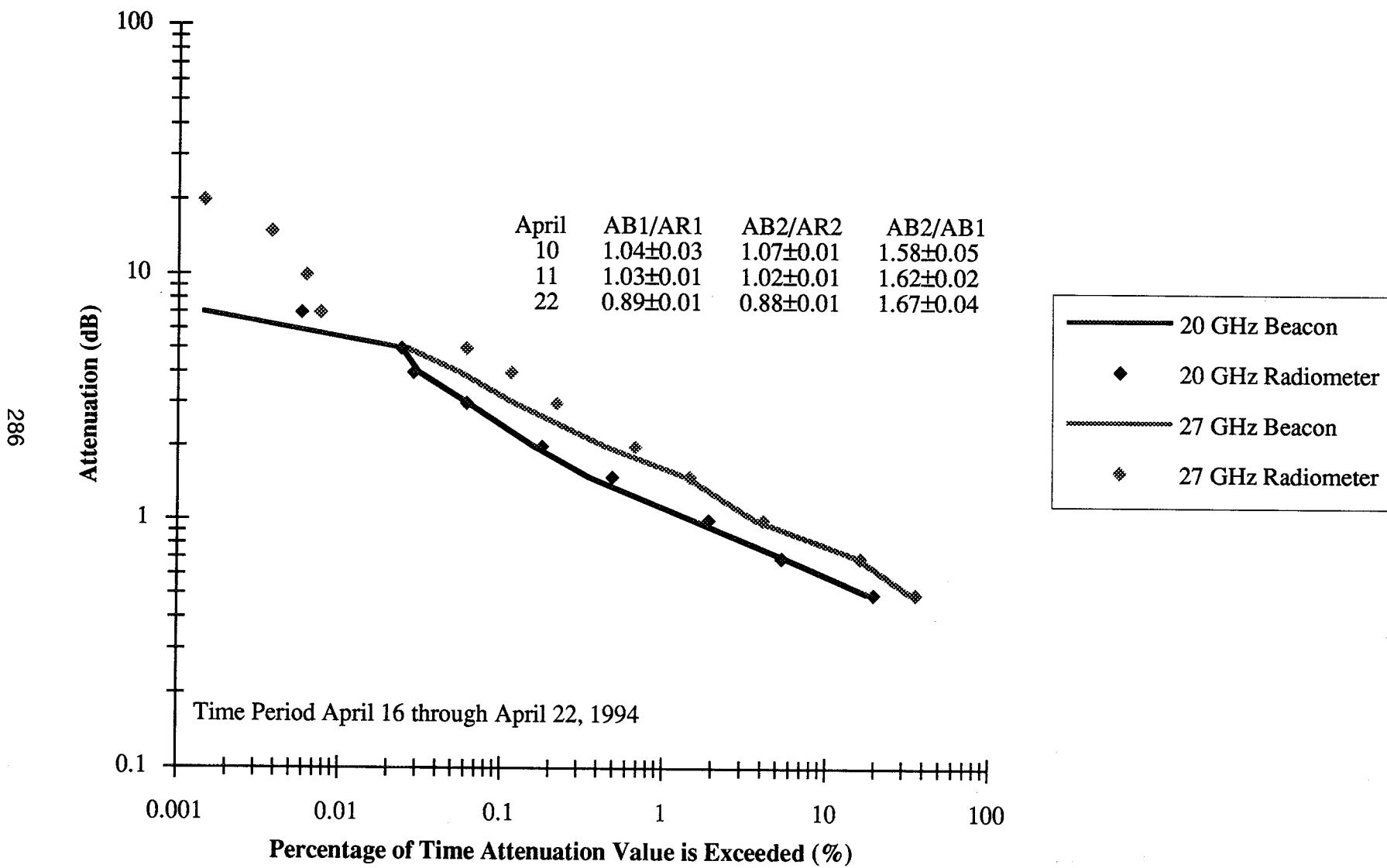
20 Beacon + Arad  
+ Ranging      20 Beacon + Arad  
+ Ranging      20 Beacon Diurnal  
Variation      20 GHz Diurnal  
Variation

27 Beacon + Arad      27 Beacon Diurnal  
Variation      27 GHz Diurnal  
Variation



Atten 20 GHz  
Beacon      Atten 20 GHz  
Radiometer      Atten 27 GHz  
Beacon  
Atten 27 GHz  
Radiometer      20 Beacon Flag      27 Beacon Flag





EERL / Univ. of Texas

# DATA CENTER STATUS REPORT

BY  
WOLFHARD J VOGEL  
&  
ALI SYED

EERL/UTAU  
10100 BURNET RD  
AUSTIN, TX 78758-4497  
PRESENTED AT APSW-VI  
VANCOUVER, BC  
JUNE 16, 1994

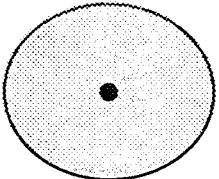
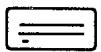
# ACTS DC Services

- Archive Raw and Pre-processed Data from Stations
- Archive Event & Fault Logs from Stations
- Audit Pre-processed Data
- Distribute Monthly Audit Reports to Stations
- Distribute Archived Data to Propagation Community

Raw Data Status														
S	9	9	9	9	9	9	9	9	9	9	9	9	9	9
T	3	4	4	4	4	4	4	4	4	4	4	4	4	4
A	1	0	0	0	0	0	0	0	0	0	0	0	0	0
T	2	1	2	3	4	5	6	7	8	9	0	0	0	0
A	1	1	1	0	0	0	0	0	0	0	0	0	0	0
S	9	9	9	9	9	9	9	9	9	9	9	9	9	9
C	31	31	28	31	30	..	..	..	..	..	..	..	..	..
C	30	31	28	31	XX	..	..	..	..	..	..	..	..	..
F	29	31	28	29	30	..	..	..	..	..	..	..	..	..
M	XX	XX	XX	XX	17	30	..	..	..	..	..	..	..	..
N	M	29	31	25	18	30	..	..	..	..	..	..	..	..
O	K	31	31	28	31	XX	..	..	..	..	..	..	..	..
The file contains 15 columns of data.														

## Pre-processed Data Status

# Data Archival Status



FIRST RAW DATA CD-ROM WRITTEN ON 5/27/94

291



COMPRESSION RATIO OF ~2.0

1105 MB IN  
838 RAW DATA  
FILES

543 MB  
ON CD-ROM



COMPRESSION RATIO OF ~3.5

751 MB IN  
570 PP DATA  
FILES

213 MB  
ON HARD DISK

# Audit & Analysis Status

(:() INCORRECT DATA STRUCTURE CAUSED ERROR  
IN AUDIT & ANALYSIS. BUG FIXED.

<input checked="" type="checkbox"/>	Time Stamp	Beacon at 20 GHz	Radiometer at 20 GHz	Beacon at 27 GHz	Radiometer at 27 GHz	Status 1	Status 2
-------------------------------------	------------	------------------	----------------------	------------------	----------------------	----------	----------

<input checked="" type="checkbox"/>	Time Stamp	Beacon at 20 GHz	Beacon at 27 GHz	Radiometer at 20 GHz	Radiometer at 27 GHz	Status 1	Status 2
-------------------------------------	------------	------------------	------------------	----------------------	----------------------	----------	----------

(:() INCORRECT SCALING FOR STATUS QUANTITIES  
CAUSED ERROR IN AUDIT REPORT. BUG FIXED.

<u>QUANTITY</u>	<u>CORRECT SCALE</u>	<u>RANGE</u>
RainGauge [Volts]	1000	0 to 500 mm/Hr
AirTemp. [C]	100	-50 to 70 C
Rel.Humd [%]	100	0 to 100 %

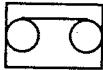
# DC System Status

- CD WRITER OK
- 120 MB TAPE DRIVE OK
- HARD DRIVE SCSI CARD FAILURE IN 3/94 RESULTED  
IN ~2 WEEKS DOWNTIME
  - ☞ SYSTEM & DATA RESTORED FROM TAPES
  - ☞ DAILY BACKUP SCHEDULE ADOPTED

# Data Tapes Status



44 DATA TAPES RECEIVED FROM STATIONS



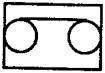
DIFFERENT BACKUP PATHS NOT A PROBLEM



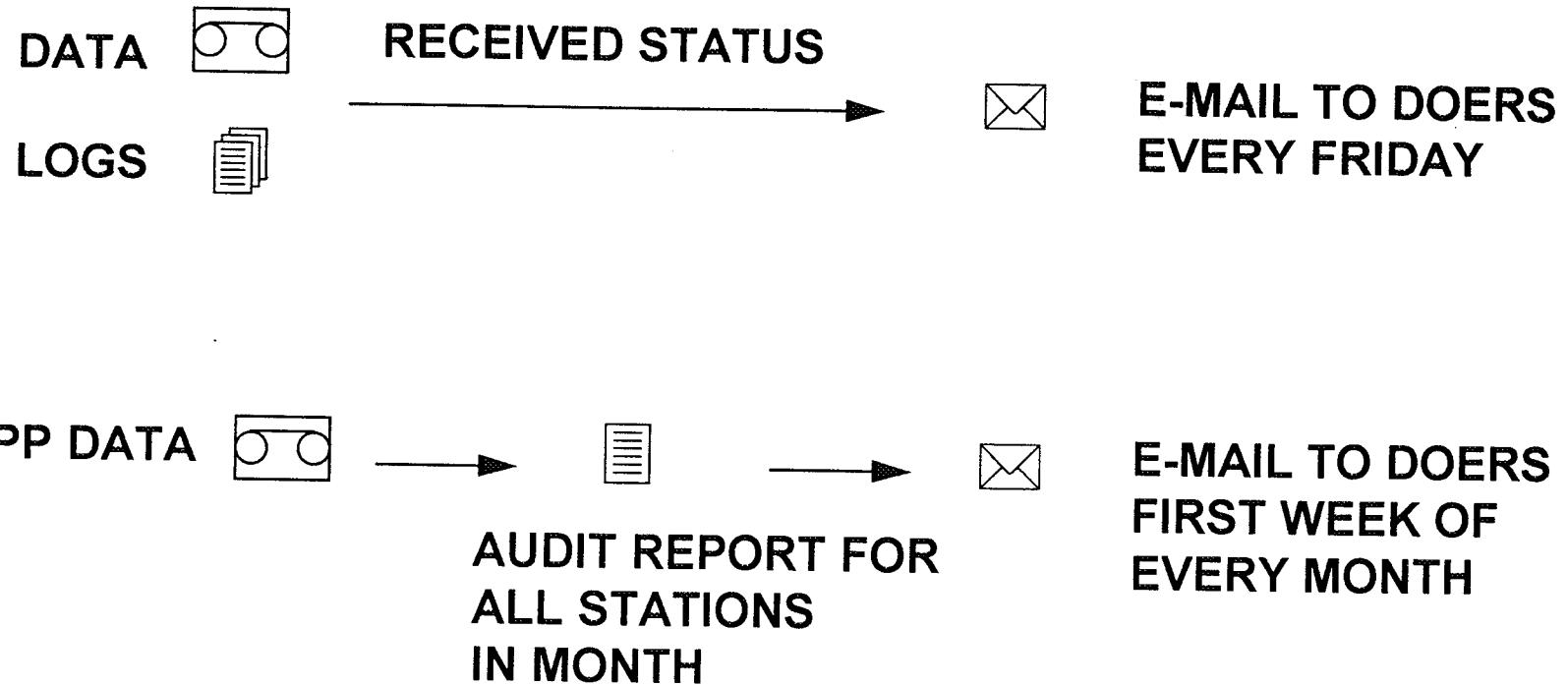
COLORADO BACKUP LITE VER 1.20 USED  
BY DATA CENTER



DATA TAPES WILL BE RECYCLED



# Feedback Schedule



# CONCLUSION

- DATA COMPRESSION AND ARCHIVAL HAS WORKED WITH REAL DATA
- BUGS FOUND IN AUDIT & ANALYSIS ROUTINES HAVE BEEN FIXED
- WEEKLY DATA RECEIVED STATUS REPORT WILL BE DISTRIBUTED VIA E-MAIL
- MONTHLY AUDIT REPORT FOR STATIONS WILL BE DISTRIBUTED VIA E-MAIL
- SOME FINE TUNING IS EXPECTED IN THE FOLLOWING MONTHS

# **ALASKA ACTS PROPAGATION TERMINAL: DATA ANALYSIS PROCEDURE, SYSTEM STATUS AND RESULTS**

**ACTS PROPAGATION MINIWORKSHOP  
AND NAPEX-XVIII  
VANCOUVER, BC  
JUNE 16, 1994**

**BRAD JAEGER  
CHARLIE MAYER  
UNIVERSITY OF ALASKA FAIRBANKS**

**Alaska ACTS Propagation**

## **OUTLINE**

- I. DATA ANALYSIS PROCEDURE AND RESULTS**
  - JAEGER**
- II. SYSTEM STATUS AND RESULTS**
  - MAYER**
- III. FUTURE PLANS**
  - MAYER**

**Alaska ACTS Propagation**

## **I. DATA ANALYSIS PROCEDURE**

- A. COUNT EVENTS**
- B. ANALYZE INDIVIDUAL EVENTS**
- C. ANALYZE CUMULATIVE STATISTICS**
- D. FORMULATE MODELS OF VARIOUS PARAMETERS**

Alaska ACTS Propagation

### **A. COUNT EVENTS**

- RAIN EVENTS**
- SNOW EVENTS**
- SCINTILLATION EVENTS**

**CATEGORIZE THESE EVENTS IN TERMS OF  
MAXIMUM FADE, FADE SLOPE, FADE  
DURATION, ETC.**

Alaska ACTS Propagation

## **B. ANALYZE INDIVIDUAL EVENTS**

- TIME SERIES ANALYSIS
- POWER SPECTRAL DENSITY ANALYSIS
- SCINTILLATION INTENSITY
- FADE SLOPE

Alaska ACTS Propagation

## **C. ANALYZE CUMULATIVE STATISTICS**

- BIN THE VARIABLES
- RUNNING AVERAGE TO REMOVE SCINTILLATIONS
- CUMULATIVE BINS
  - DAY
  - MONTH
  - YEAR
  - EXPERIMENT LENGTH

Alaska ACTS Propagation

## C. ANALYZE CUMULATIVE STATISTICS

- STATISTICAL ANALYSIS
  - CDFs
  - TIME PERCENTAGES VALUES EXCEEDED
  - WORST MONTH
    - » WORST MONTH TO ANNUAL AVERAGE
    - » WORST MONTH TO OTHER MONTHS
  - FREQUENCY SCALING
    - » ATTENUATION RATIOS
    - » SCINTILLATION RATIOS
  - SCINTILLATION DIURNAL AND ANNUAL VARIABILITY PLOTS
  - RAIN RATE ANALYSES
    - » DIURNAL VARIABILITY
    - » ANNUAL VARIABILITY

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## D. FORMULATE MODELS OF VARIOUS PARAMETERS

- ATTENUATION RATIO VS. FREQUENCY
- SCINTILLATION RATIO VS. FREQUENCY
- SCINTILLATION INTENSITY VS. ELEVATION ANGLE
- ULTIMATE FADE DEPTH
- FADE DURATION
- TIME BETWEEN FADES

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## BINNING PROCEDURE

Variable	Small Bin	Large Bin	Increment
Rain Rate	0 mm/hr	>200 mm/hr	2 mm/hr, R<30 mm/hr
			5 mm/hr, R>30 mm/hr
Beacon Attenuation	-8 dB	30 dB	1 dB or 0.2 dB
Attenuation Ratio	0	15	0.05
Radiometric Attn.	0 dB	15 dB	1 dB or 0.2 dB
Fade Slope	-1.25 dB/s	1.25 dB/s	0.05 dB/s
Ultimate Fade Depth	1 dB	30 dB	1 dB or 0.2 dB
Fade Duration	0-1 s; 1-2, 2-3, 3-5, 5-10, 10-20, 20-30, 30-60 s & min., >60 min.		for fade levels of -8 to 30 dB in 1 dB increments
Time Between Fades	as above		as above
Sky Temperature	0 K	>300 K	2 K
Scintillation Intensity	0	4	0.05

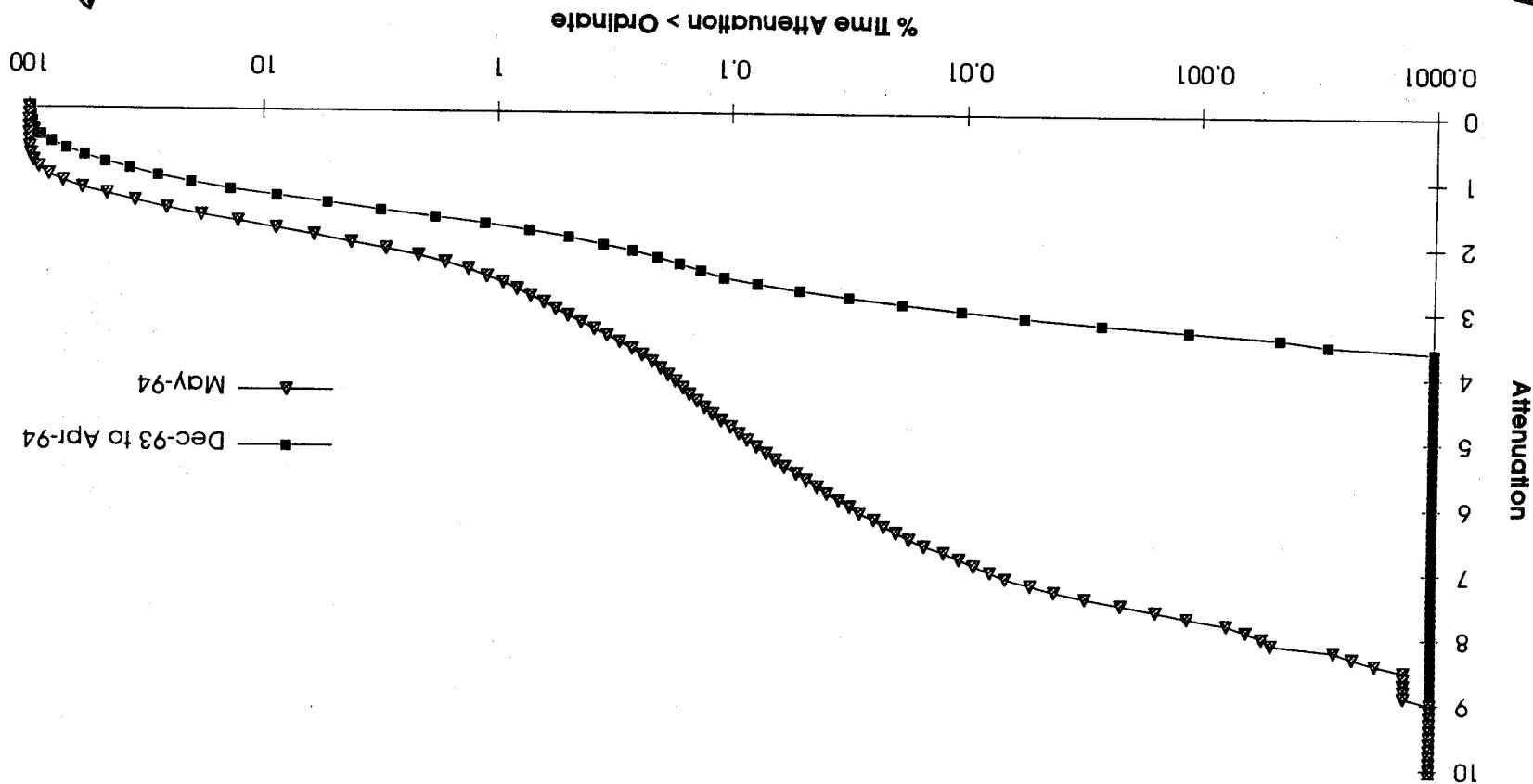
Alaska ACTS Propagation

## II. SYSTEM STATUS

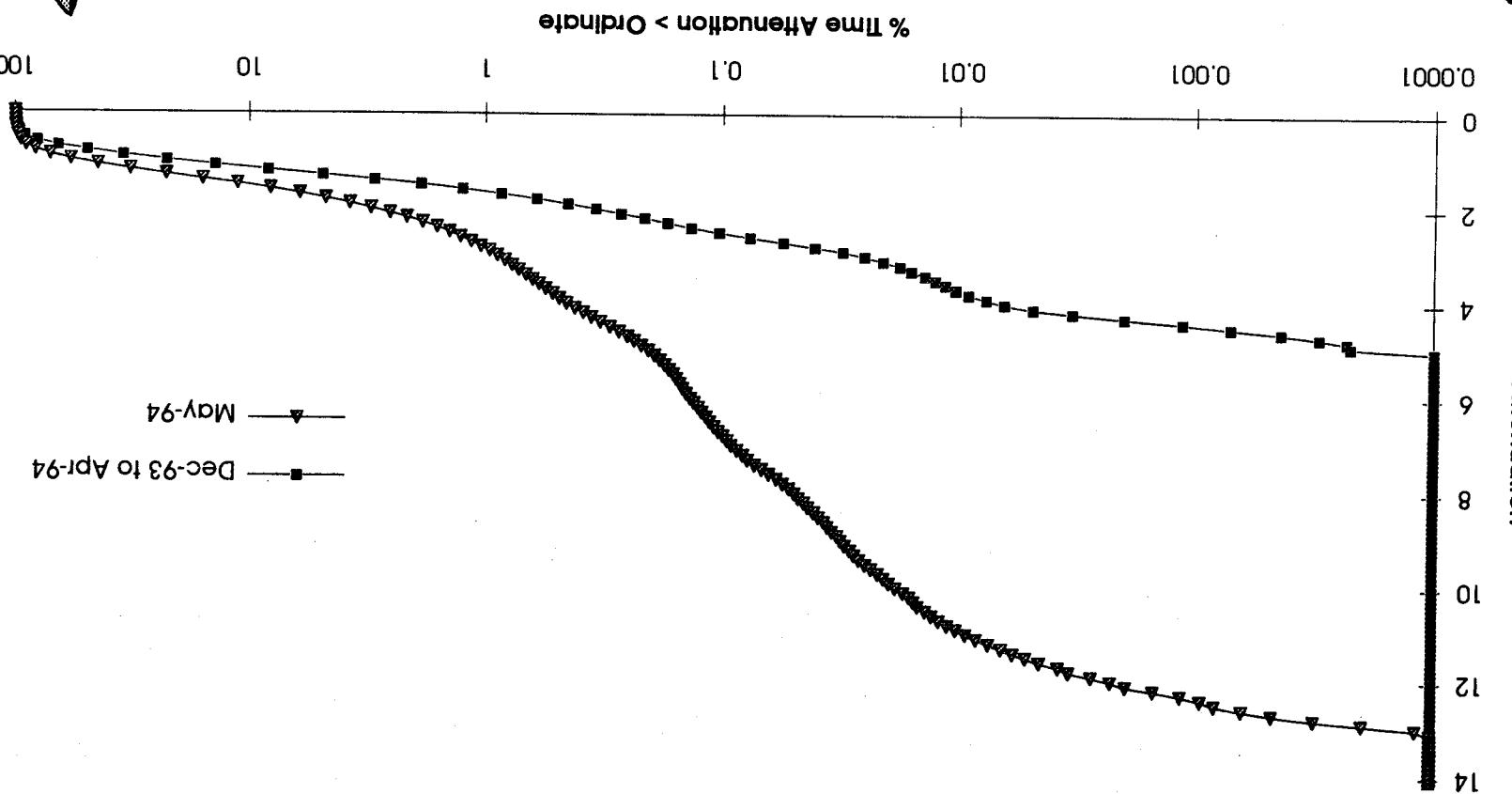
- APT MODIFICATIONS
  - ANGLED MOUNT POLE
  - RF BOX BRACING
  - SNOW FAN
  - ADDITIONAL INSULATION WITH REFLECTIVE COATING
- PROBLEMS
  - EMI
  - DYNAMIC RANGE LIMITATIONS
  - SATELLITE POINTING VARIATIONS
- OPERATION
  - POWER OUTAGES

Alaska ACTS Propagation

# Alaska ACTS Propagation

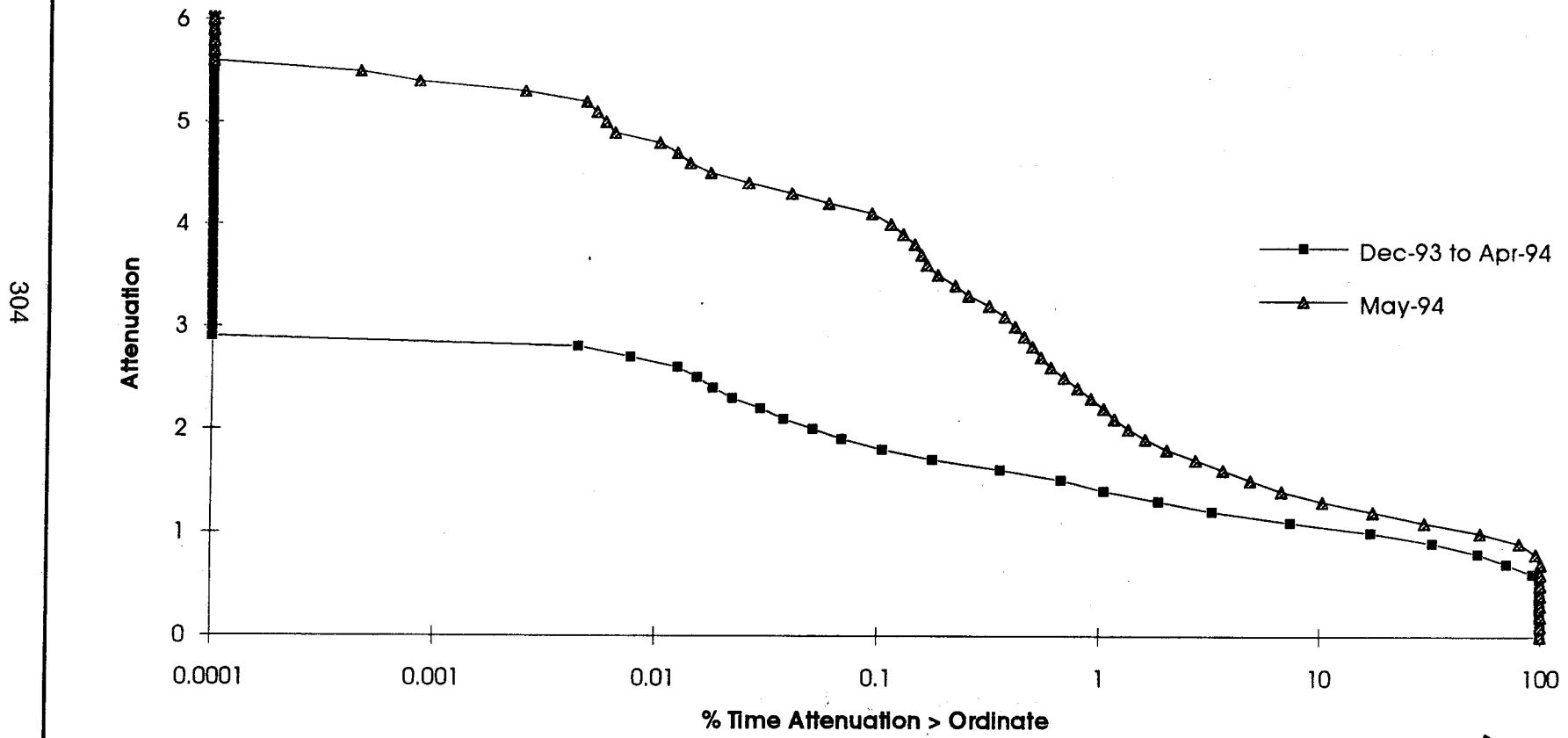


# Alaska ACTS Propagation



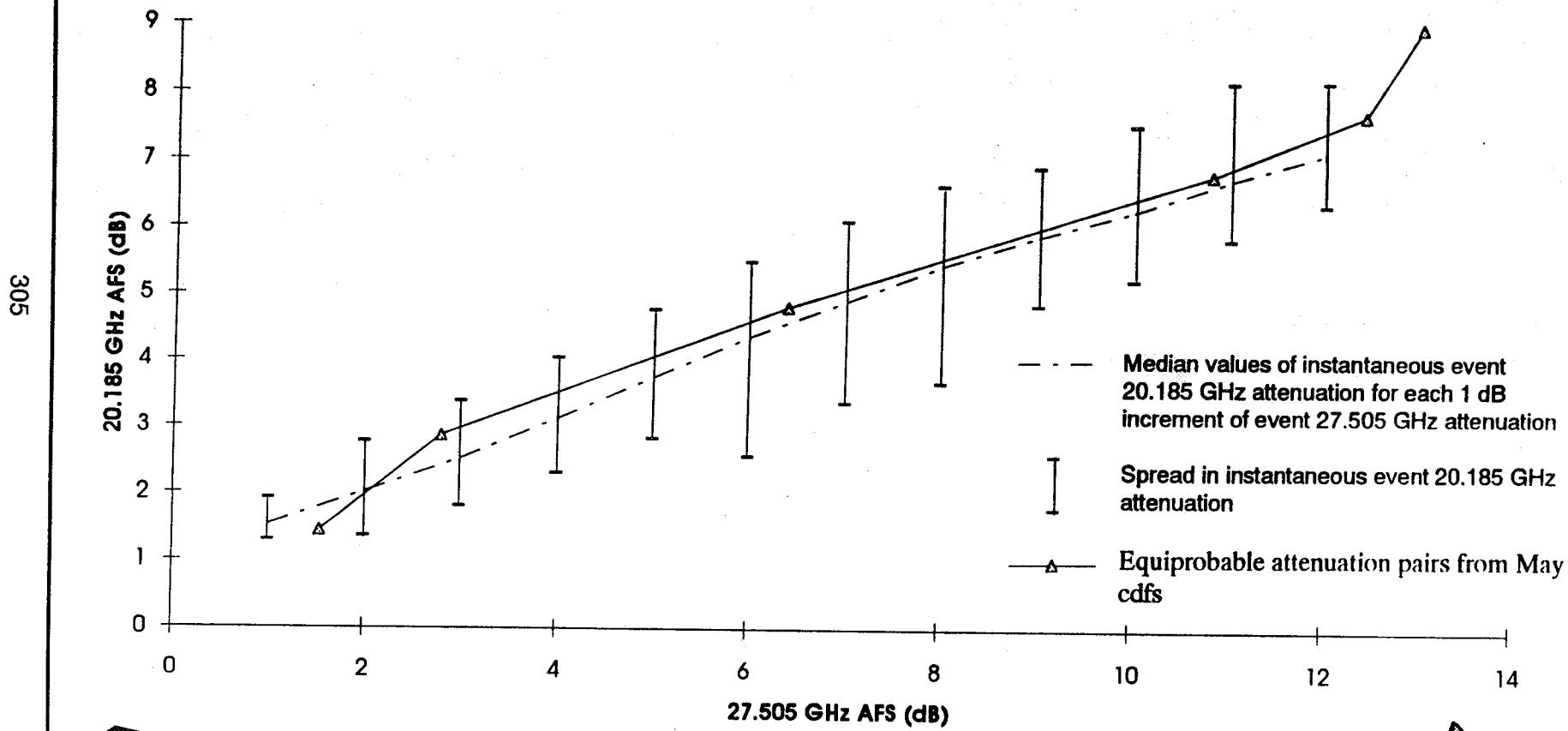
27.505 GHz Beacon CDFs

### 27.505 GHz Radiometer CDFs



Alaska ACTS Propagation

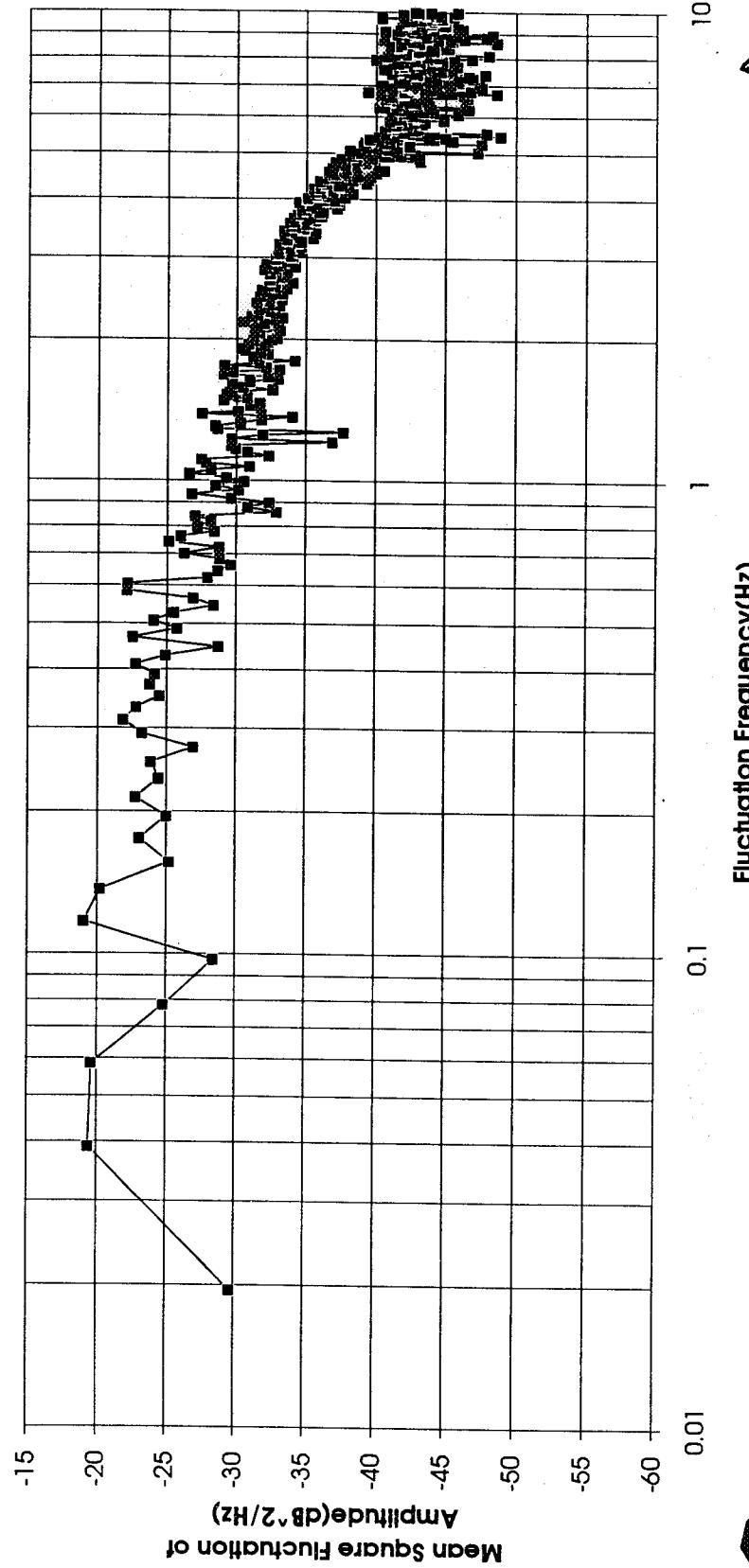
**20.185GHz AFS vs 27.505 GHz AFS 5/24/94 11-12 H GMT**



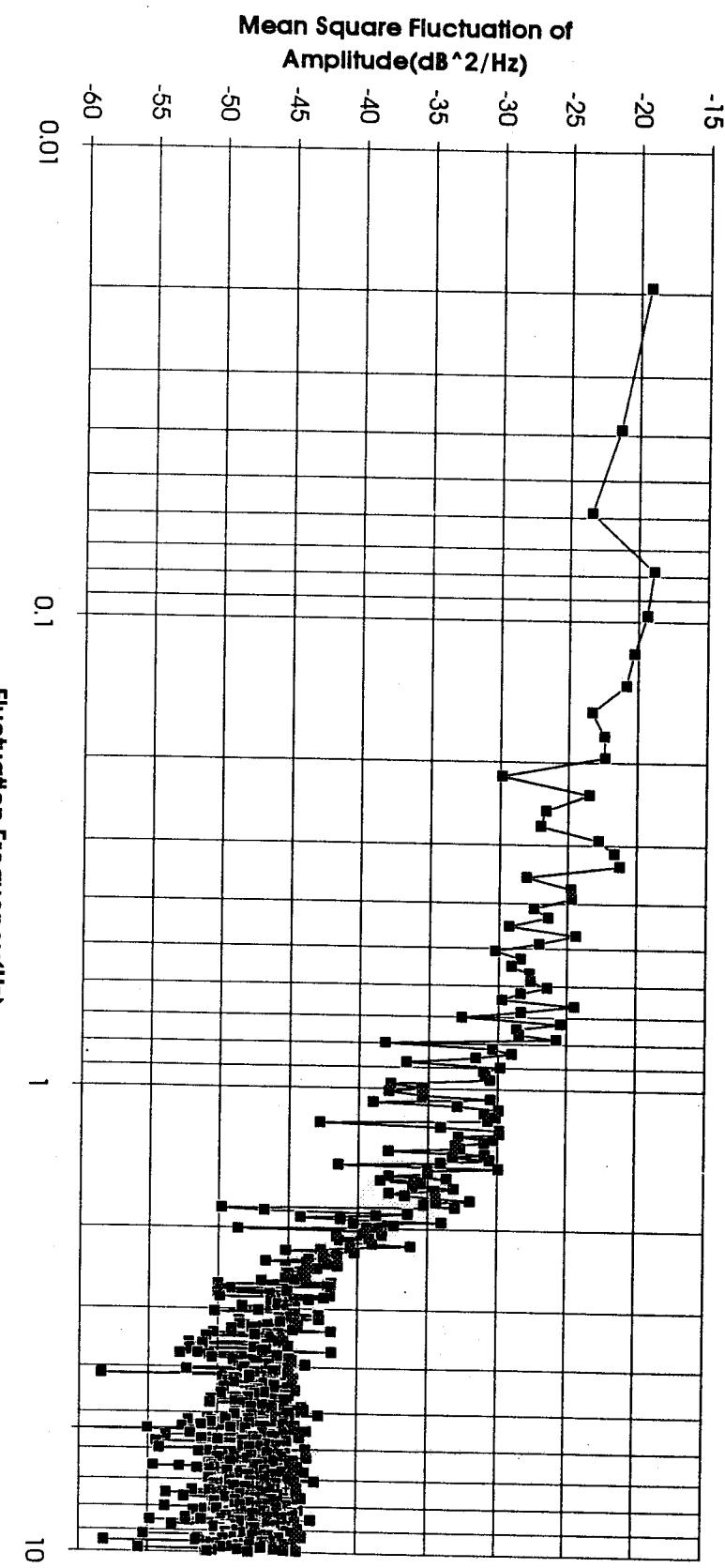
**Alaska ACTS Propagation**

# Alaska ACTS Propagation

27.505 GHz Scintillation Spectrum  
Scintillation Intensity of 0.19 on 5/25/94 07:41:51-07:42:42.2 GMT

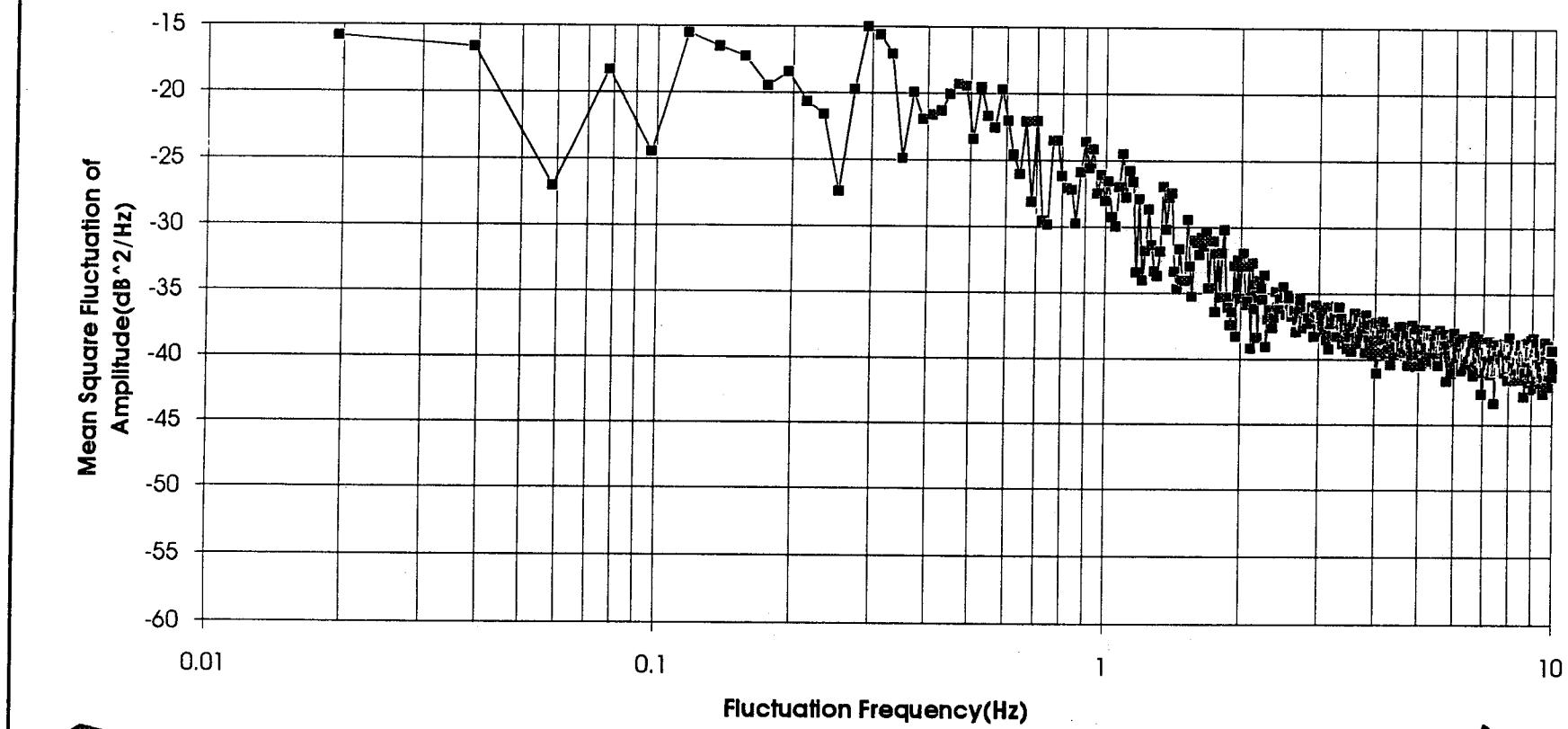


27.505 GHz Scintillation Spectrum  
Scintillation Intensity of 0.50 on 5/25/94 22:57:04-22:57:55.2 GMT



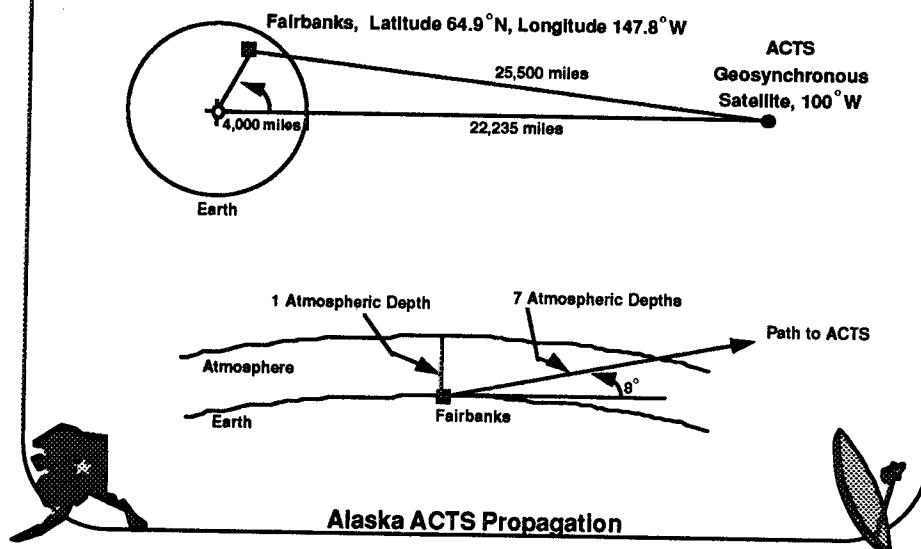
Alaska ACTS Propagation

**27.505 GHz Scintillation Spectrum**  
**Scintillation Intensity of 0.51 with 3.4 dB AFS on 5/27/94 23:14:42-23:15:33.2 GMT**

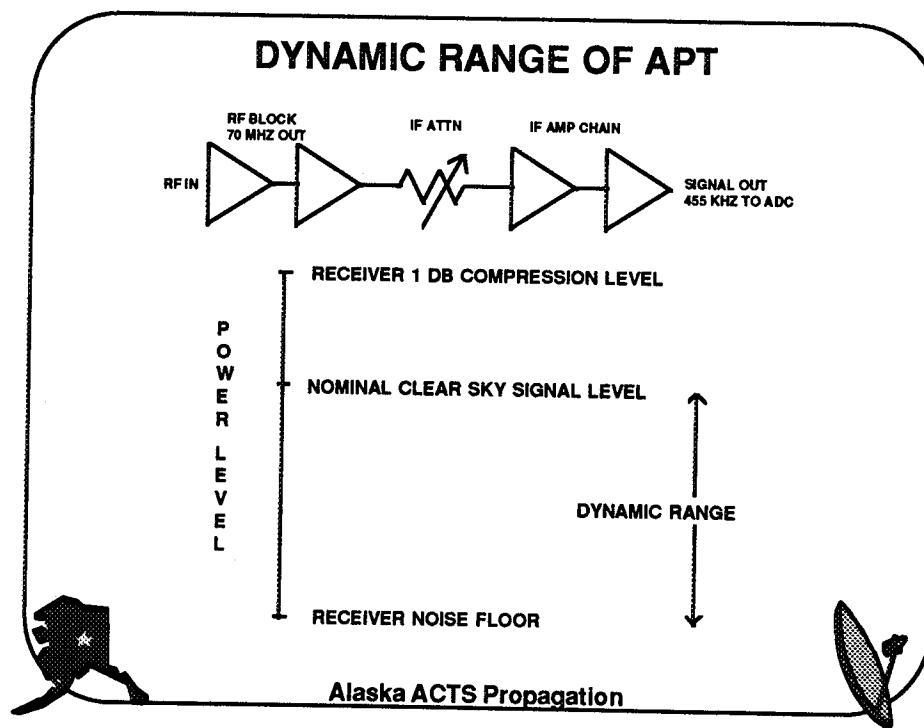


**Alaska ACTS Propagation**

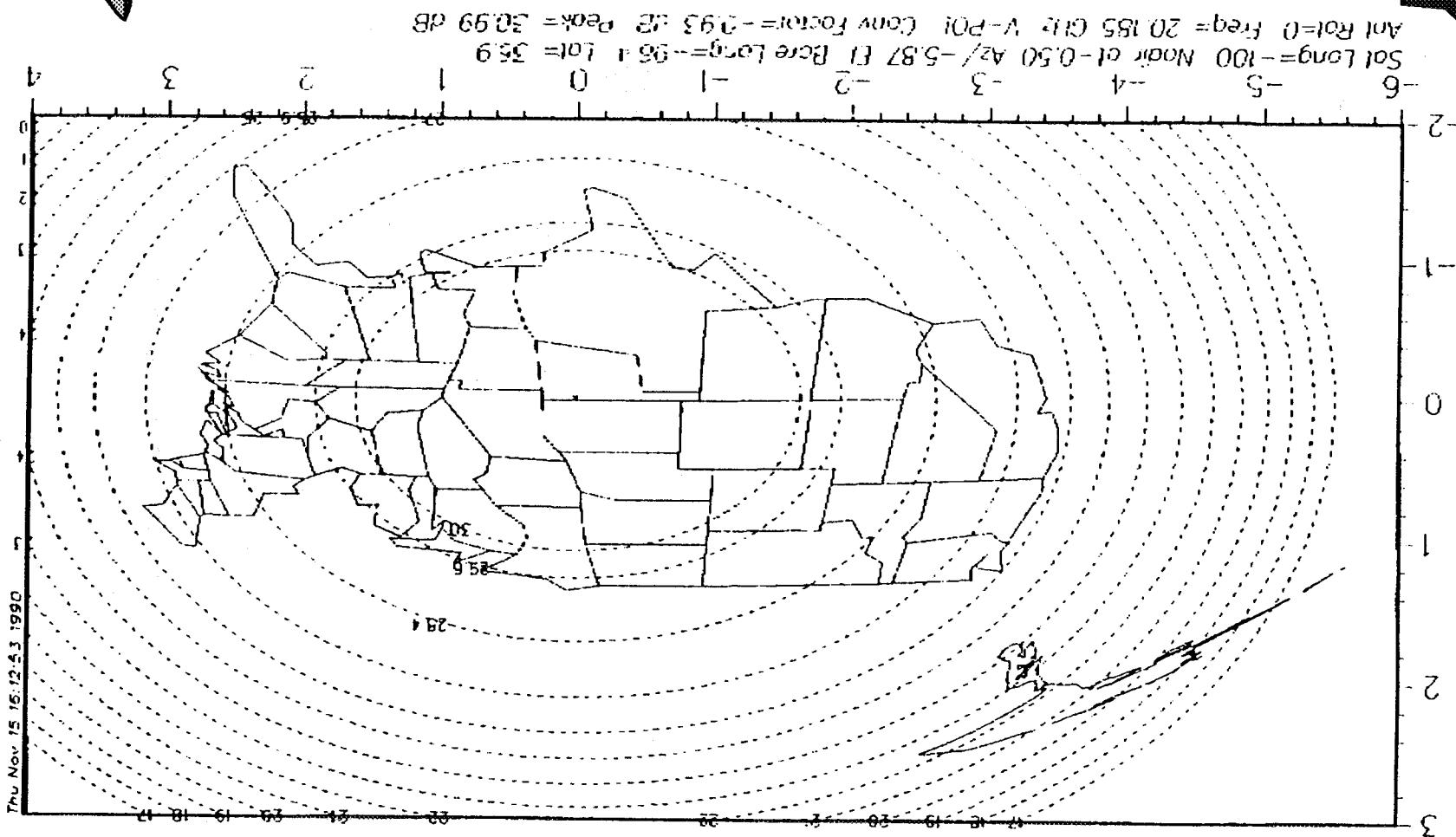
## SATELLITE TO EARTH GEOMETRY

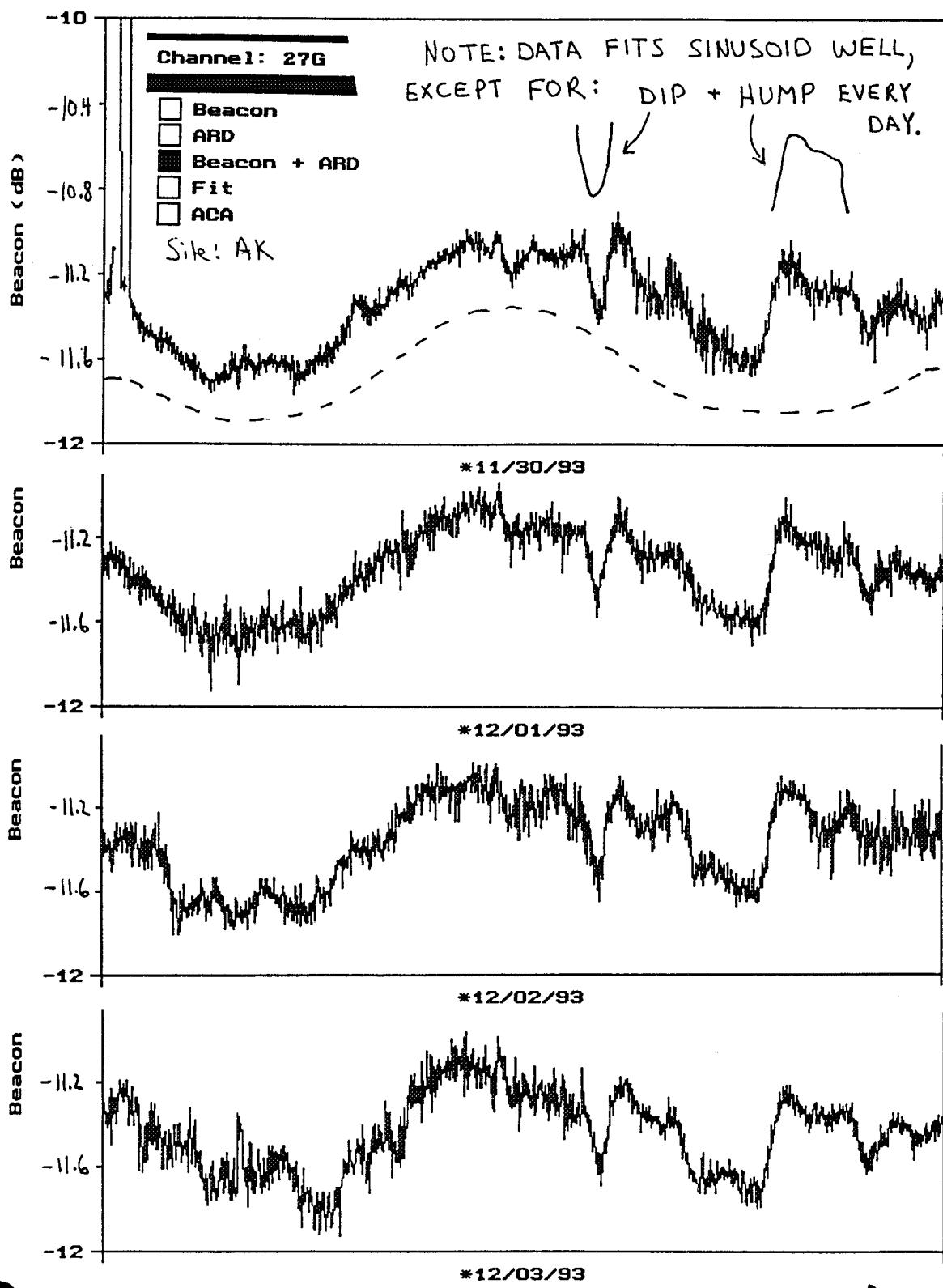


## DYNAMIC RANGE OF APT



# Alaska ACTS Propagation

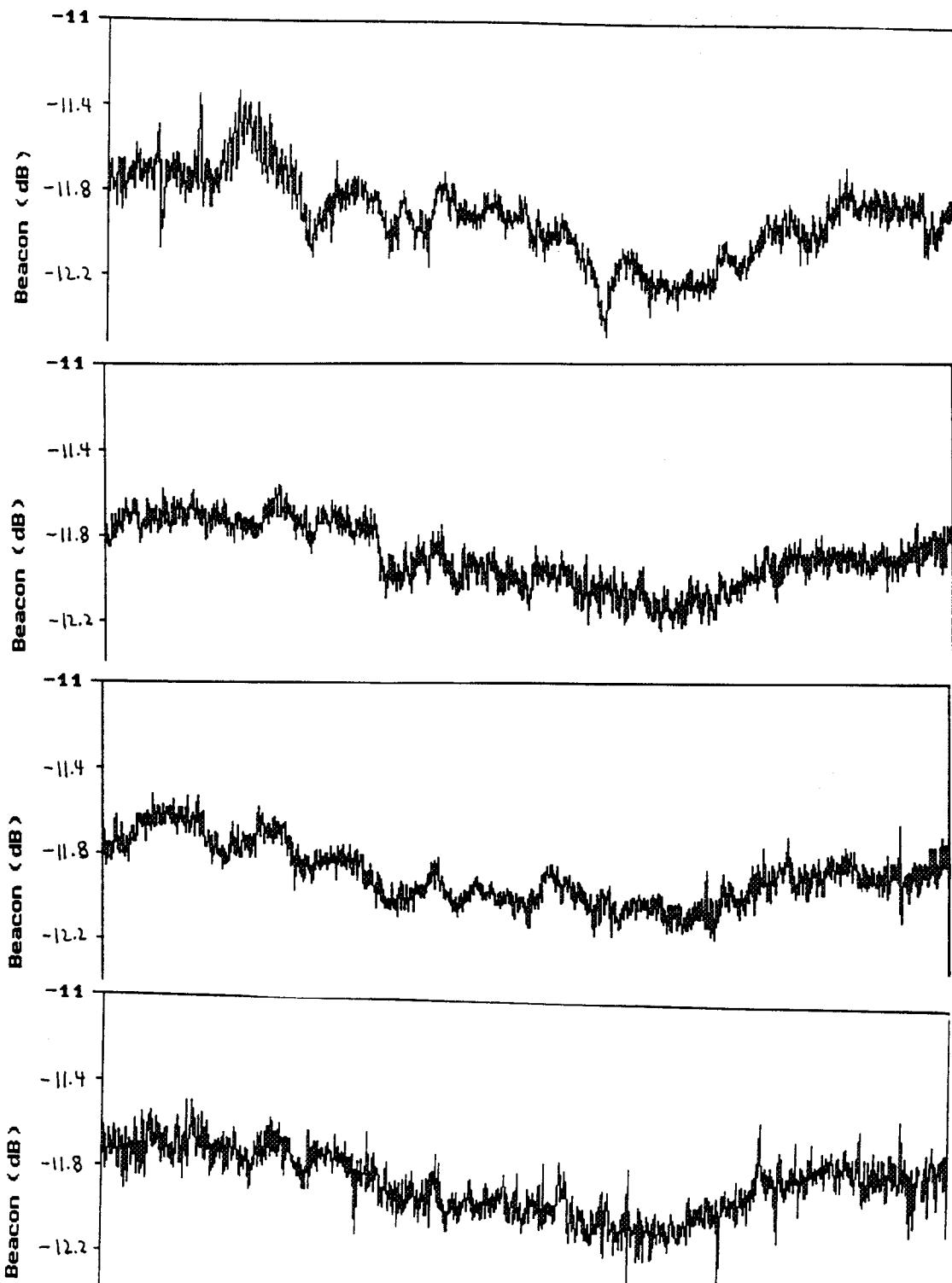




Alaska ACTS Propagation

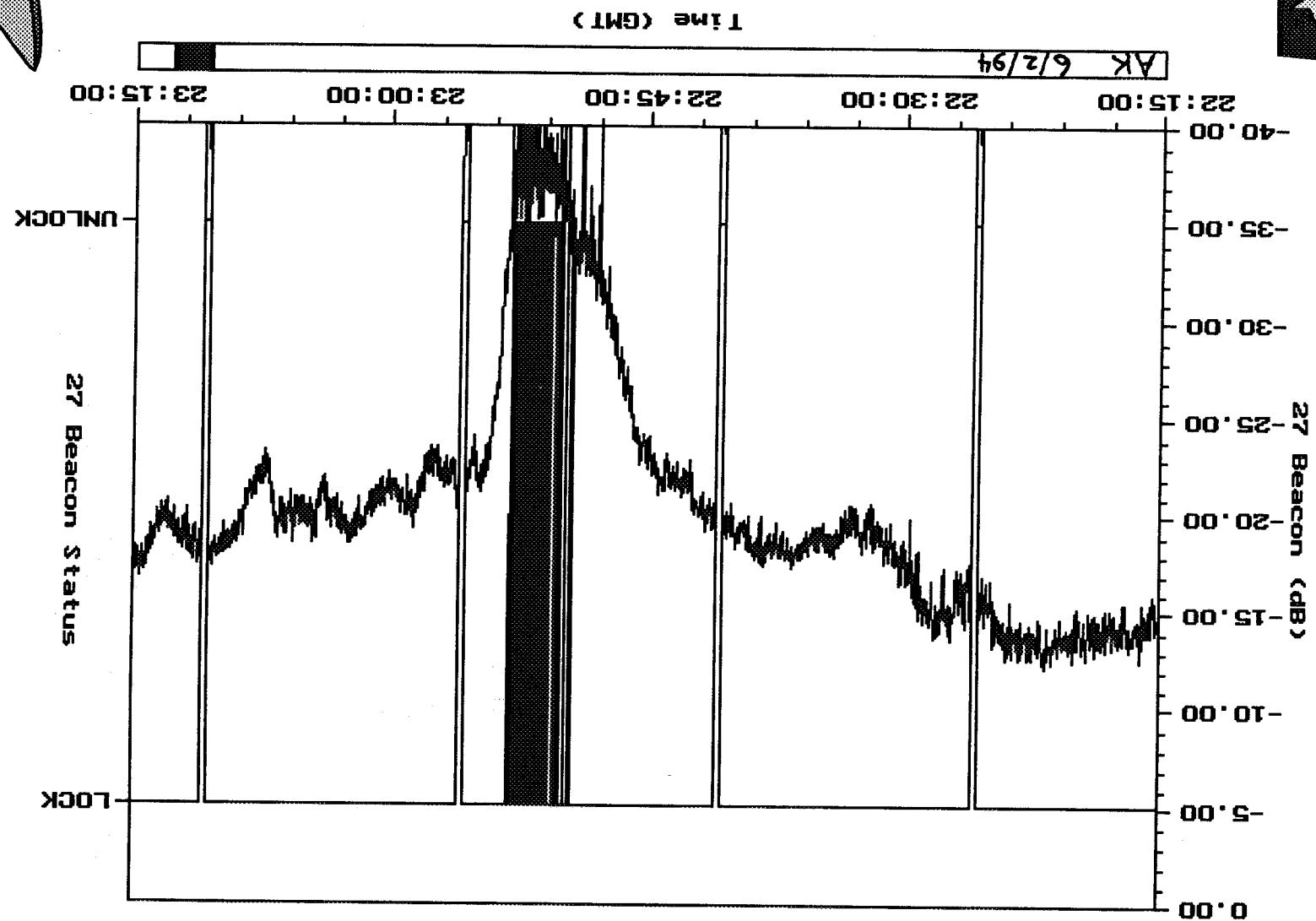
27 GHz Beacon + ARD  
0.4 dB/tick mark

2/20-23/94  
Site: AK



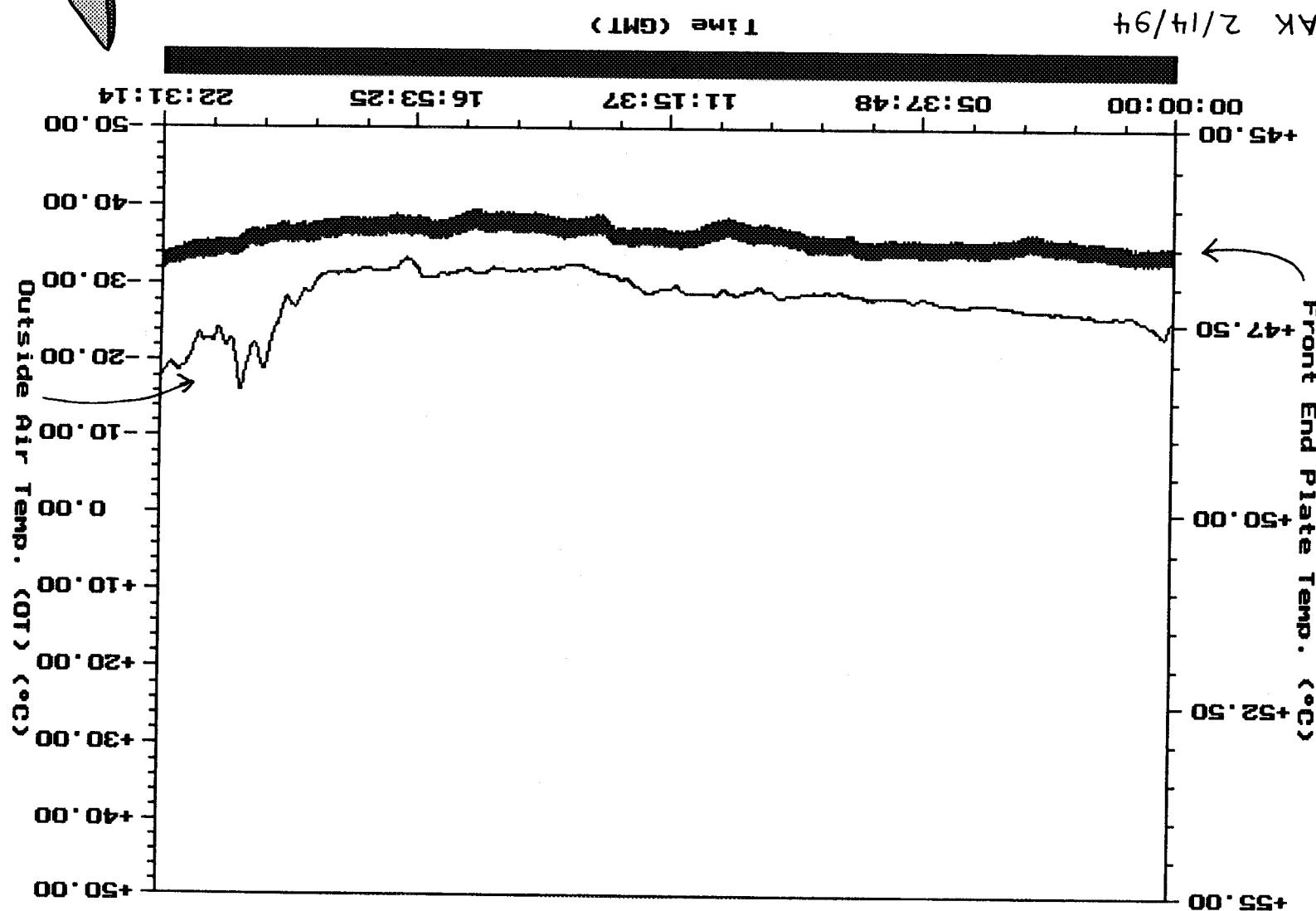
Alaska ACTS Propagation

# Alaska ACTS Propagation



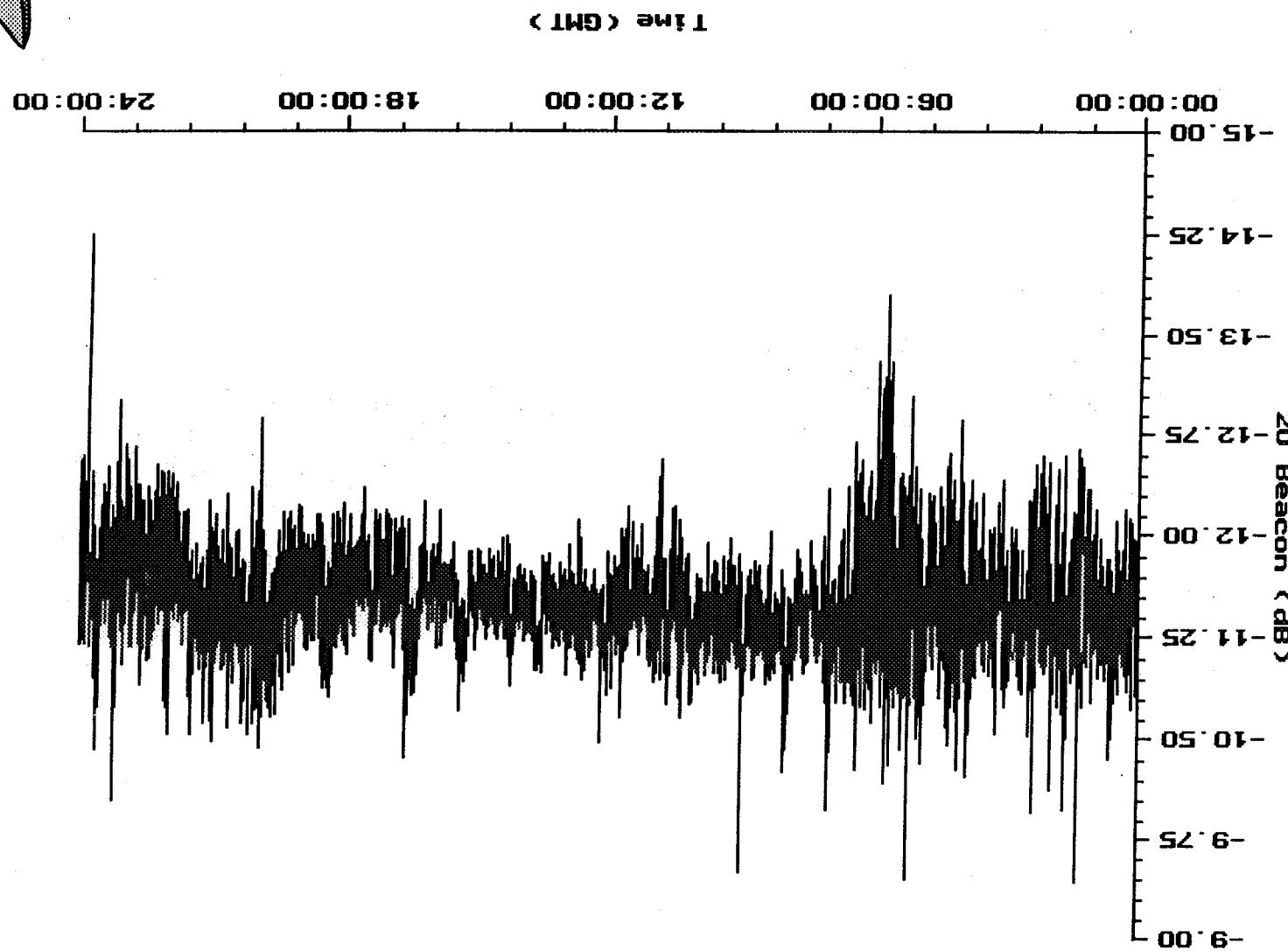
# AK Dynamic Range Limitation

# Alaska ACTS Propagation



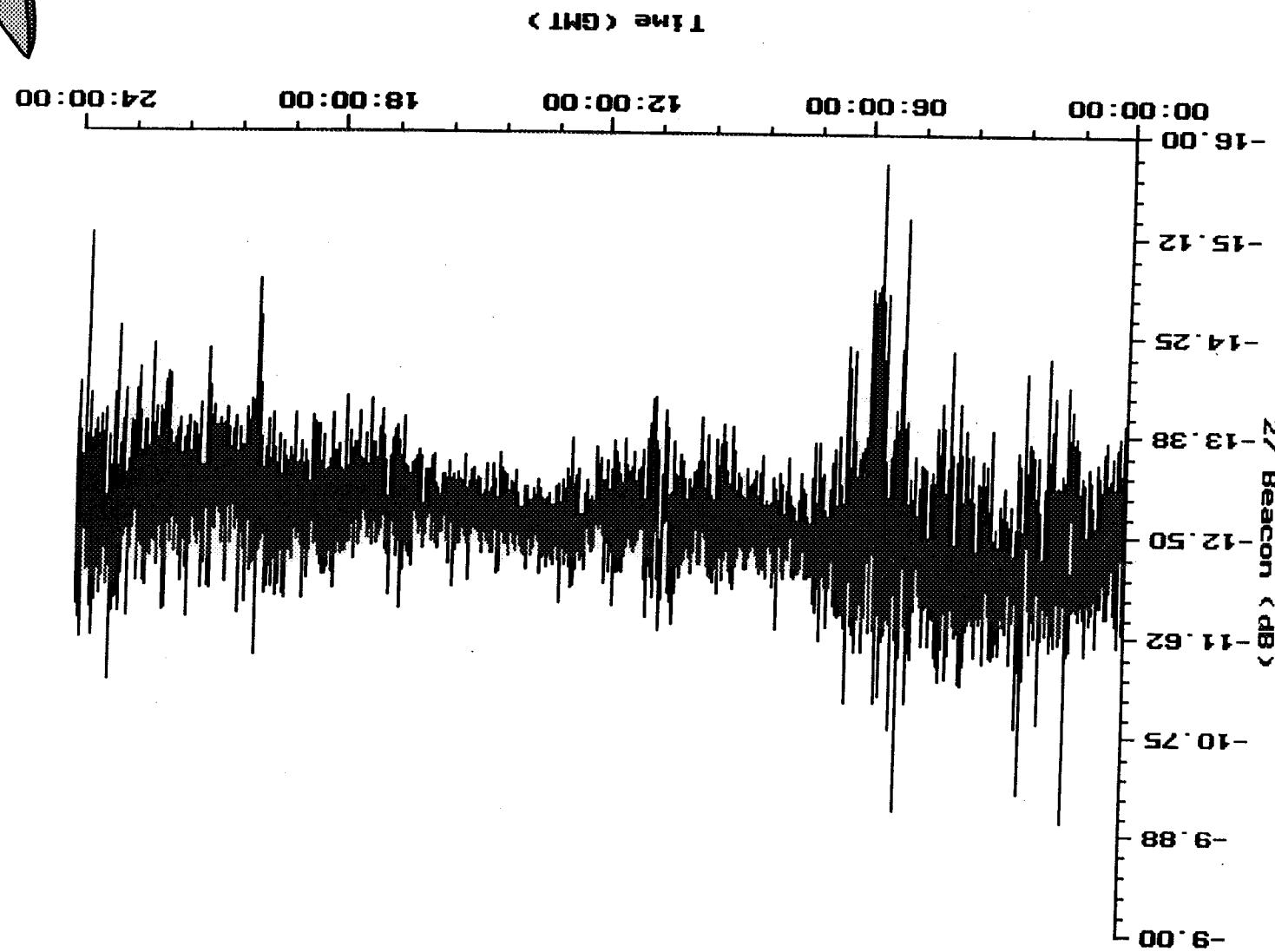
Outside Air and Front End Plate Temperatures

# Alaska ACTS Propagation

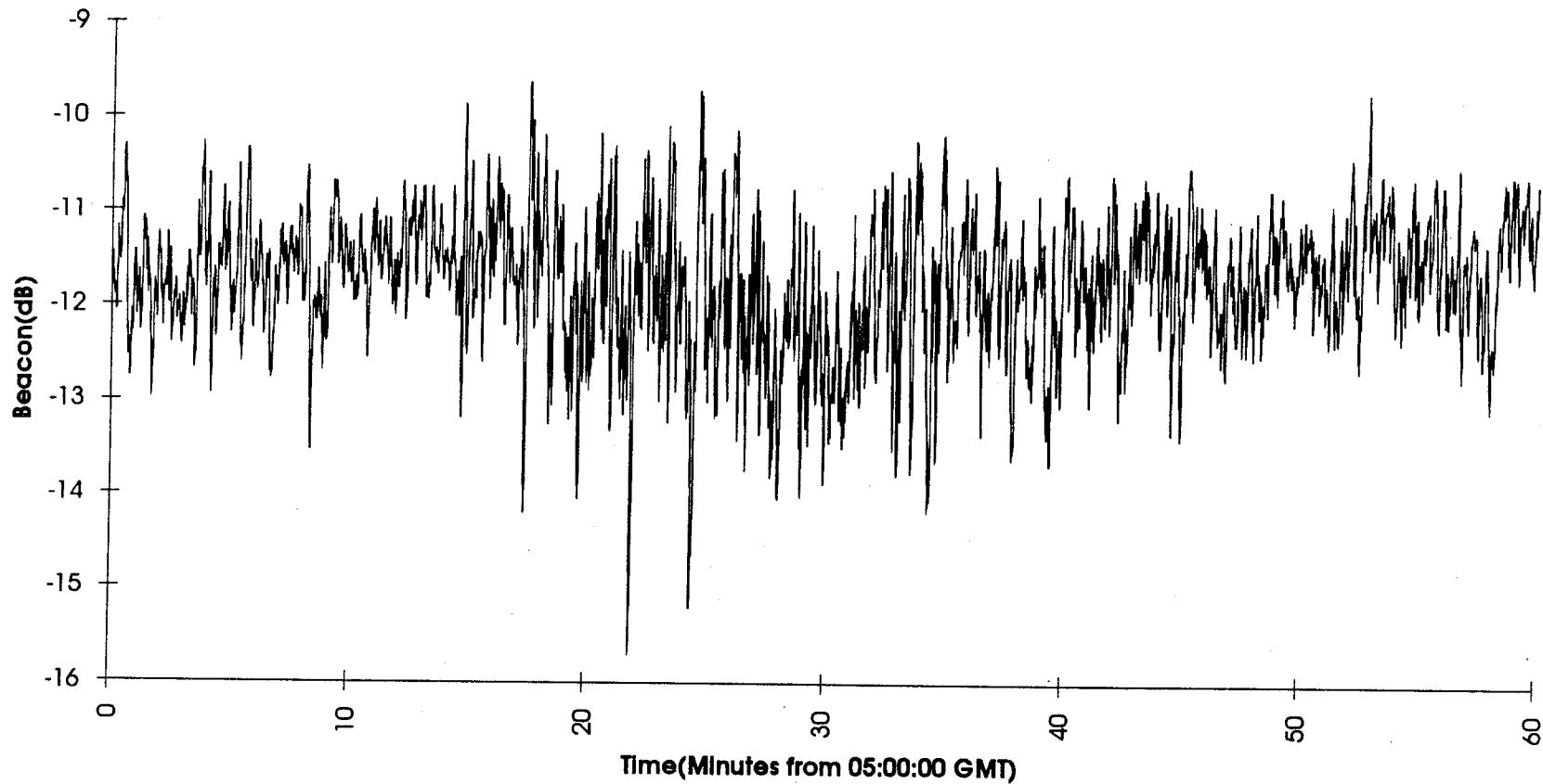


20.185 GHz Beacon 5/14/94 0-24 H GMT

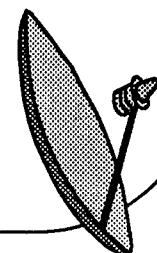
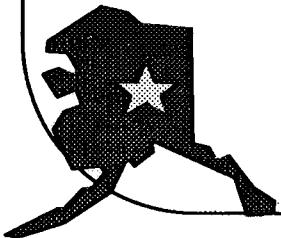
# Alaska ACTS Propagation



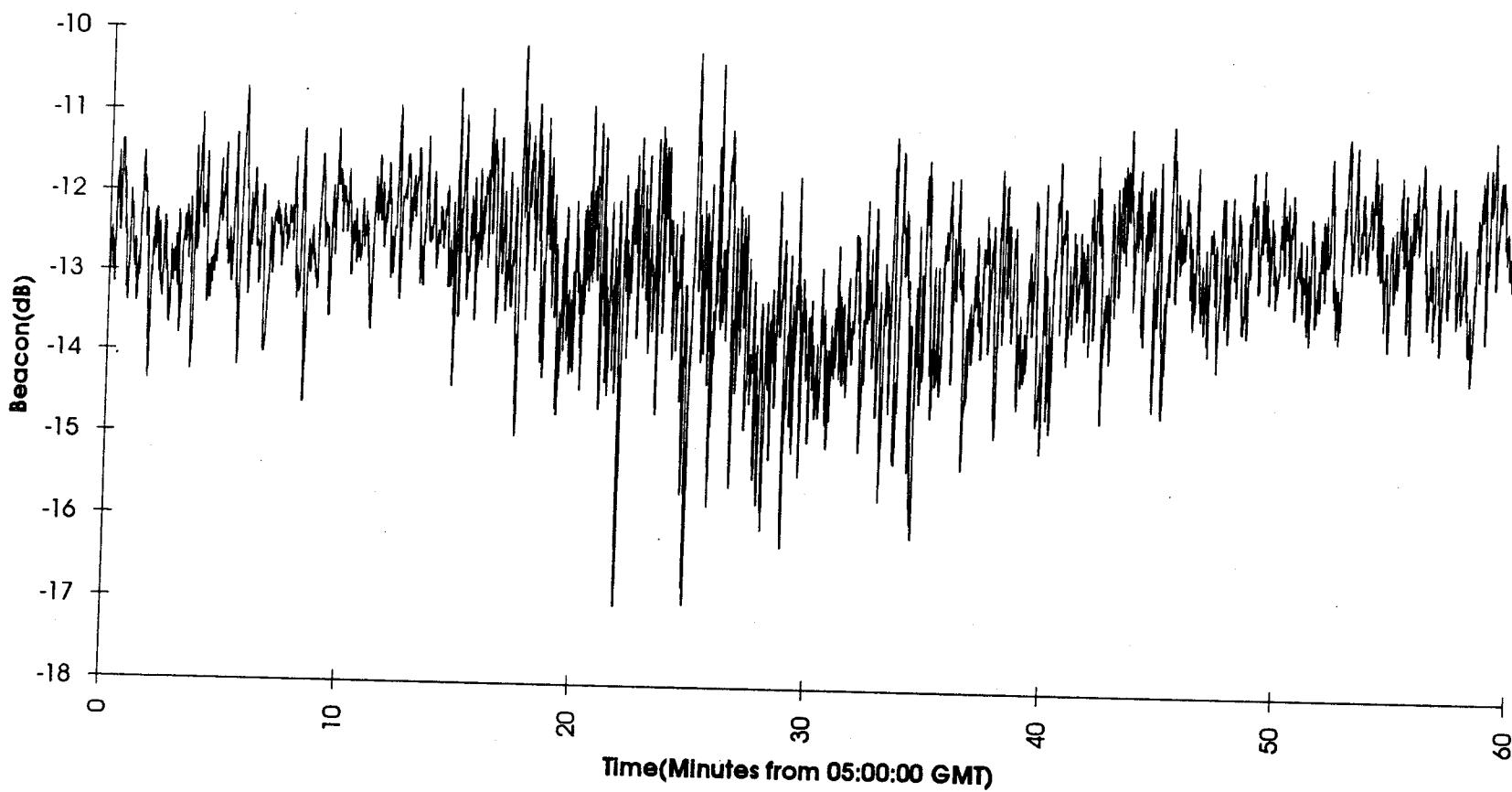
**20.185 GHz Beacon 5/14/94 5-6 H GMT**



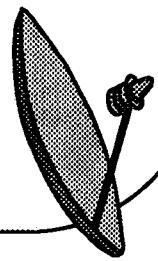
**Alaska ACTS Propagation**



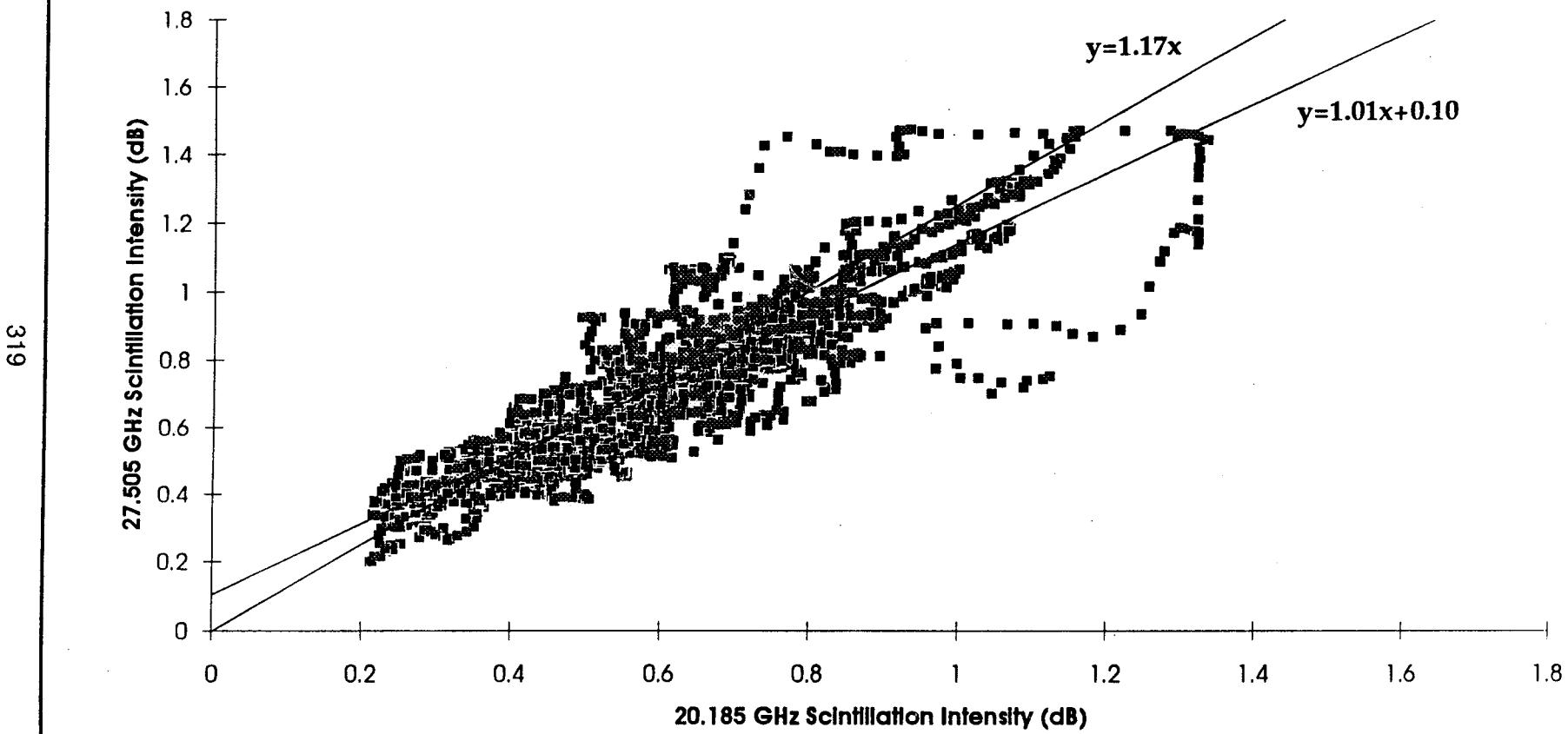
**27.505 GHz Beacon 5/14/94 5-6 H GMT**



**Alaska ACTS Propagation**



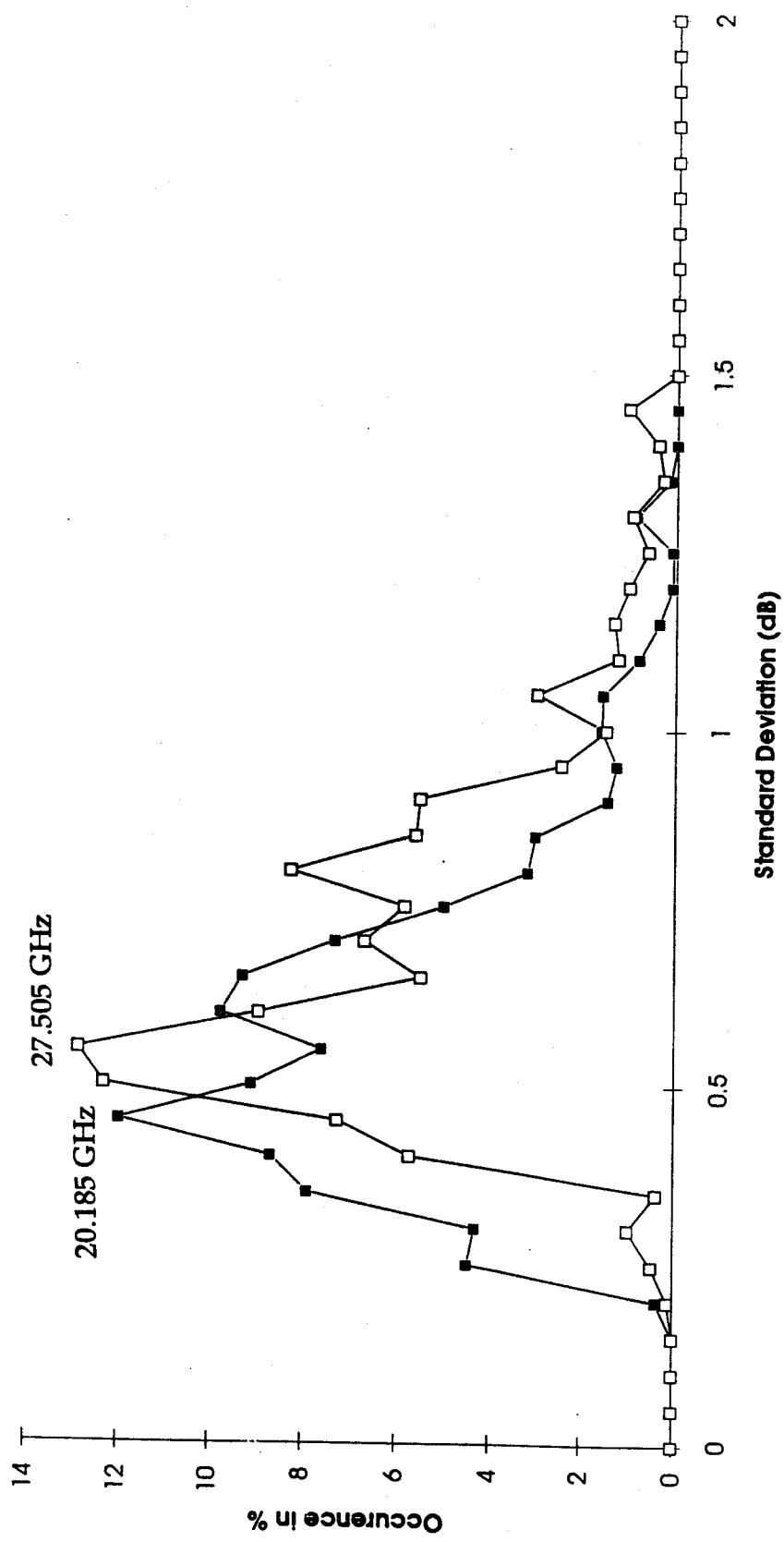
Scatter Plot of Scintillation Intensity 5/14/94 5-6 H GMT



Alaska ACTS Propagation

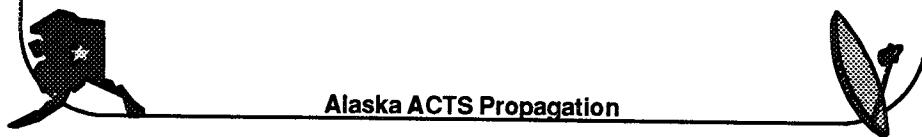
# Alaska ACTS Propagation

Measured p.d.f. 5/14/94 5-6 H GMT



## **SCINTILLATION RATIO PREDICTIONS**

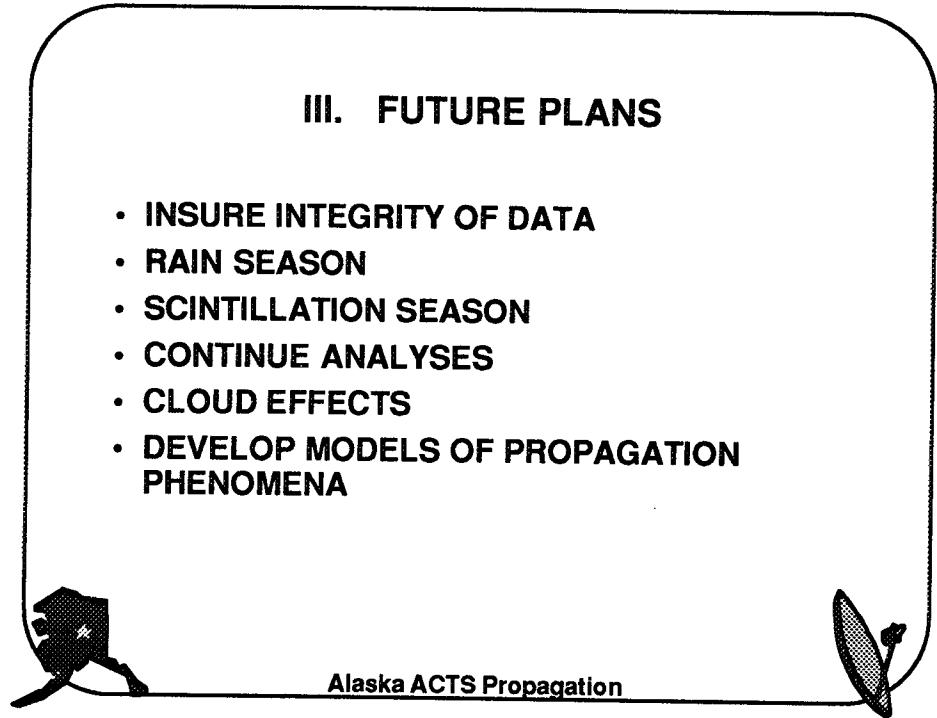
- FREQUENCY RATIO, 27.5/20.2 GHZ
  - FOR 1.22-M ANTENNA
    - » 1.19
- ANTENNA SIZE RATIO, 1.5"/1.22-M
  - FOR 20.2 GHZ FREQUENCY
    - » 1.03
- USED CCIR/CRANE MODEL



Alaska ACTS Propagation

## **III. FUTURE PLANS**

- INSURE INTEGRITY OF DATA
- RAIN SEASON
- SCINTILLATION SEASON
- CONTINUE ANALYSES
- CLOUD EFFECTS
- DEVELOP MODELS OF PROPAGATION PHENOMENA



Alaska ACTS Propagation



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# U.B.C. ACTS PROPAGATION EXPERIMENT

By:

I. Dommel  
R. Hulays  
M. Kharadly

Electrical Engineering Department  
University of British Columbia

June 16, 1994

## OUTLINE

- STATUS
- SOME PROBLEMS
- SOME OBSERVATIONS
- PRESENT AND FUTURE WORK

## STATUS

325

- LATEST DACS SOFTWARE UPDATE INSTALLED ON JUNE 7, 1994
- RAW DATA, PRE-PROCESSED DATA AND EVENT AND FAULT LOGS UP TO, AND INCLUDING APRIL 1994 WERE SENT TO ACTS DATA CENTER. MAY DATA IS NOW COMPLETE
- ELEVATION TILT SCAN
  - ◊ Weather has not been cooperative!
  - ◊ No local sounding stations. The closest stations are:

- \* Quillayute (Olympic peninsula): 220 km, S.W.
- \* Port Hardy (Northern Vancouver island): 360 km, N.W.
- \* Vernon (Okanagan): 300 km, E.

- ◊ Possibility of interpolating between the three sounding sites
- ◊ Results thus obtained may not be valid at our site up to a height of 2 km.
- ◊ Attempting to arrange for a sounding on Campus

- HYDROPHOBIC PAINT TEST
  - ◊ This has been tested, loss is hardly measurable, less than 0.1 dB signal loss at 29.6 GHz
  - ◊ Has not yet been applied to antenna
- SURVEILLANCE CAMERA AND TIME-LAPSE RECORDER
  - ◊ Installed to keep track of antenna surface conditions (e.g., Icing) and weather conditions (e.g., Rain, Snow)
  - ◊ Records are obtained every 8 seconds with tape lasting 40 days

## ADDITIONAL RESOURCE

- AIRPORT WEATHER STATION

- ◊ Approx. 8 km from APT site
- ◊ Close to propagation path
- ◊ Will use their monthly statistics to compare to ours

## SOME PROBLEMS

- 27 GHz RADIOMETER STEPS CAUSING RADIOMETER RESTARTS, Fig. 1
- RADIOMETERS VOLTAGE DRIFT, Fig. 2
  - ◊ A manual reboot, at times, corrects the problem
- ACTSEdit PROBLEMS
  - ◊ Inability of software to remove certain spikes (e.g. Fig. 3)

- ◊ This causes error in the attenuation cumulative distribution function plots (Fig. 4)
- DR. CRANE'S EDITING PROGRAM
  - ◊ We have not yet been able to make it work

## SOME OBSERVATIONS

- TYPICAL FADES AT VANCOUVER, Figs. 5 and 6
  - ◊ Long duration
  - ◊ Low fade
  - ◊ Radiometer-derived attenuation generally agrees with Beacon-derived attenuation

- ATYPICAL FADES AT VANCOUVER, Figs. 7 and 8

- ◊ Strong fade - System lost lock
- ◊ Radiometer-derived attenuation does not agree with Beacon-derived attenuation (Radiometer saturates at 10 dB?)
- ◊ 20 GHz attenuation > 27 GHz attenuation, Fig. 9
  - \* Some snow-fall was recorded
  - \* Possible cause (defocusing due to snow layer on antenna surface?)

- MONTHLY ATTENUATION STATISTICS
  - ◊ For the Month of January, Figs. 10 and 11
  - ◊ For the Month of March, Figs. 12 and 13
- ⇒ 20 GHz attenuation reaches higher values than 27 GHz attenuation!
- SCINTILLATIONS
  - ◊ Clear weather, Fig. 14
  - ◊ Rain, Fig. 15

## PRESENT AND FUTURE WORK

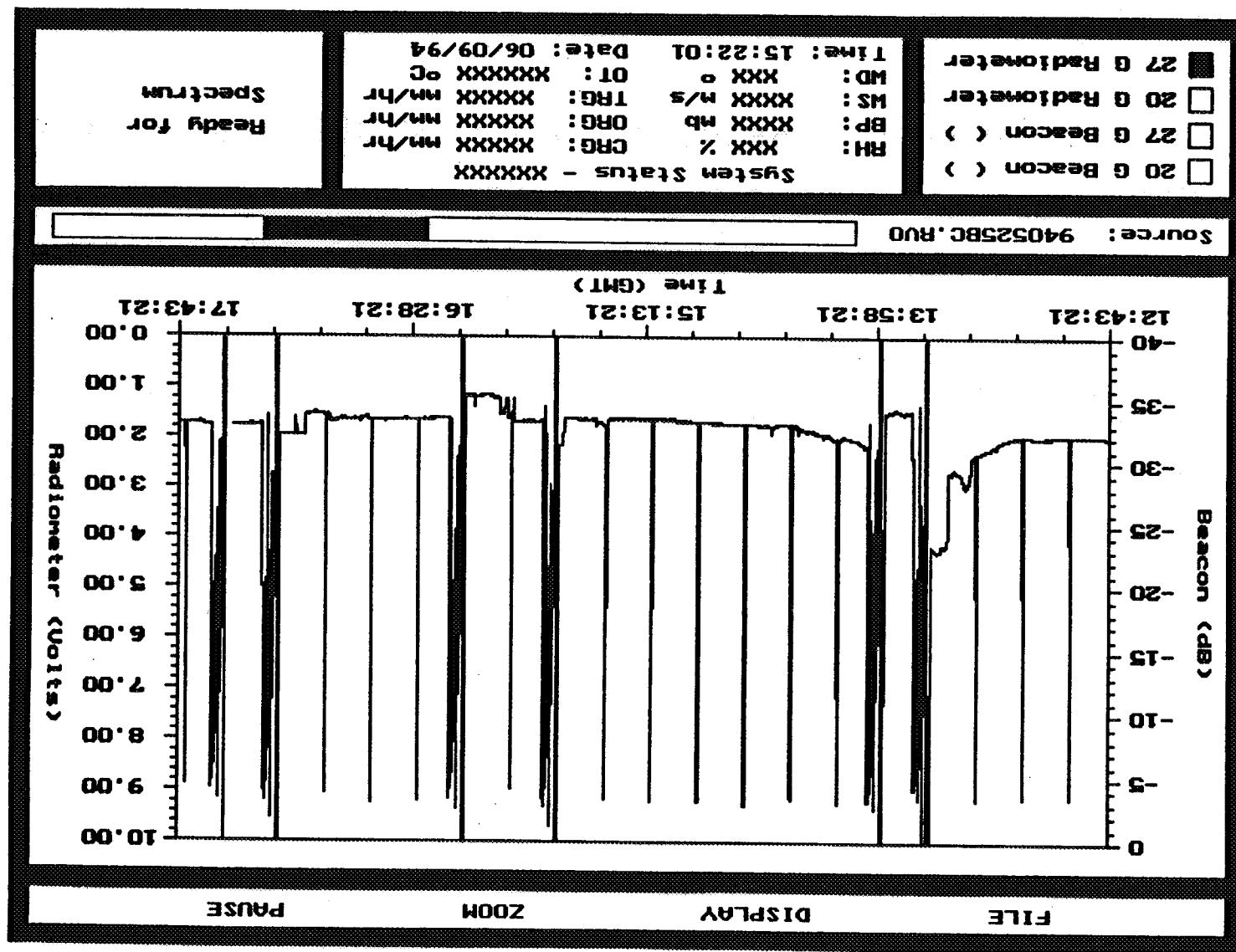
- ANALYSIS PACKAGE
  - ◊ Exceedance statistics
  - ◊ 27 GHz attenuation vs 20 GHz attenuation
  - ◊ Fade-duration statistics
  - ◊ Fill in missing data

- MELTING LAYER

- ◊ Estimation of the excess attenuation caused by the presence melting layer

- SCINTILLATIONS

Fig. 1: Typical 27 GHz radiometer steps causing automatic restart



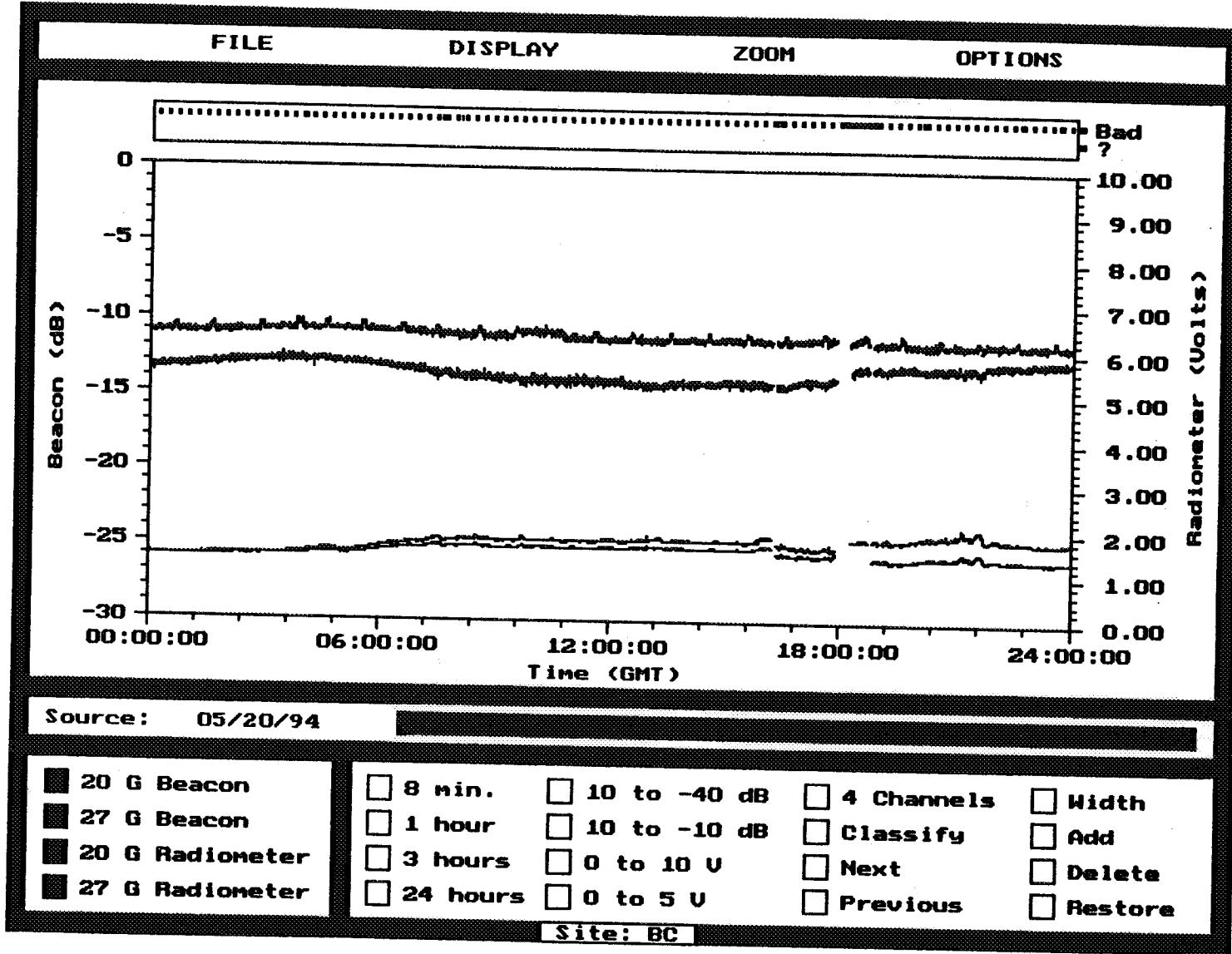


Fig. 2: Radiometer voltage drift

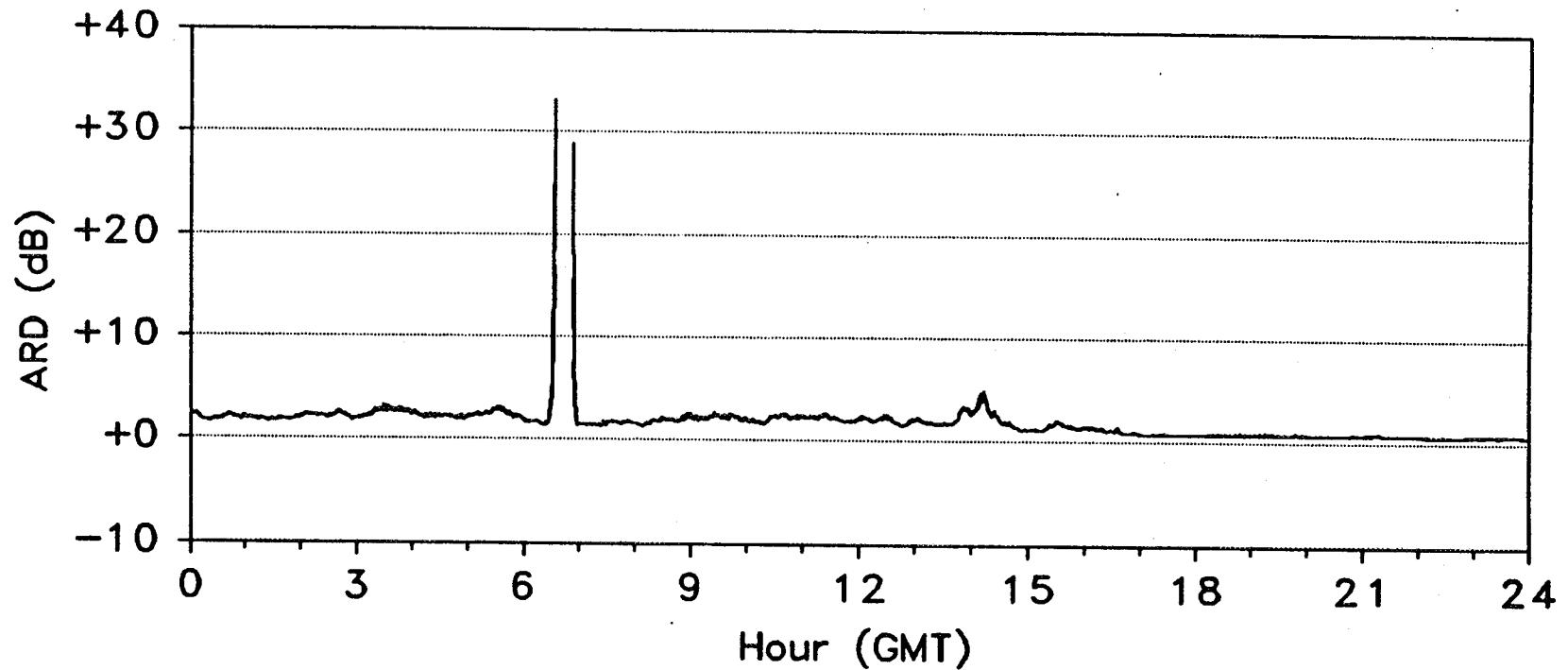


Fig. 3: Pre-processing software was unable to remove spike in 27 GHz radiometer-derived attenuation

FEB 1994 - 20 GHz AND 27 GHz RADIOMETER - BC

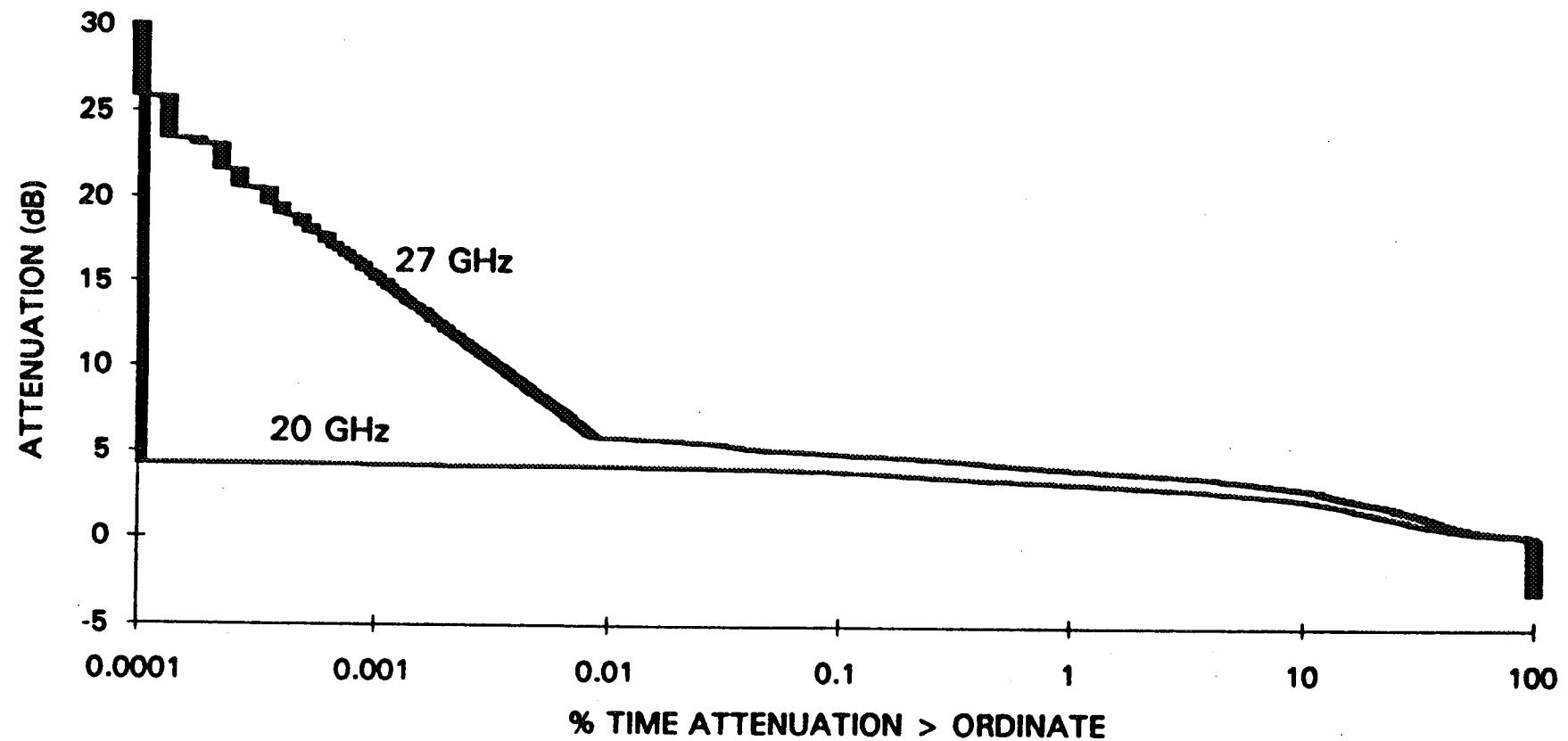


Fig. 4: Effect of the spike in Fig. 3 on the Cumulative Distribution Function of the 27 GHz radiometer-derived attenuation

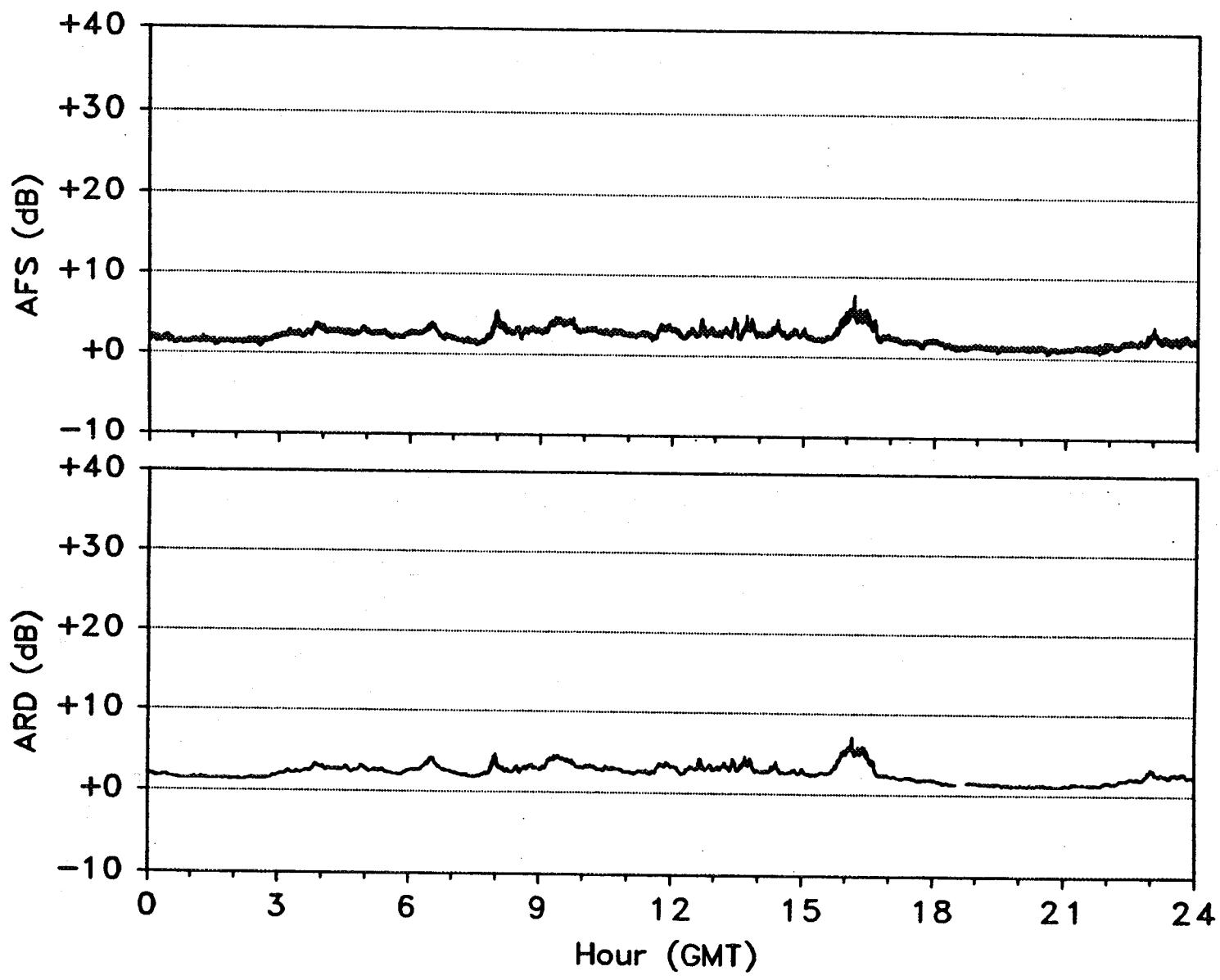


Fig. 5: 20 GHz attenuation for March 1, 1994

Fig. 6: 27 GHz attenuation for March 1, 1994

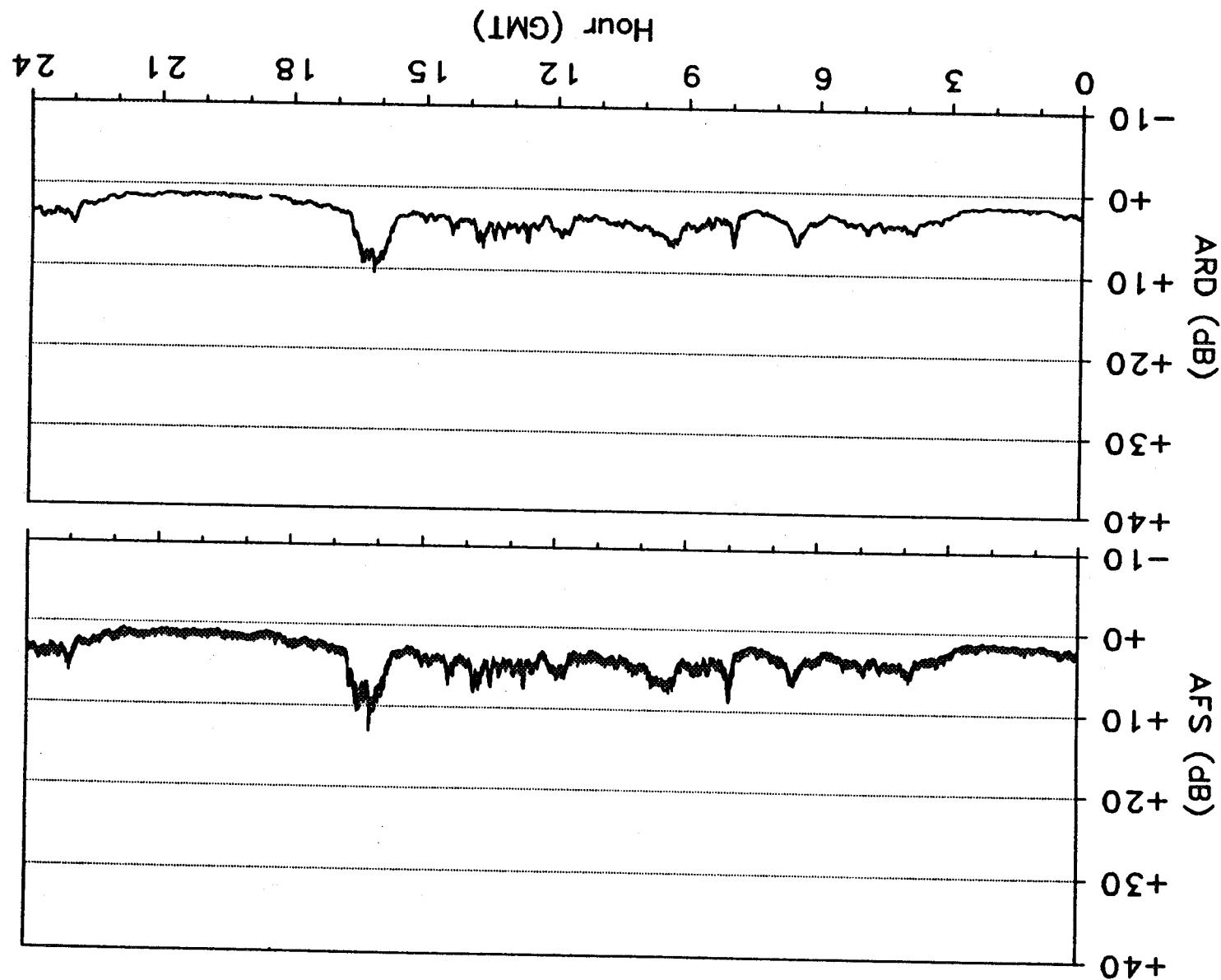


Fig. 7: 20 GHz attenuation for March 22, 1994

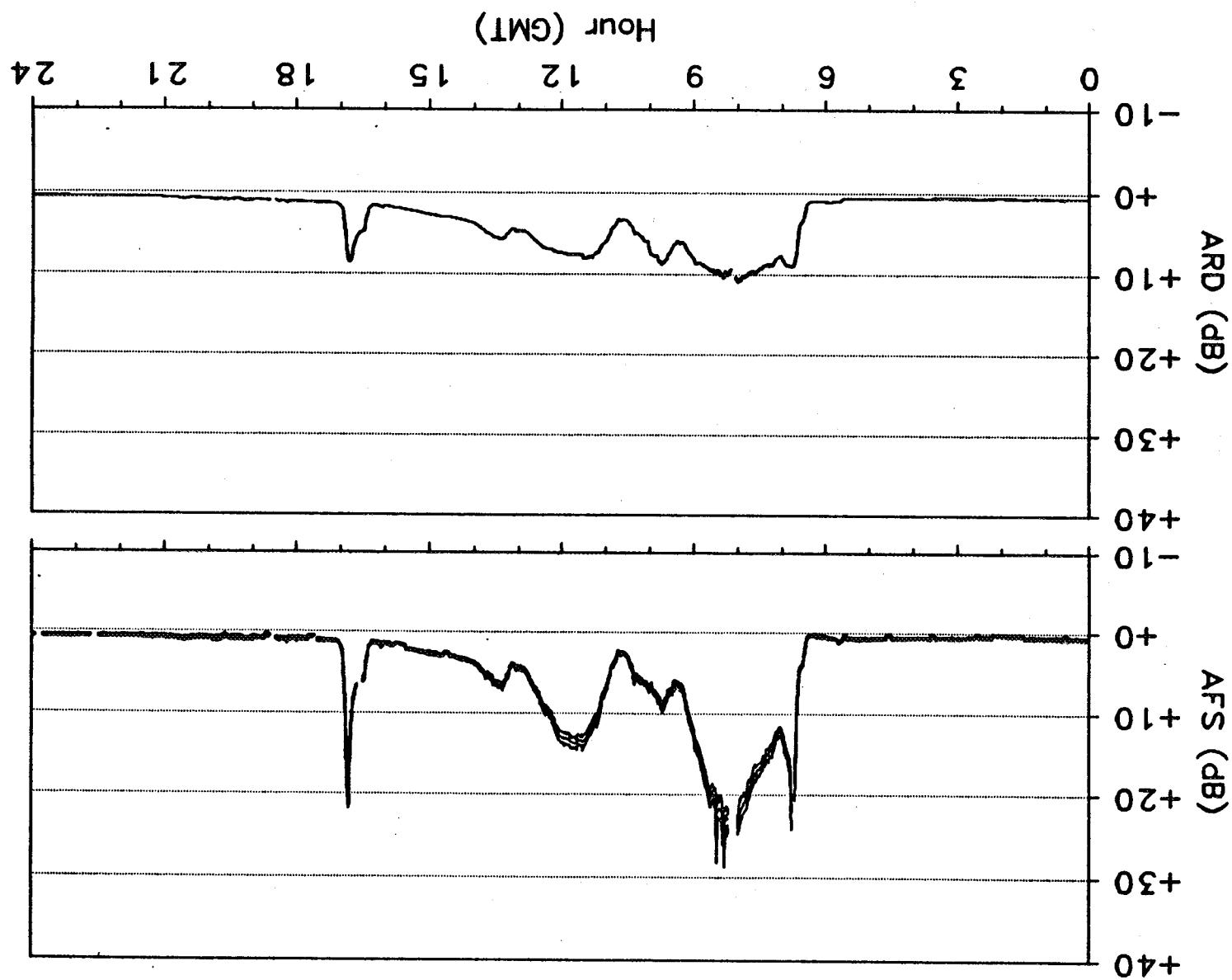


Fig. 8: 27 GHz attenuation for March 22, 1994

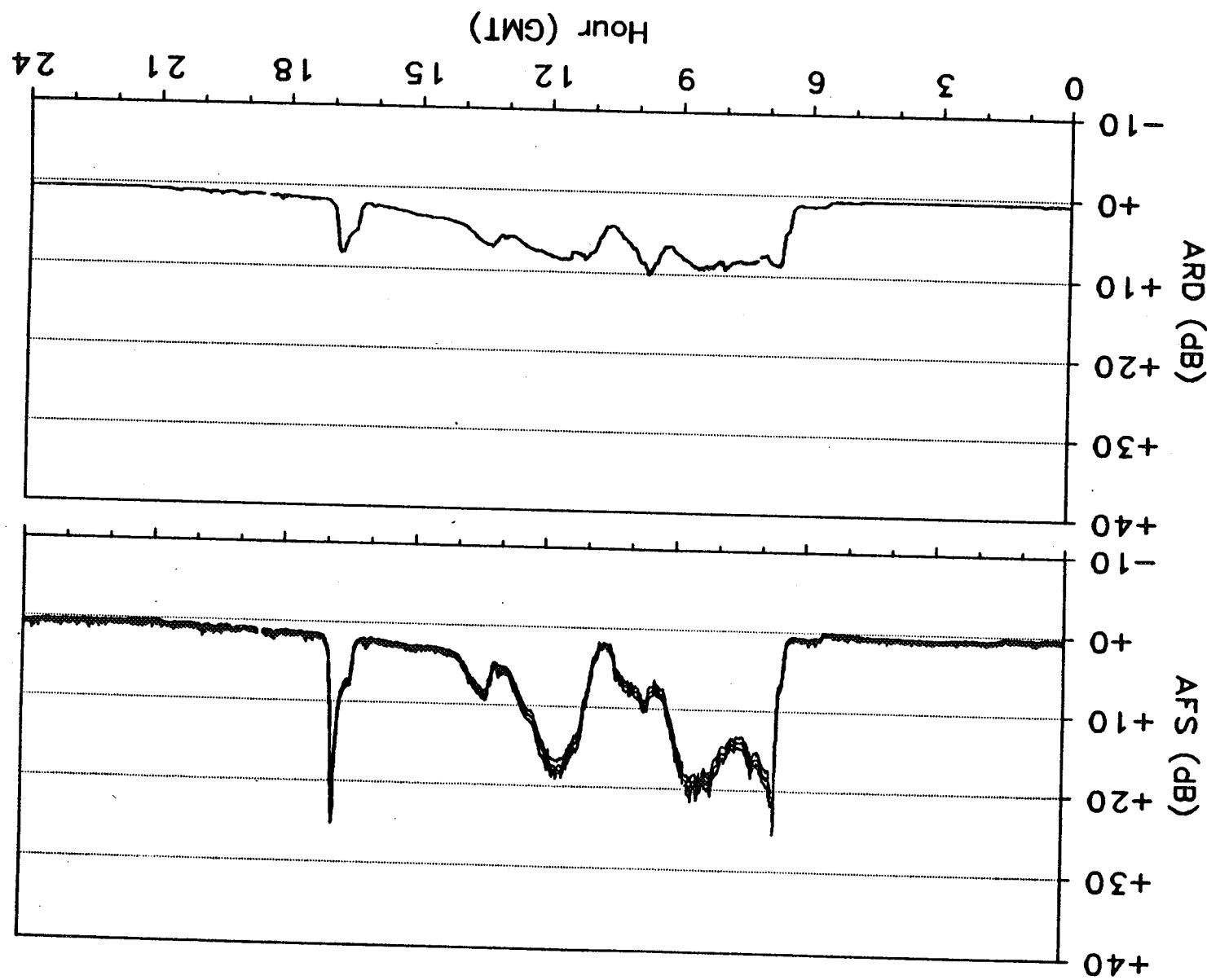
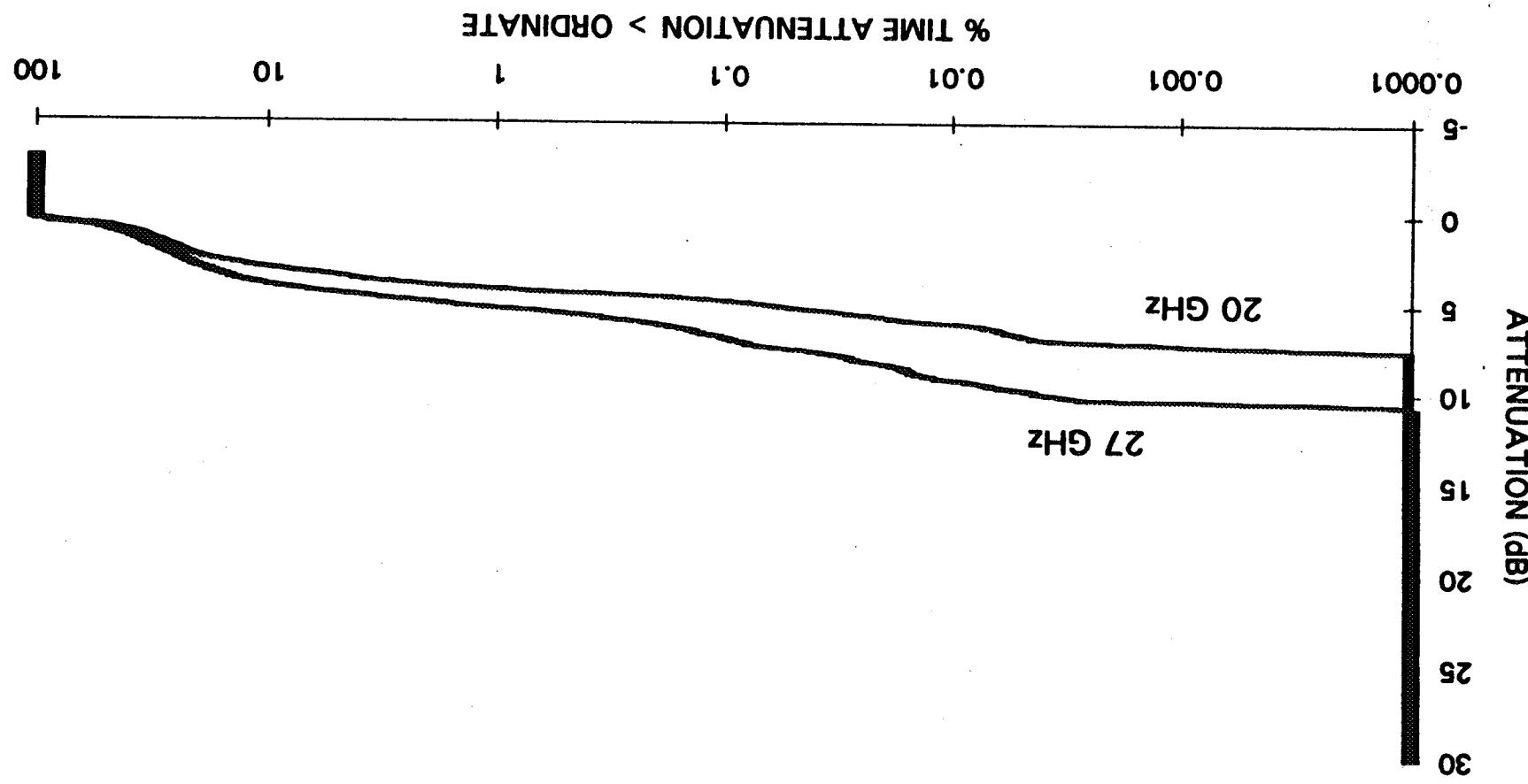


Fig. 11: Cumulative distribution functions of the 20 and 27 GHz  
radiometer-derived attenuation for the month of January, 1994



JAN 1994 - 20 GHz AND 27 GHz RADIOMETER - BC

**MAR 1994 - 20 GHz AND 27 GHz BEACON - BC**

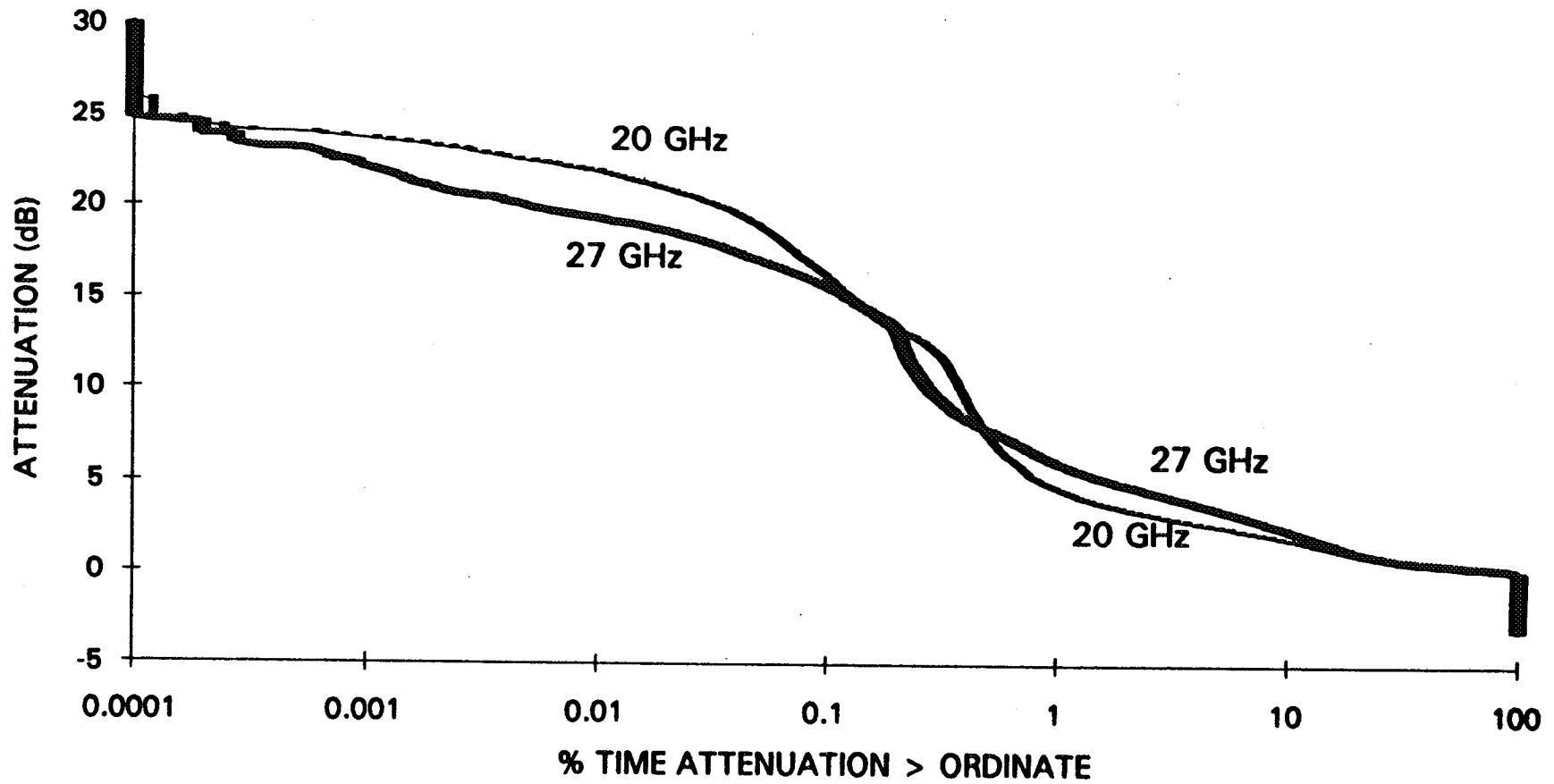
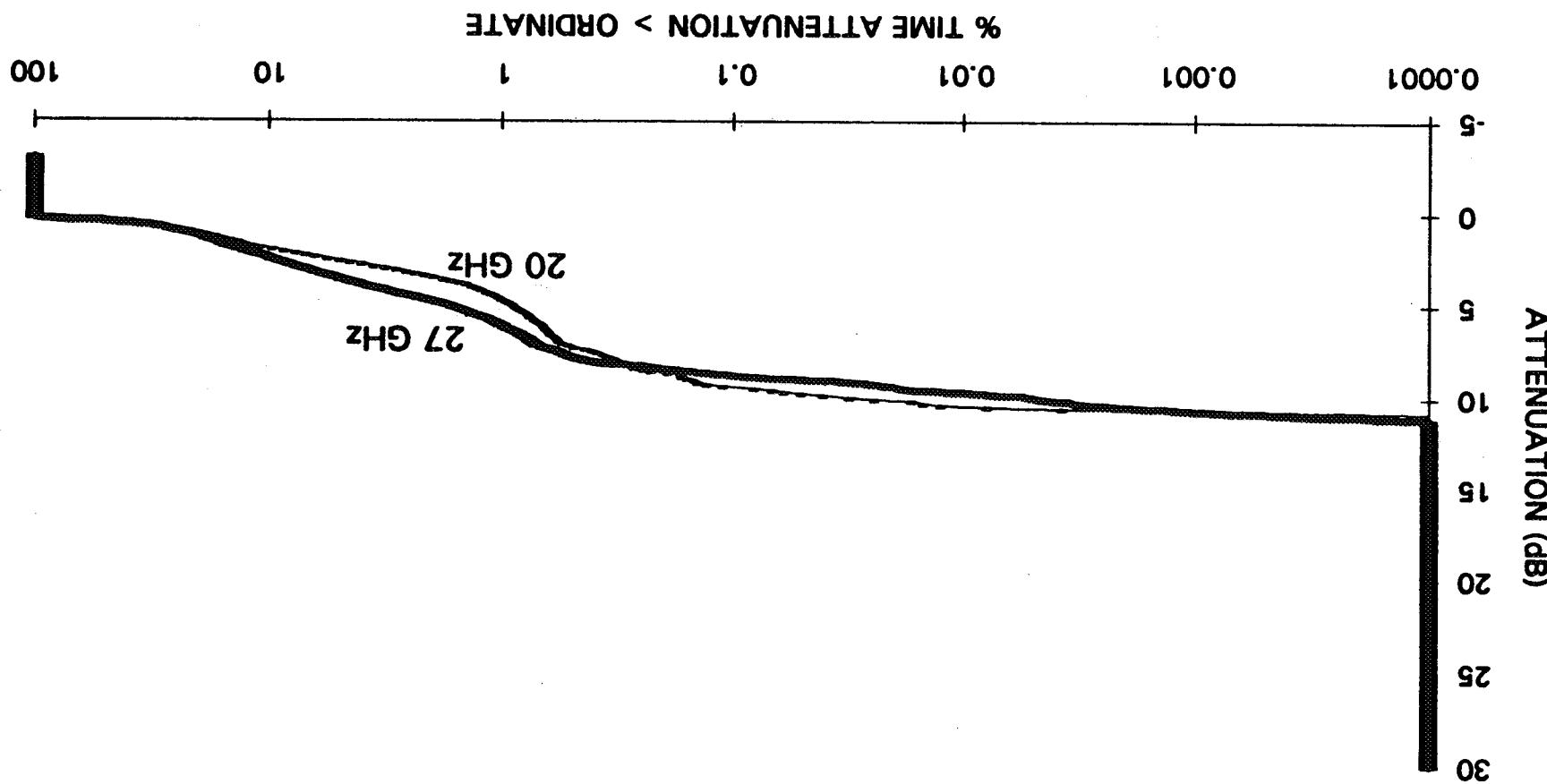


Fig. 12: Cumulative distribution functions of the 20 and 27 GHz beacon-derived attenuation for the month of March, 1994

Fig. 13: Cumulative distribution functions of the 20 and 27 GHz  
radiometer-derived attenuation for the month of March, 1994



MAR 1994 - 20 GHz AND 27 GHz RADIOMETER - BC

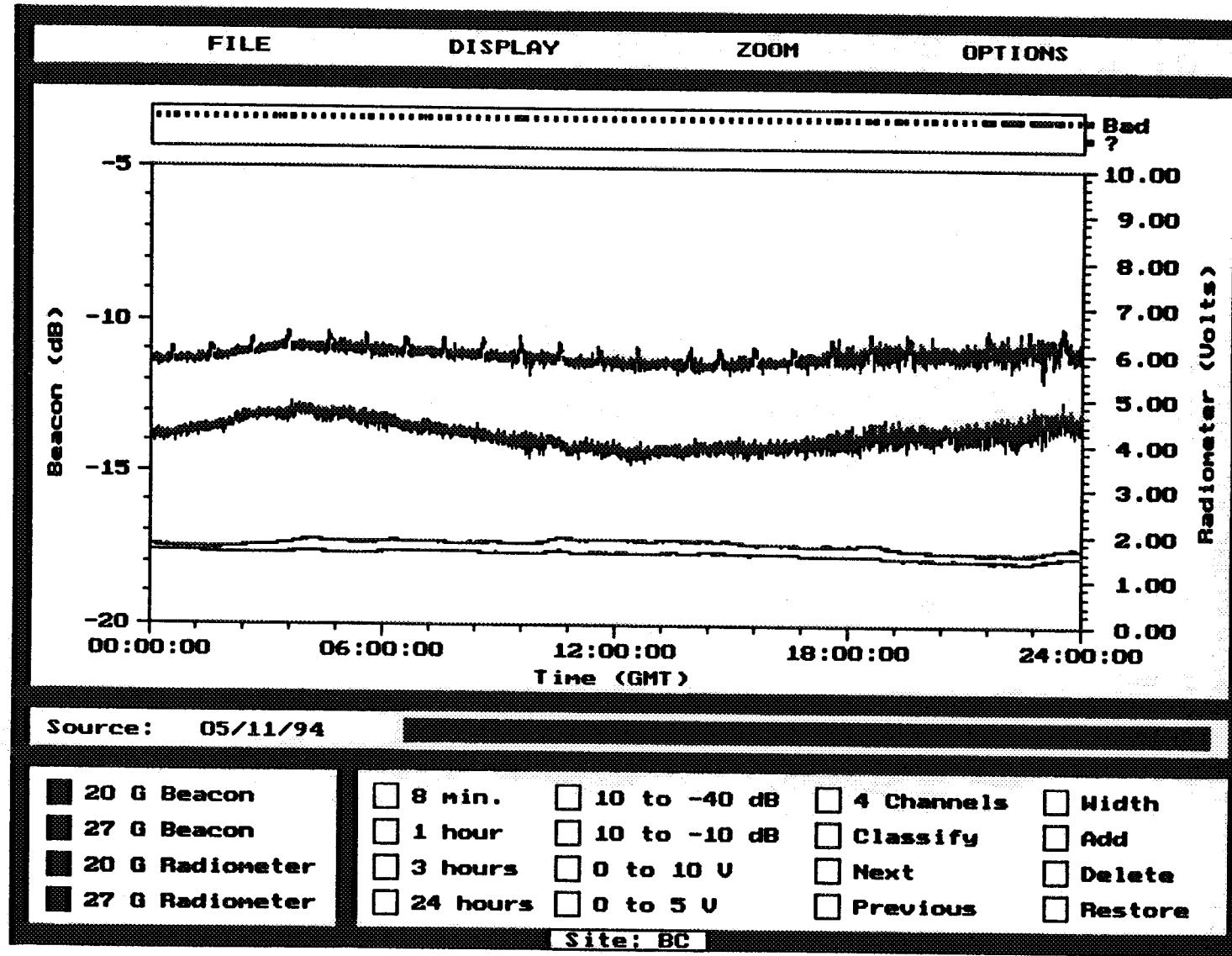


Fig. 14: Clear air scintillation on May 11, 1994

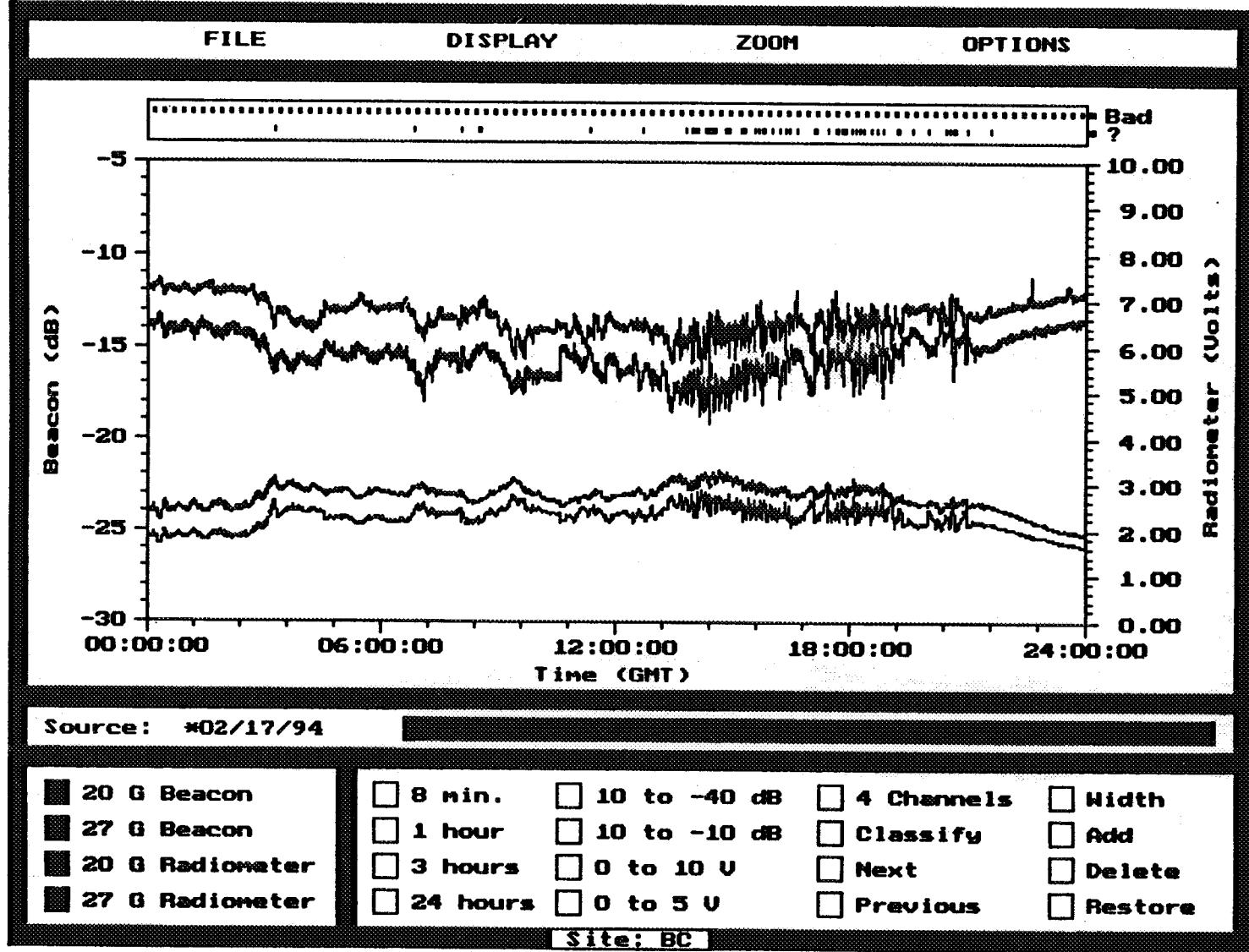


Fig. 15: Rainy weather scintillation on February 17, 1994

**Ka-band Propagation Measurements  
Using the ACTS Propagation Terminal  
and the CSU-CHILL Multiparameter Radar**

**Experimenters**

Colorado State University  
Department of Electrical Engineering  
Ft. Collins, CO 80523

**Investigators**

V.N. Bringi, Professor  
John Beaver, Ph.D. Candidate  
Joseph Turk, Research Associate

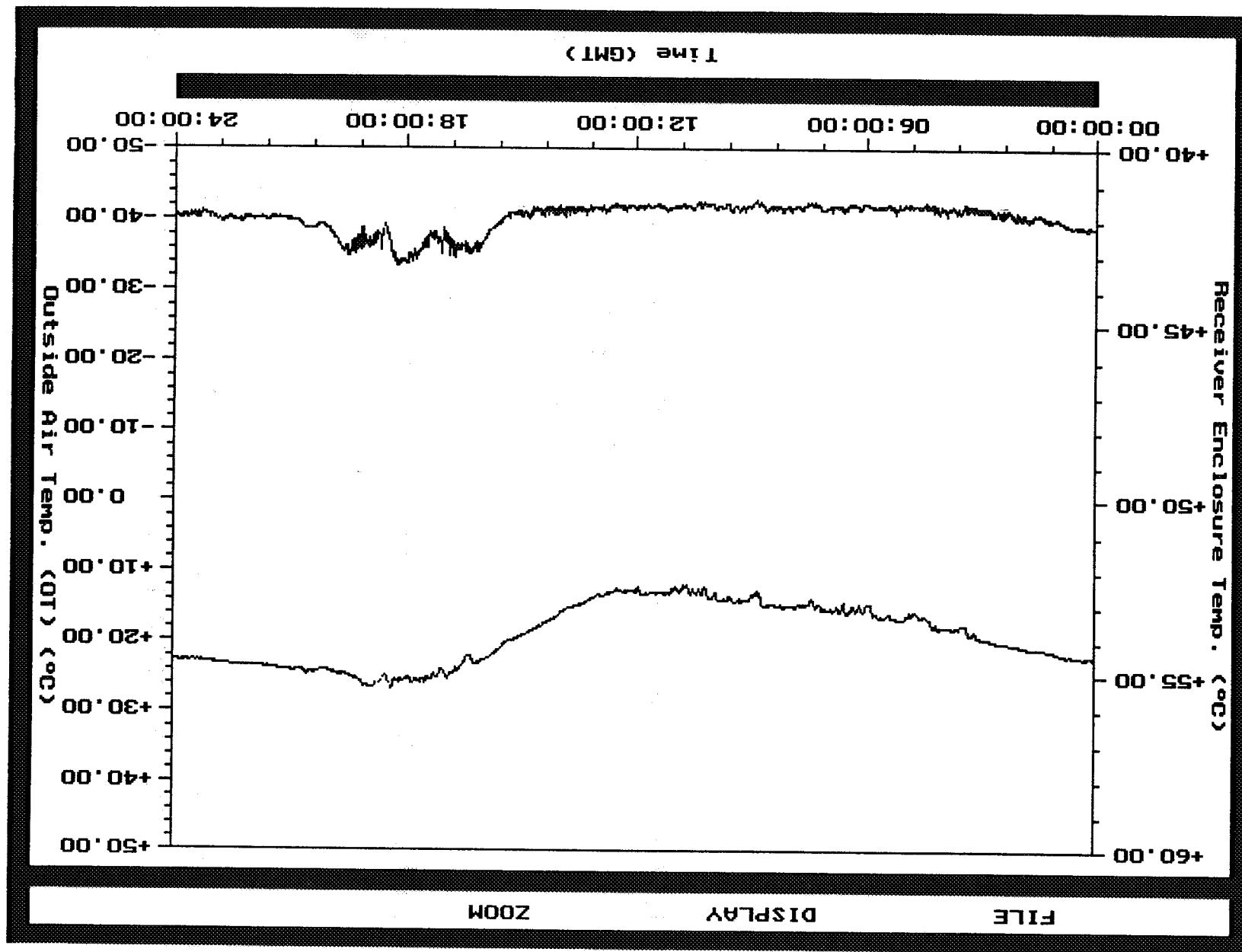
**ACTS Propagation Studies Mini-Workshop  
June 16, 1994**

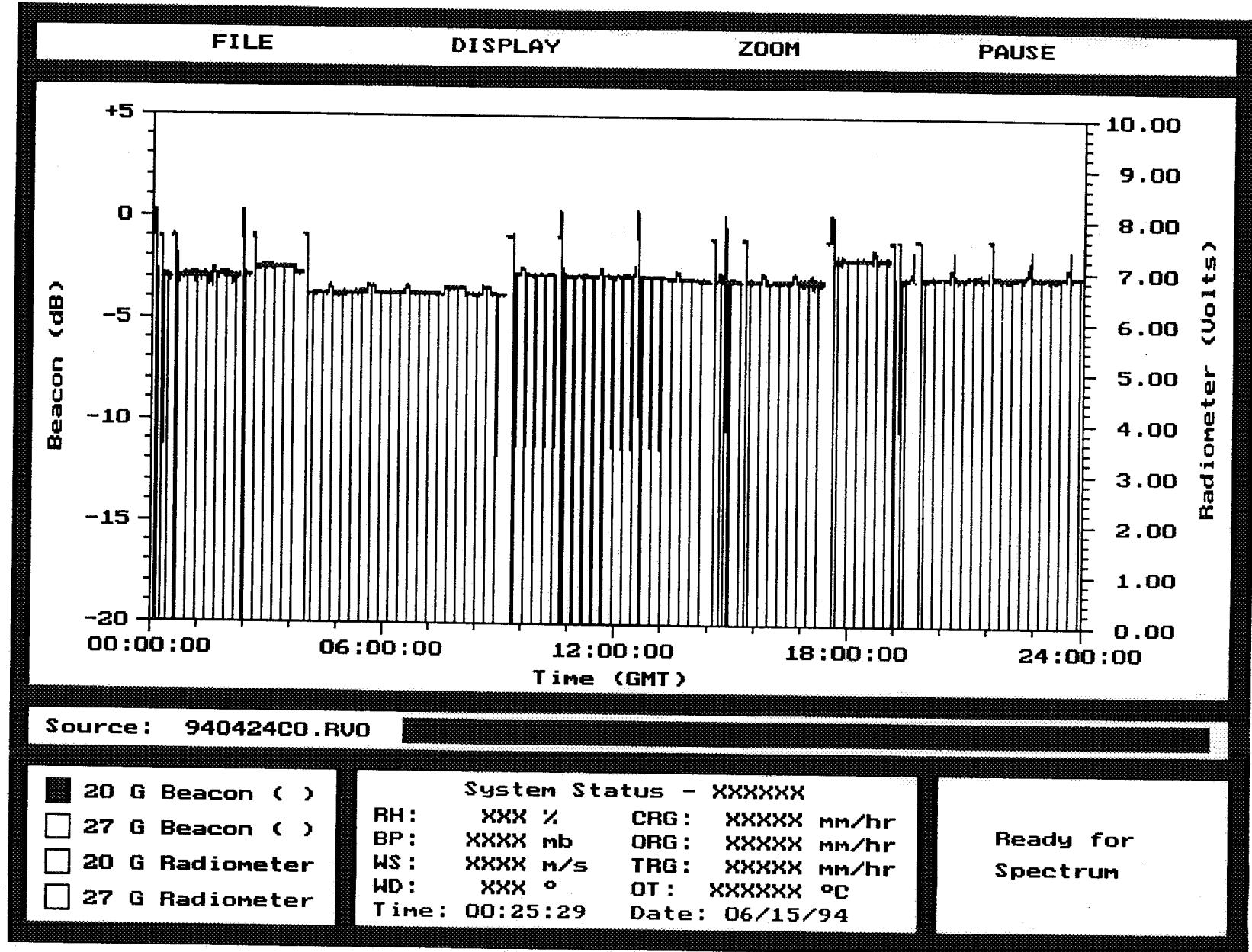
## **Outline**

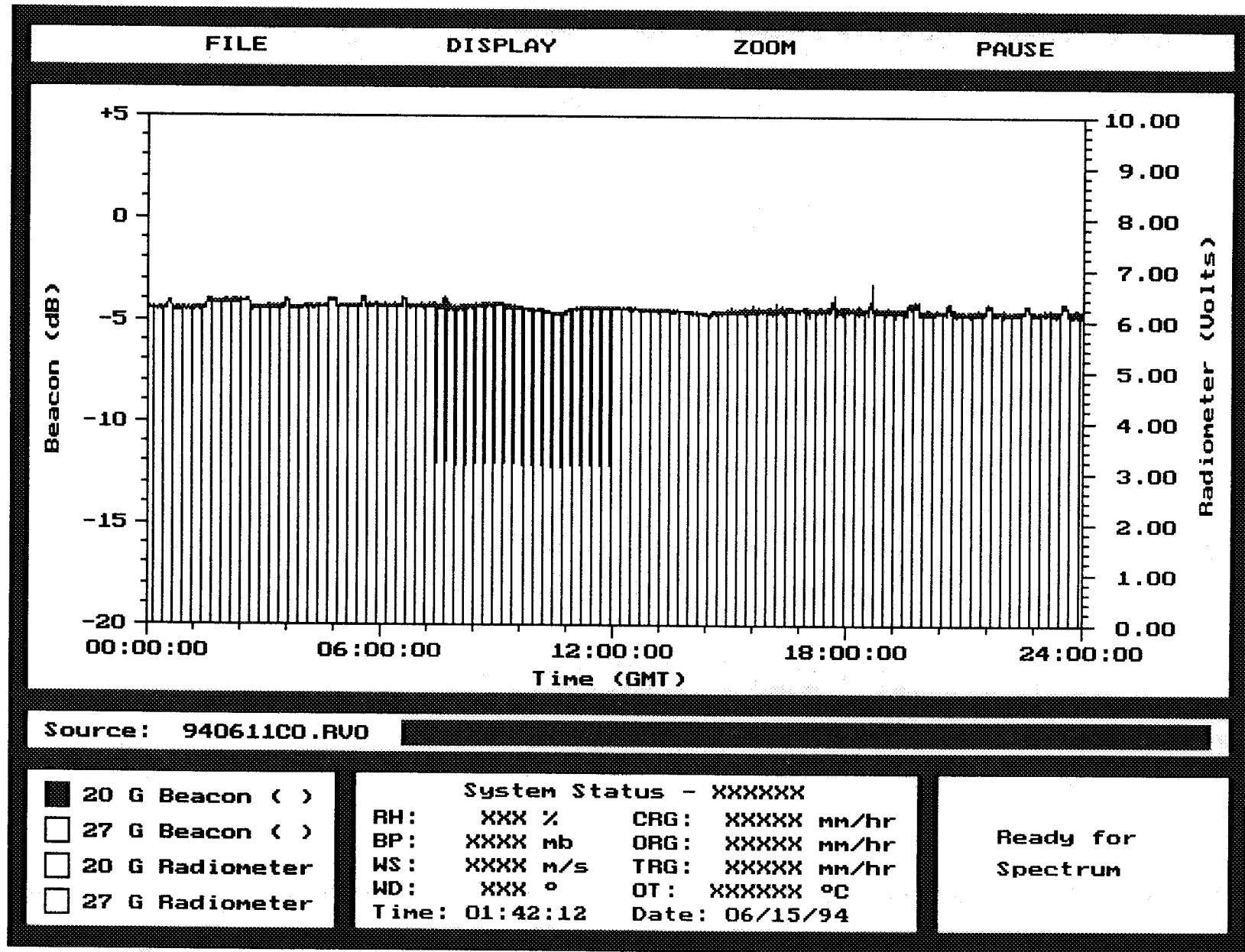
- CSU – ACTS Propagation Terminal Status
  - Hardware Problems and Solutions
  - Software Discussion
- ACTS Propagation Measurements
  - ACTS and CSU – CHILL measurements
- Modelling Efforts

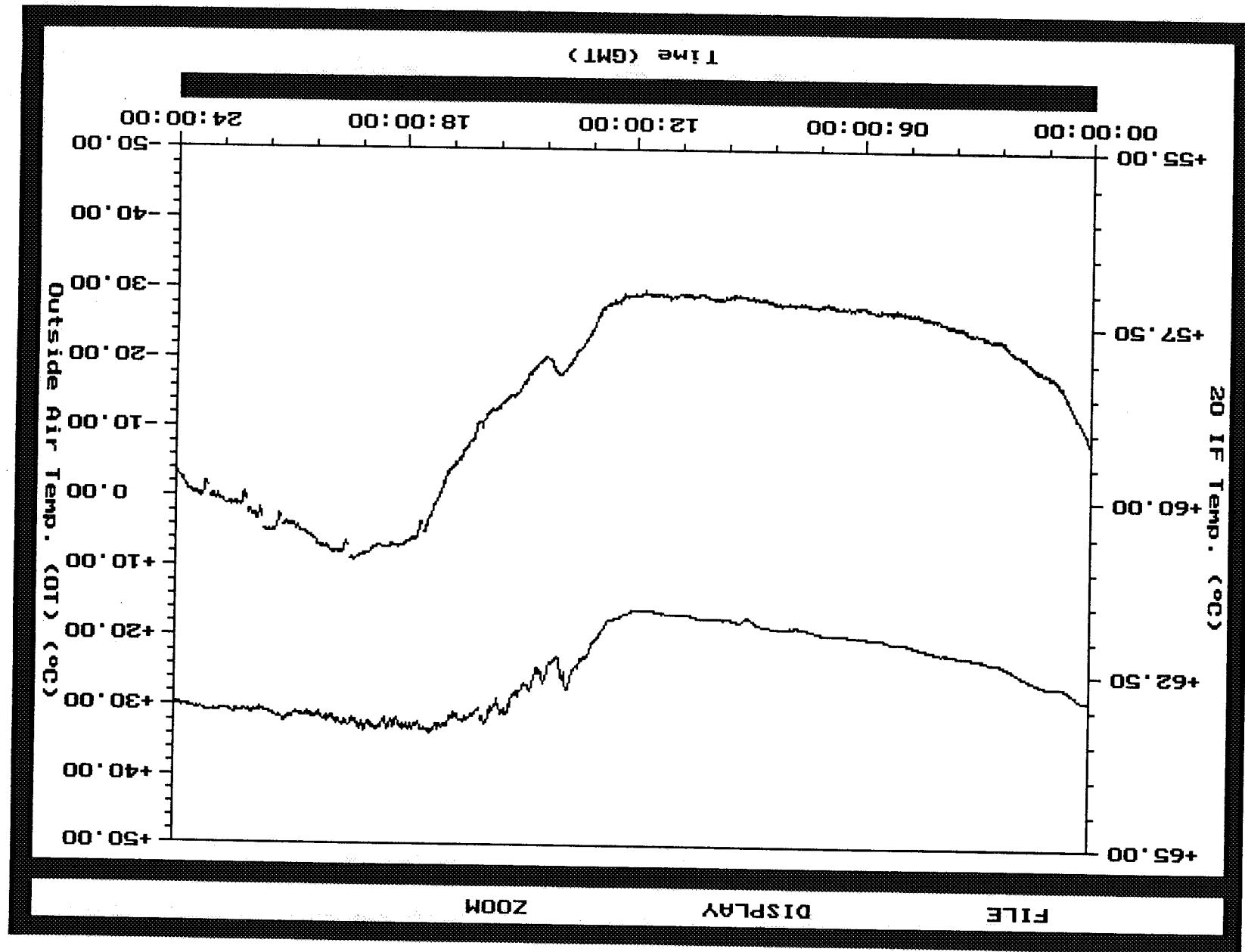
## **Hardware Problems and Solutions**

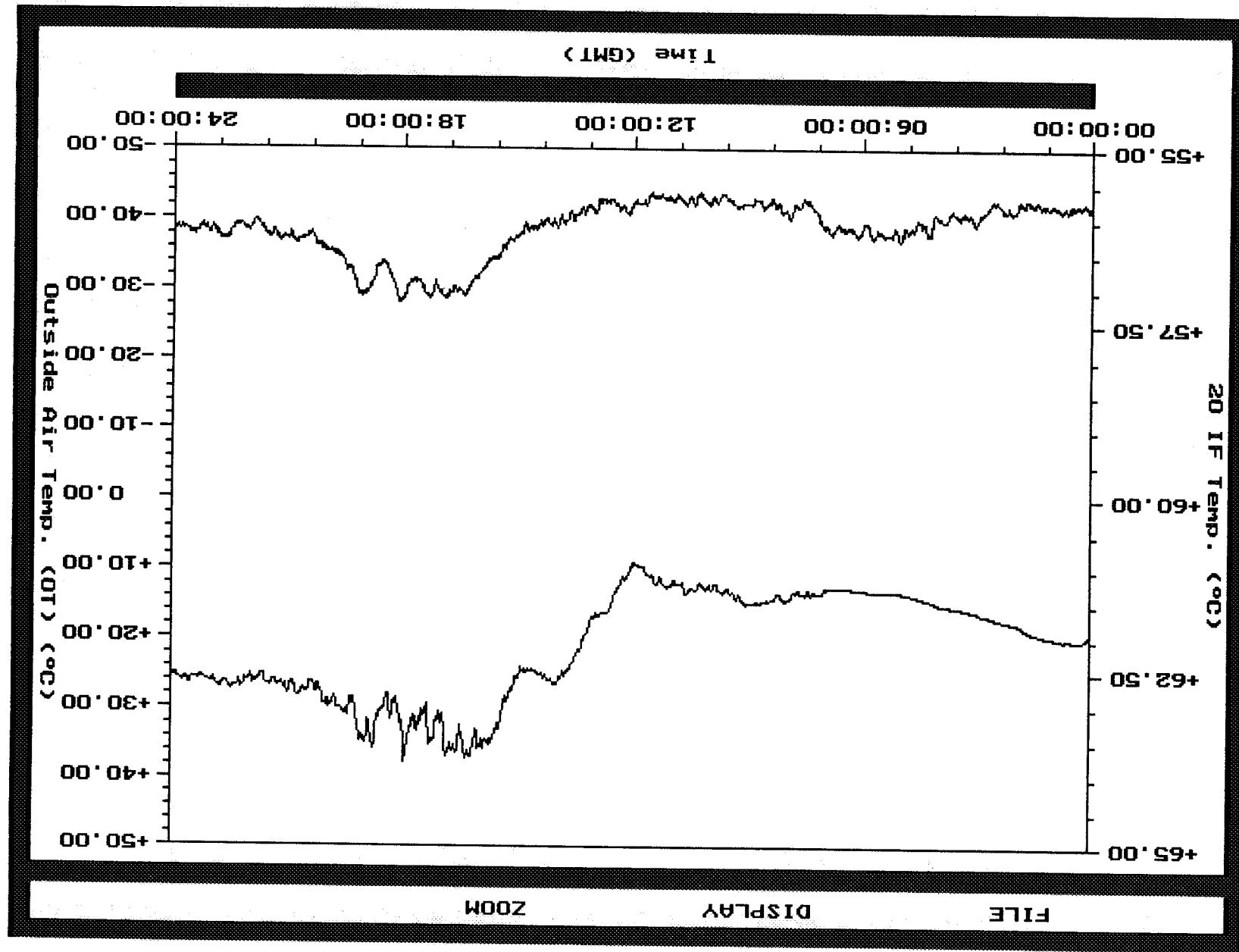
- Snow accumulation on the antenna surface
  - Installed a heating unit on the back surface of antenna
- Frequent system crashes and reboots
  - Reduced the receiver enclosure temperature to 40° Celcius
- Loss of 27GHz beacon signal
  - Lost lock on February 28, 1994.
  - After retuning the Master Oscillator, reacquired signal on March 4.

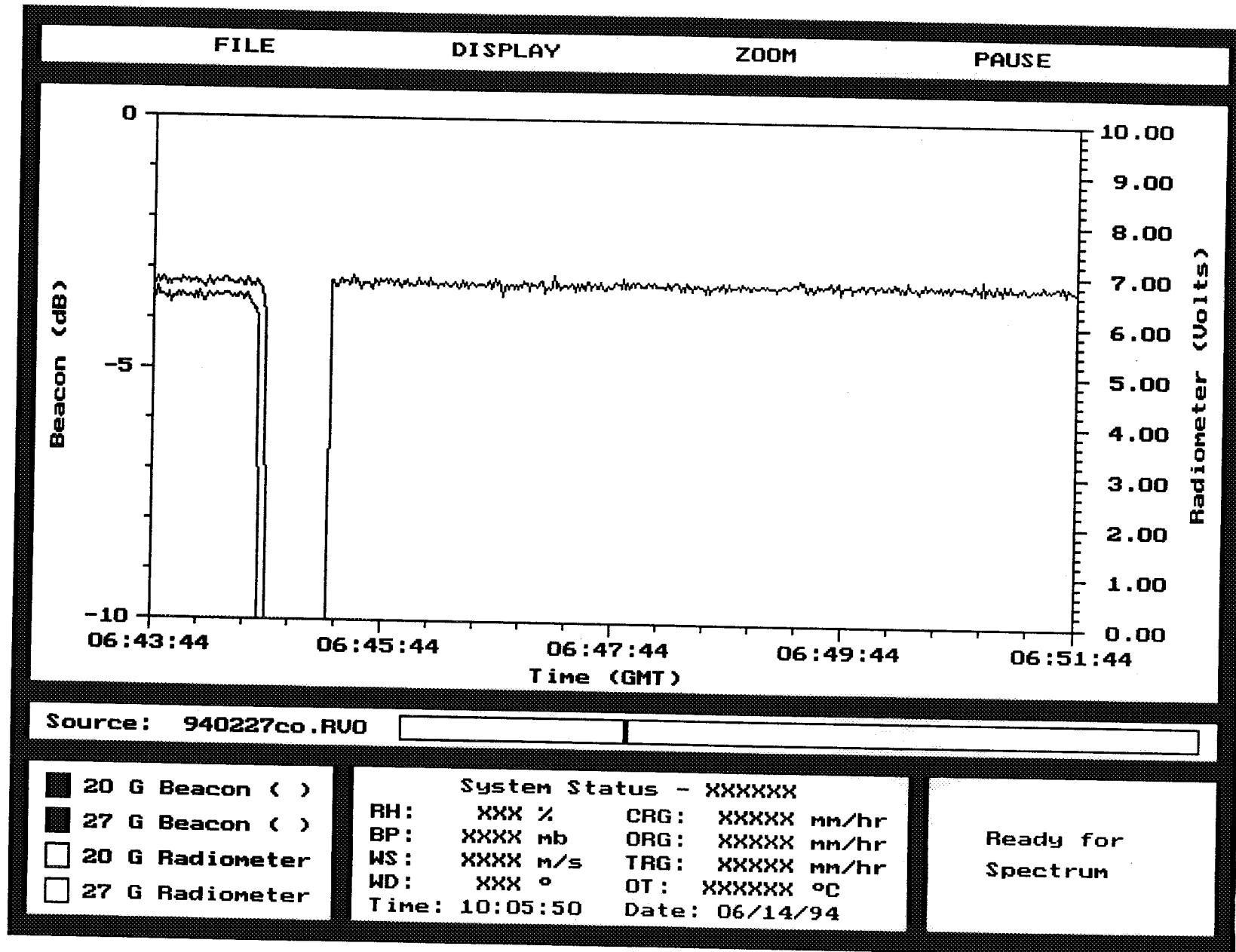




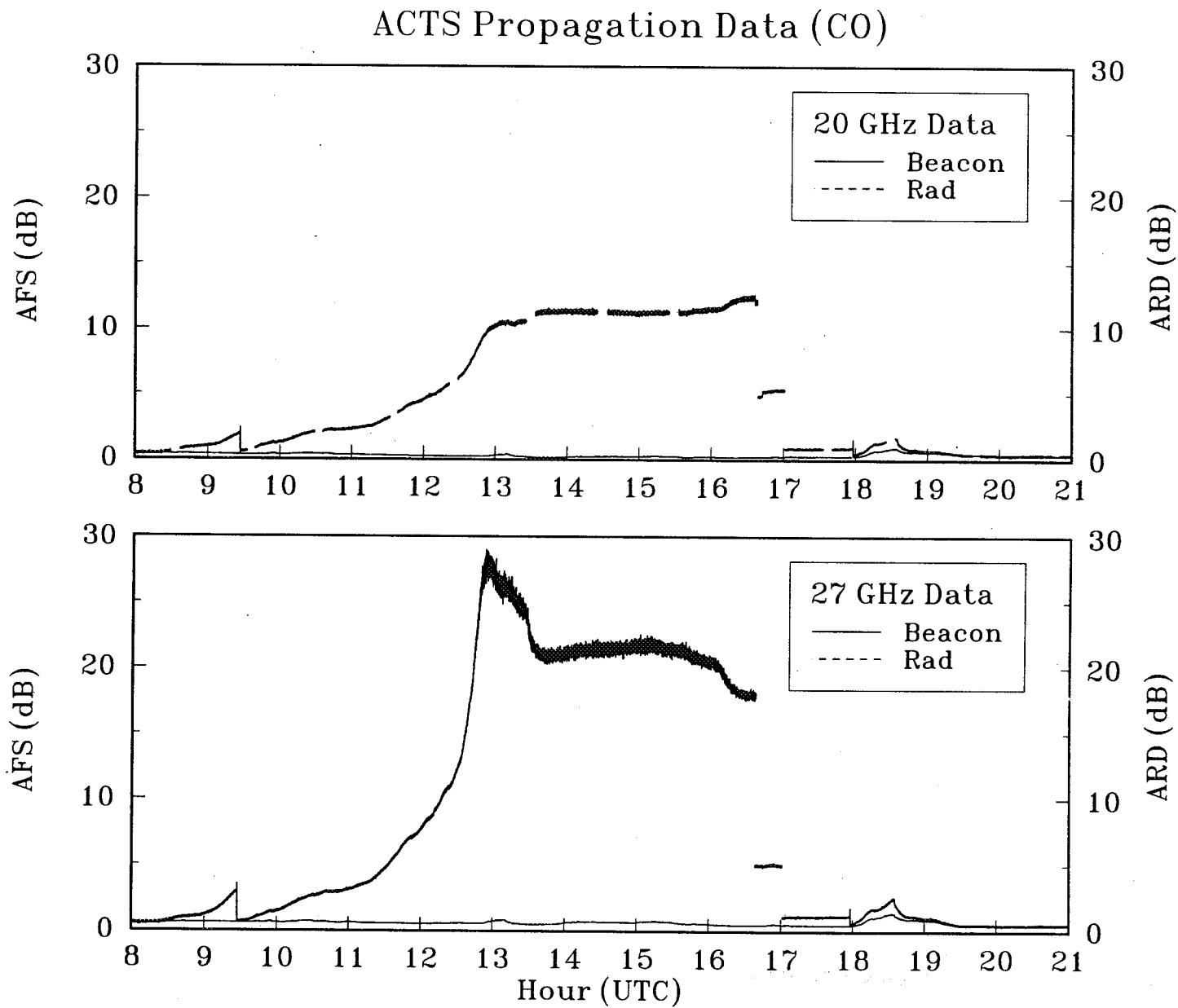




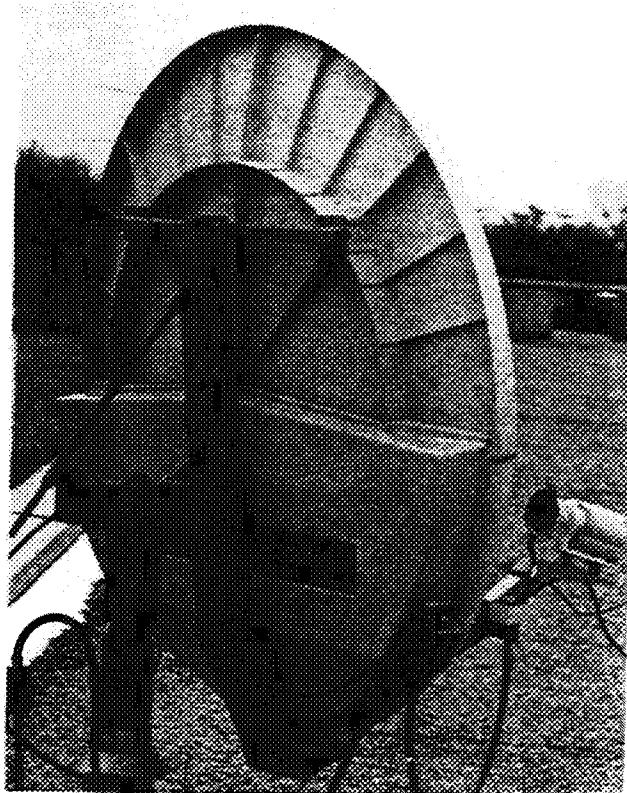




# Snow Accumulation on Antenna Surface



For Prodelin 1.2m, 1.8m  
and 2.4m Earth Stations



Model RAD-P18H-1-S-53 mounted on Prodelin 1.8m Reflector

### Self-Regulating Performance

The polymer heater element used in SoftHeat Radiant Anti-Icing Systems is self regulating, allowing the thermal power delivered to the antenna to vary depending on the environmental conditions the antenna experiences: as ambient temperature decreases, heat output increases.

### Radiant Heating Simplicity

Radiant heat transfer, as applied to antenna anti-icing, provides special benefits due to its inherent uniformity. Furthermore, SoftHeat Radiant systems respond differently to varying heat transfer conditions across the reflector surface, so that no mechanical means are required for even heat distribution. Thus the system has no moving parts other than controller contacts.

### Ease of Installation

The SoftHeat Radiant Anti-Icing System is designed for quick and simple installation. It is complete and ready for installation

The SoftHeat Radiant Anti-Icing System family comprises models for the Prodelin 1.2m, 1.8m, and 2.4m reflectors. Field installation is simple, making them ideal for either initial installation or subsequent retrofit applications. Through the use of self-regulating heating elements, sufficient thermal power is delivered to the front surface of the antenna for effective anti-icing, while the uniform radiant heat minimizes reflector distortion.

as shipped, requiring no special structural adaptations or additional framing.

### High Thermal Flux

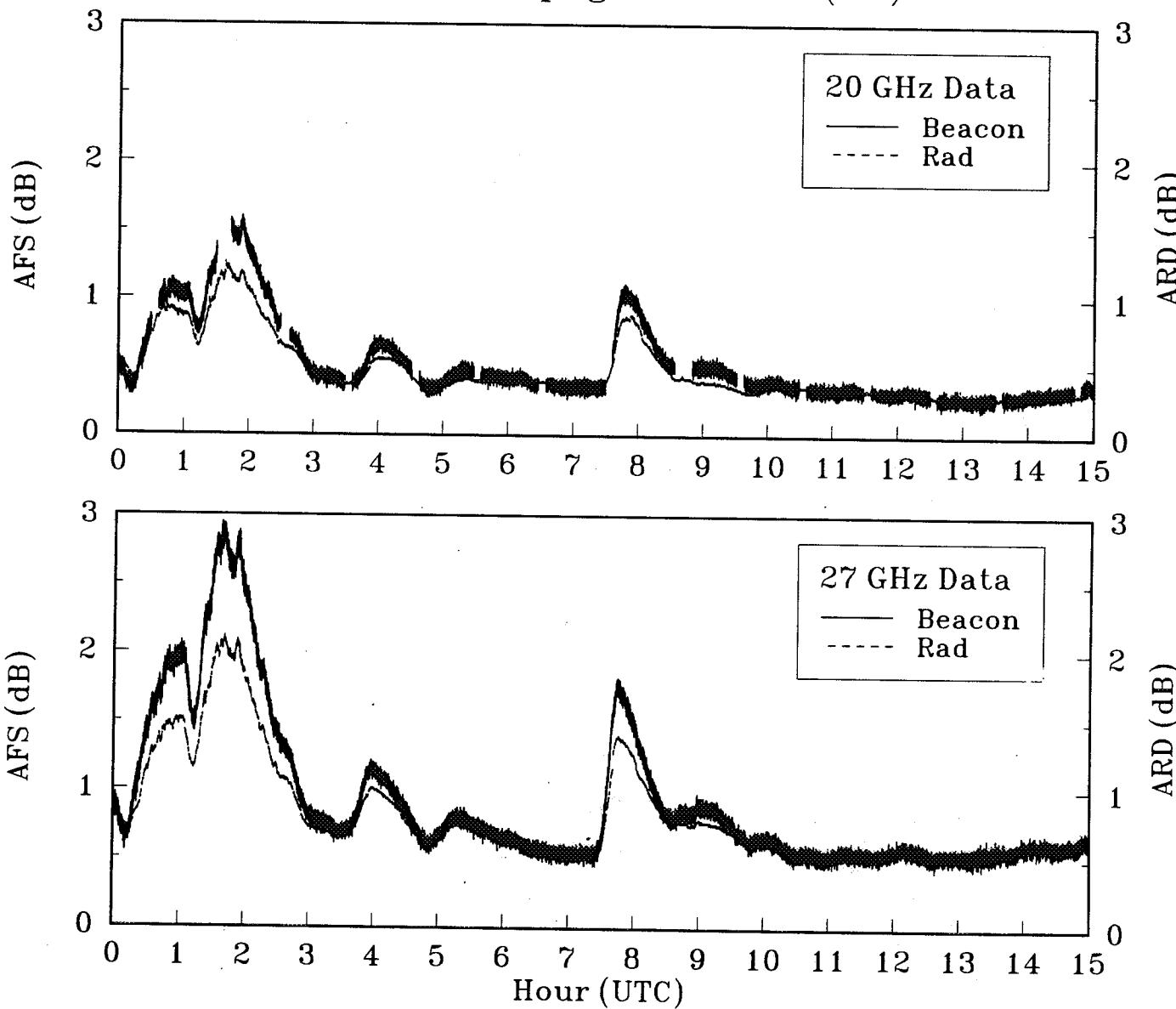
SoftHeat Radiant Anti-Icing Systems provide a high thermal flux, strongly biased **forward**, where snow and ice accumulation can cause severe signal attenuation. SoftHeat/Prodelin systems have demonstrated greater than 85% thermal efficiency toward the front of the antenna.

### Features

SoftHeat Radiant Anti-Icing Systems are designed specifically for Prodelin 1.2m, 1.8m, or 2.4m reflectors. All systems operate on 120 volt A.C.; power connection for 1.2m and 1.8m systems uses a simple plug and cord. A feedhorn heating system reduces outages from ice and snow accumulation in the critical feedhorn window. An advanced solid state moisture/temperature sensor reduces energy consumption on 1.8m and 2.4m systems.

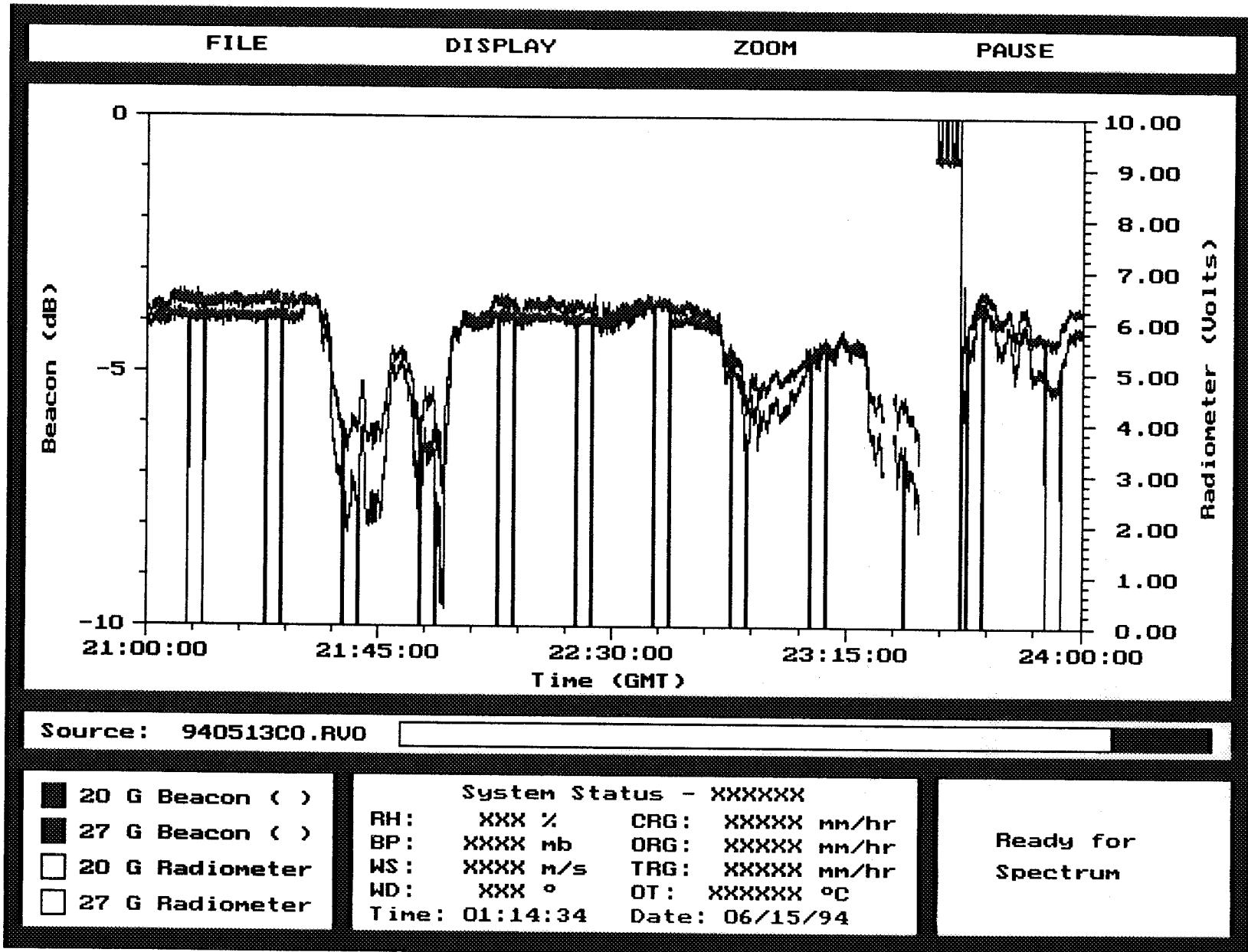
# Measured Snow Event after De-Icing Unit was Installed

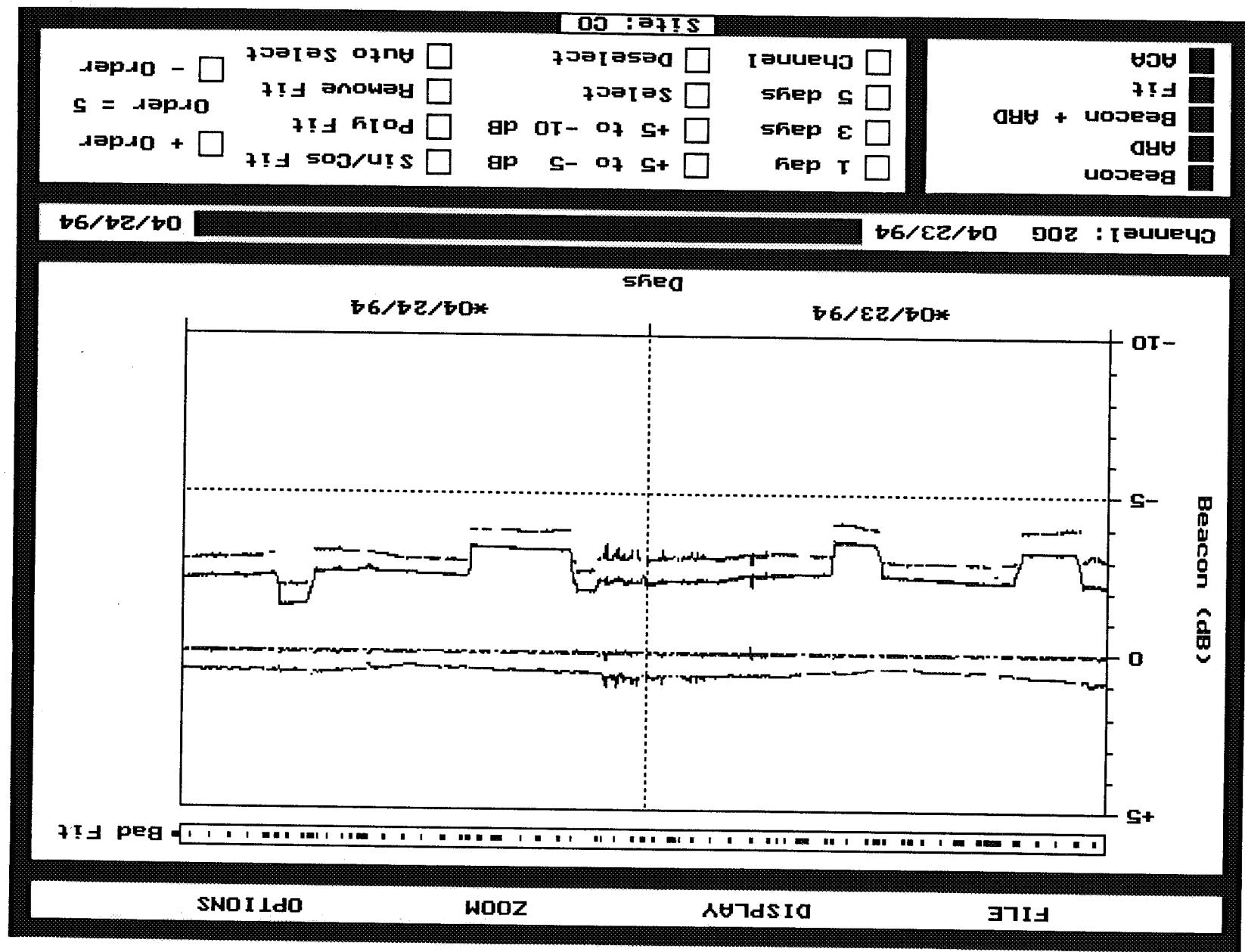
ACTS Propagation Data (CO)

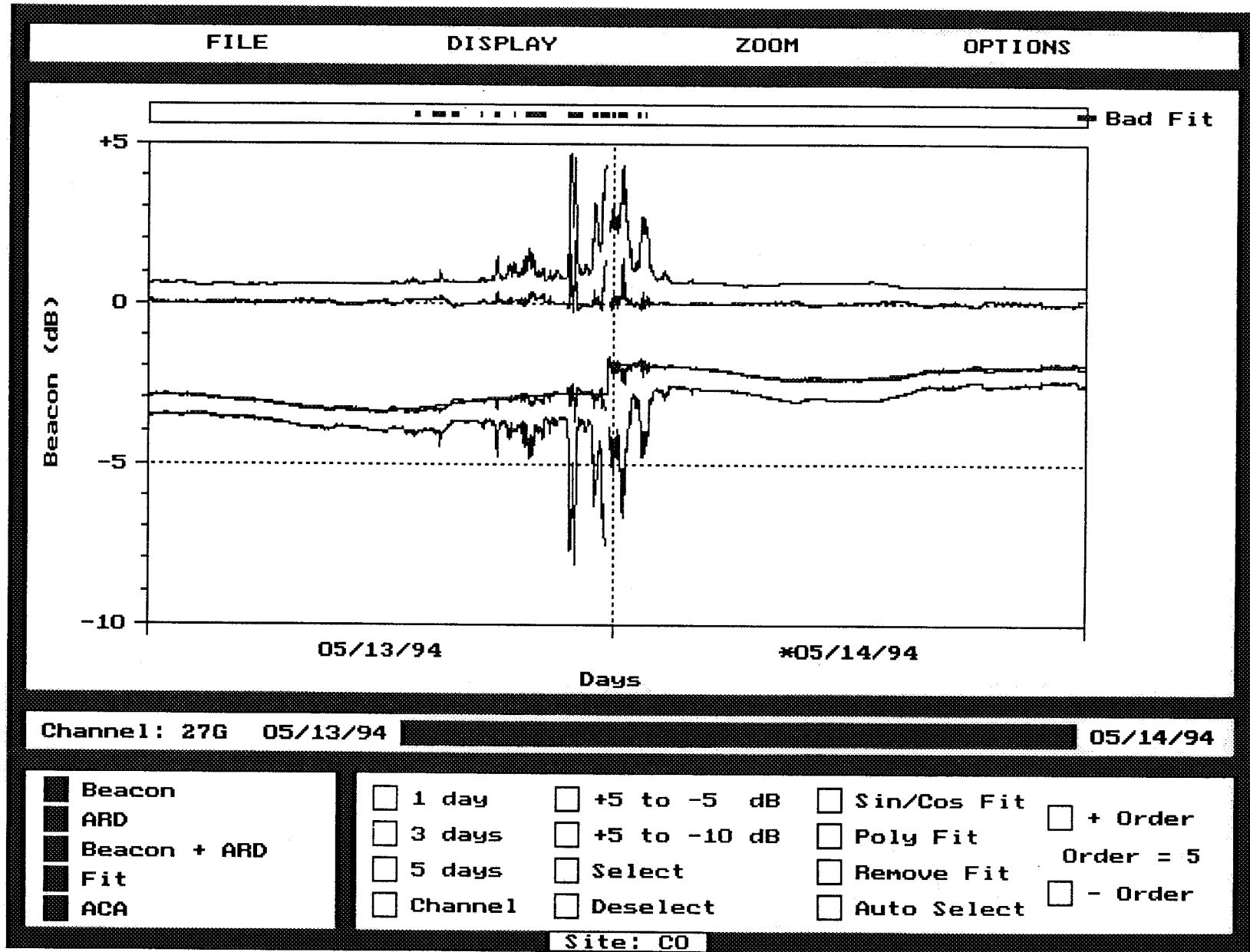


## **Software Discussion**

- Shorter set up times
- Level shifts in data after set ups
- Time axis in bias removal

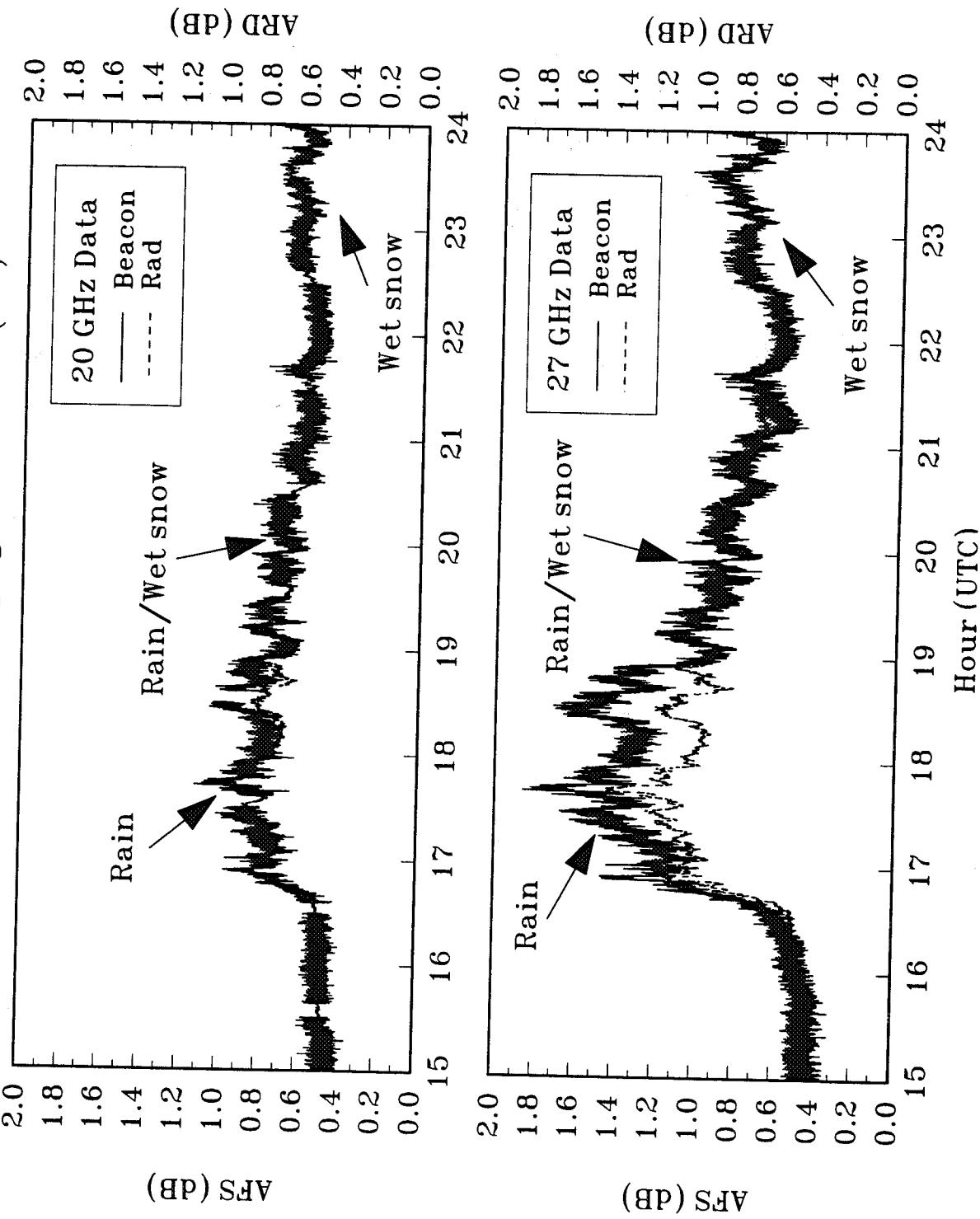






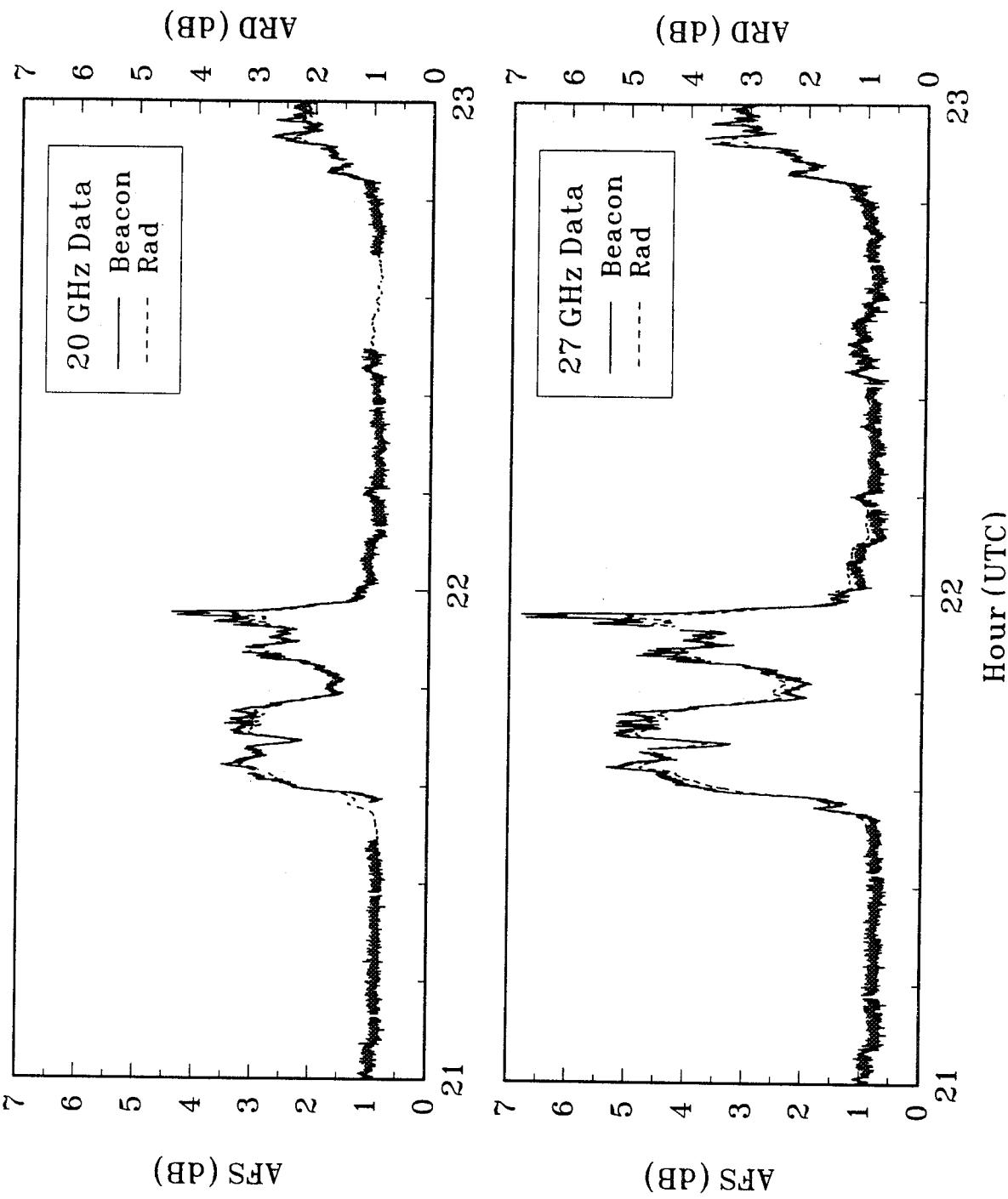
# Rain / Wet Snow Event

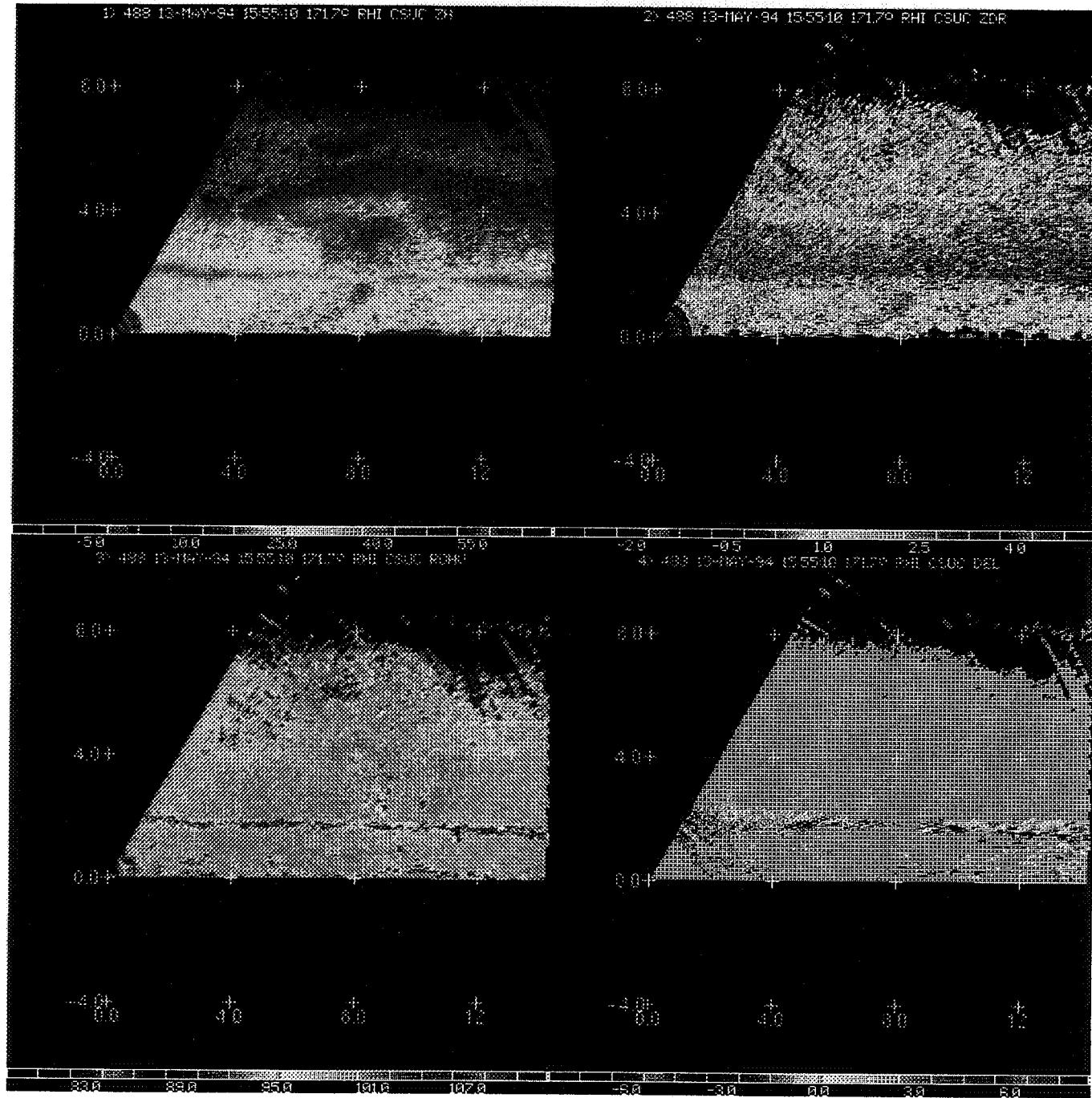
## 4/9/94 ACTS Propagation Data (CO)



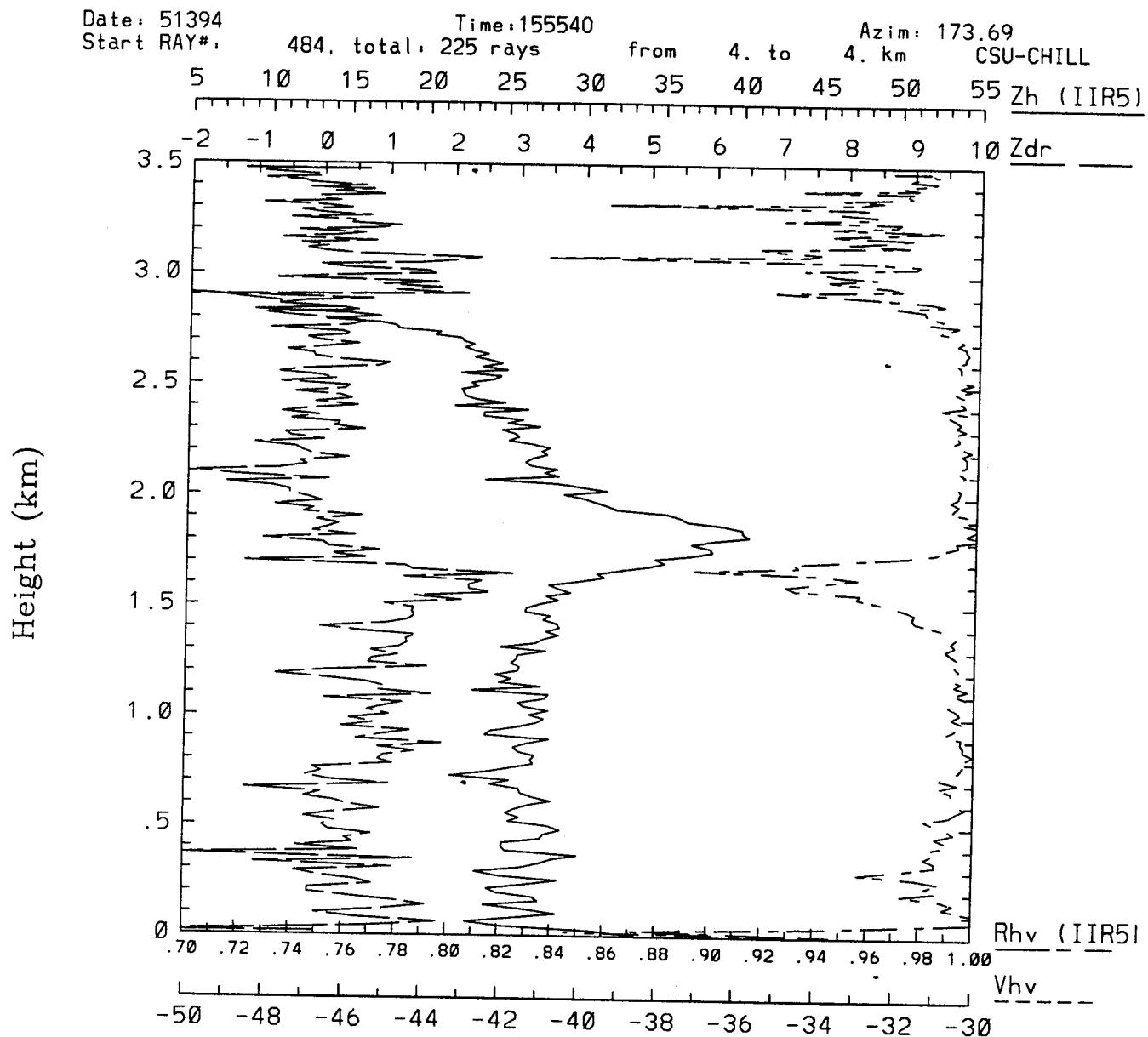
# ACTS / CSU CHILL Data (Bright Band Case)

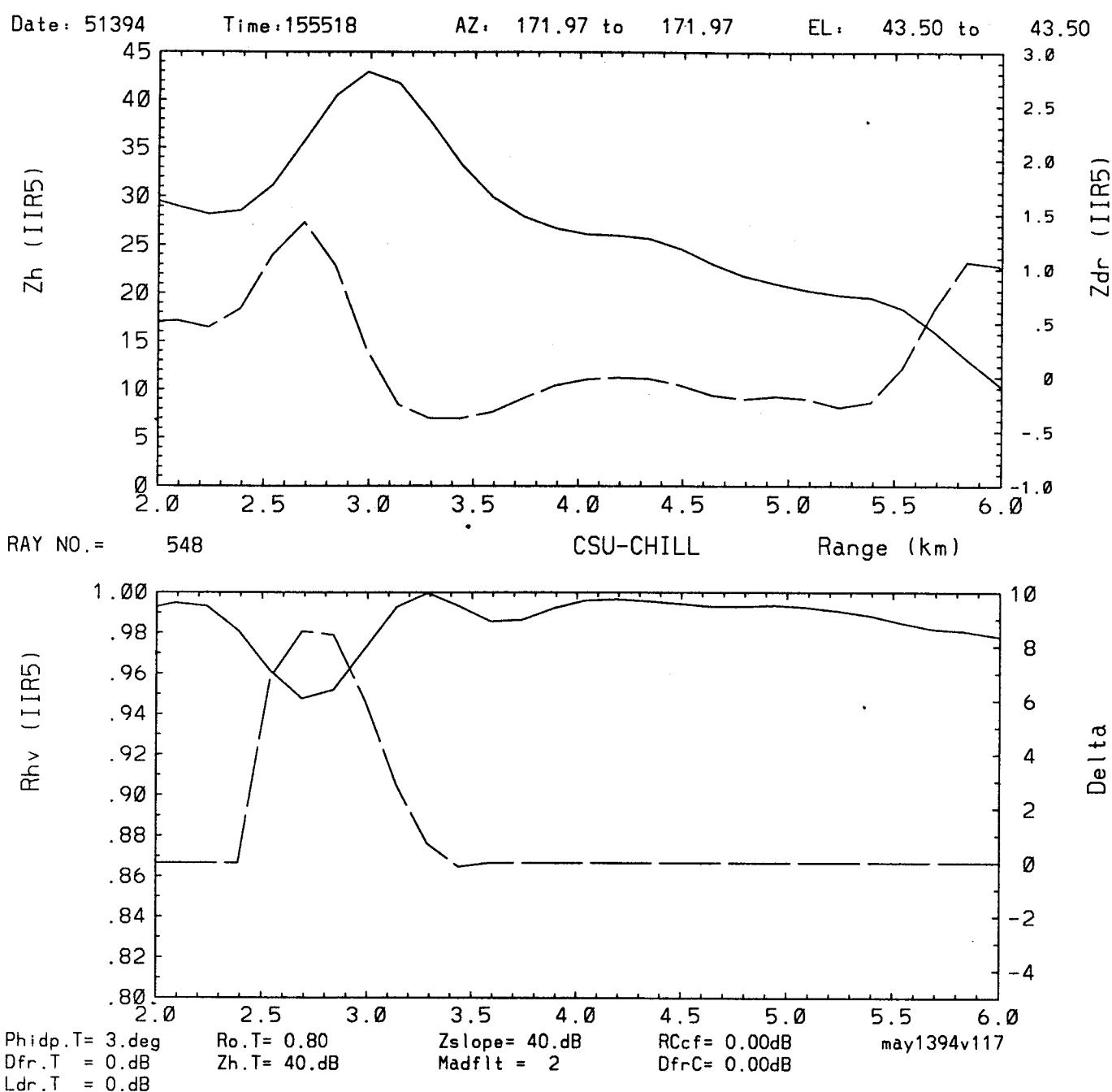
## 5/13/94 ACTS Propagation Data (CO)





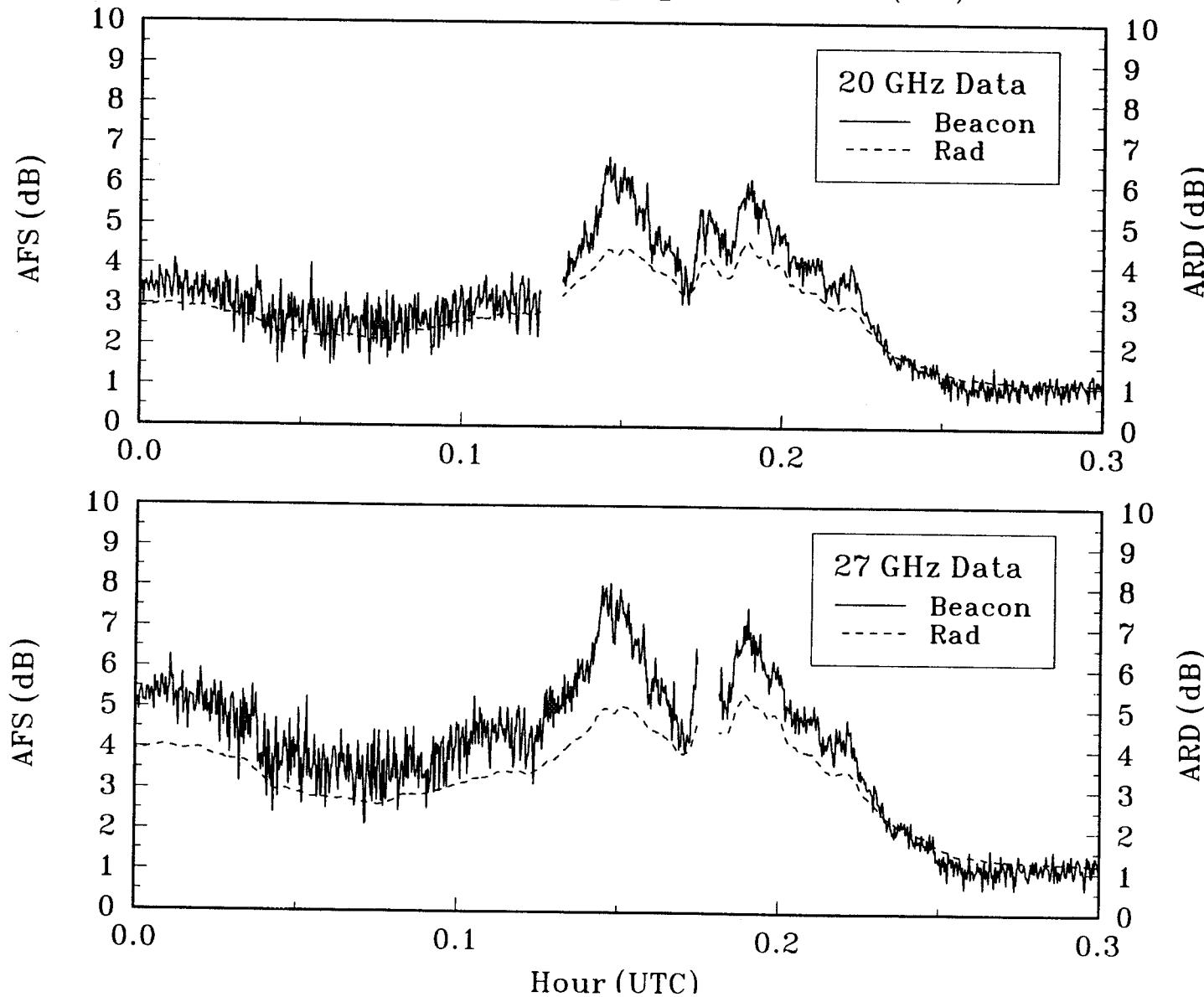






# ACTS/CSU CHILL Data (Convective Case)

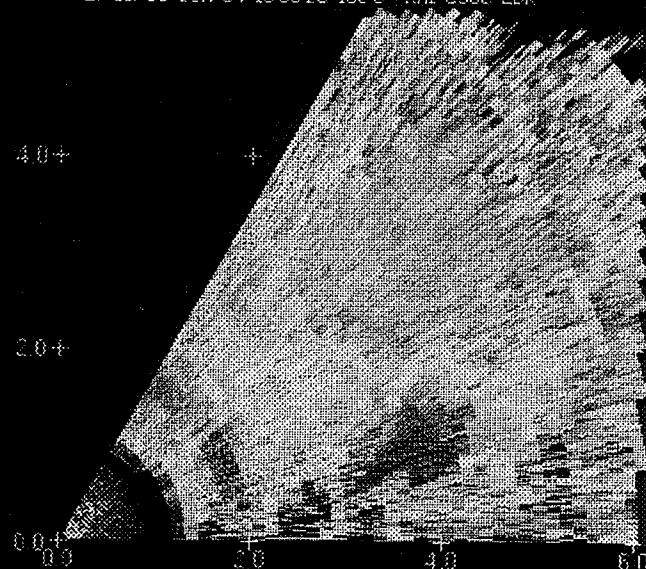
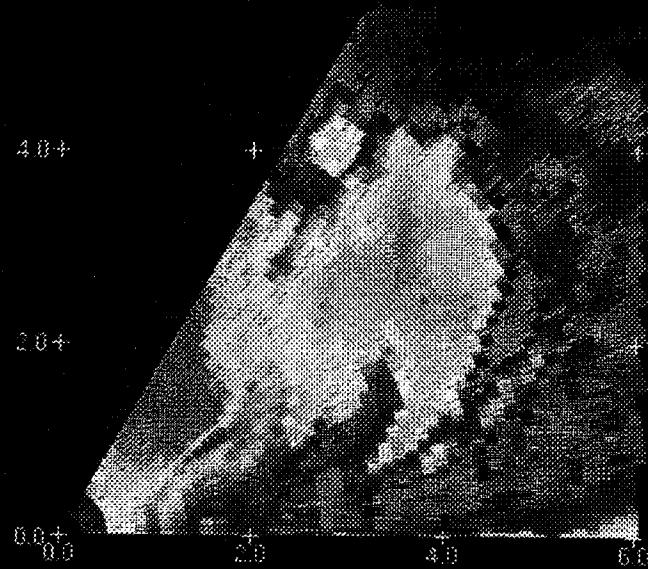
## 6/3/94 ACTS Propagation Data (CO)





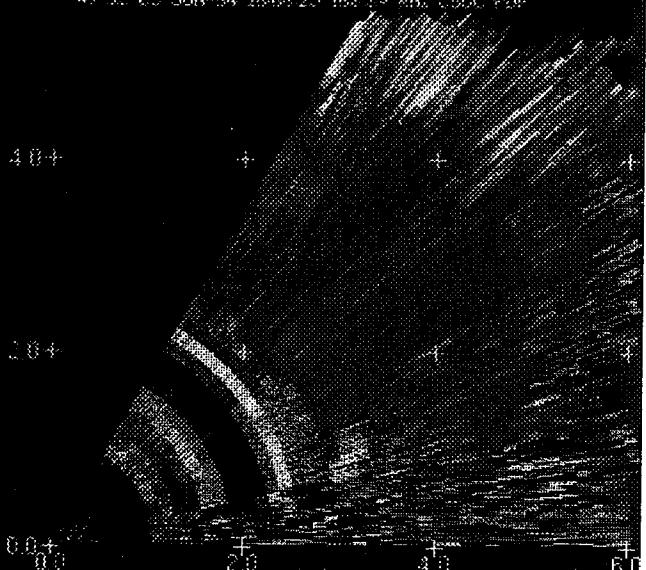
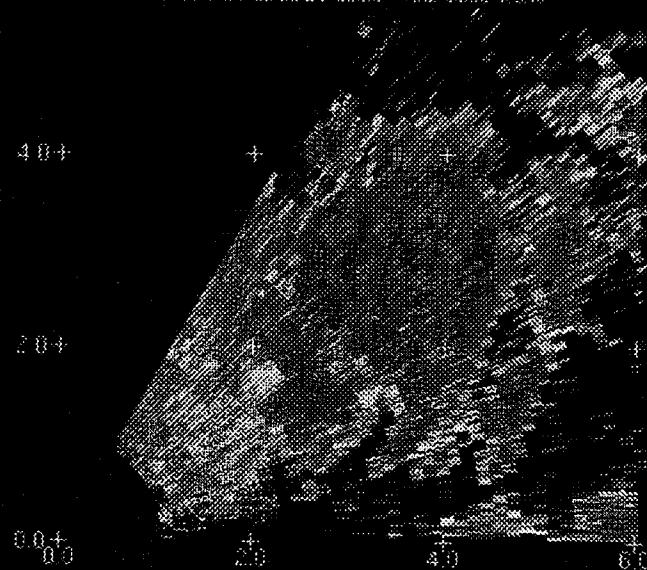
D 32 00-JUN-94 18:00:25 168.9° RHI CSUC ZH

D 32 00-JUN-94 18:00:25 168.3° RHI CSUC ZDR

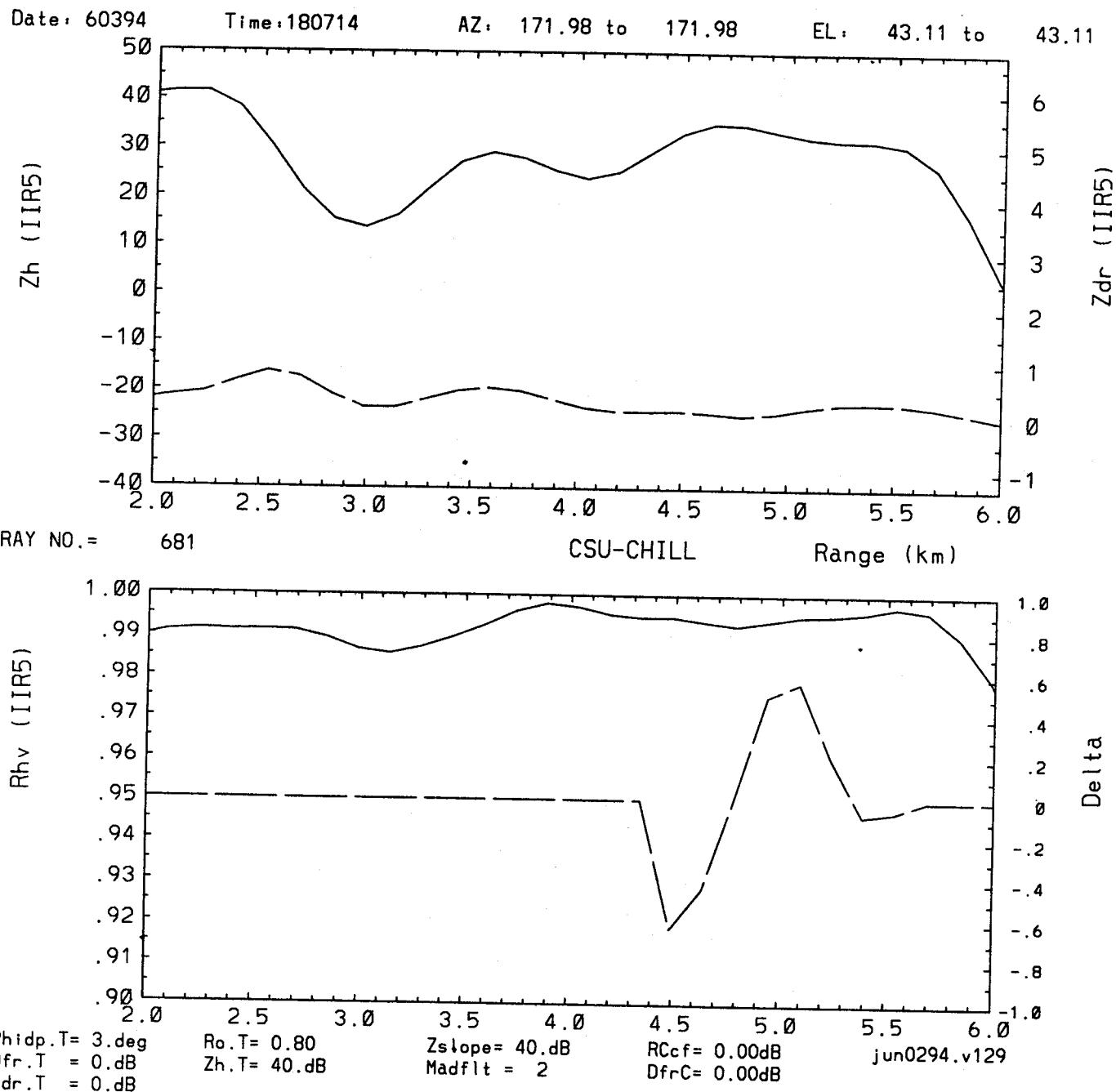


3 32 00-JUN-94 18:00:25 168.9° RHI CSUC PDP

3 32 00-JUN-94 18:00:25 168.3° RHI CSUC PDP

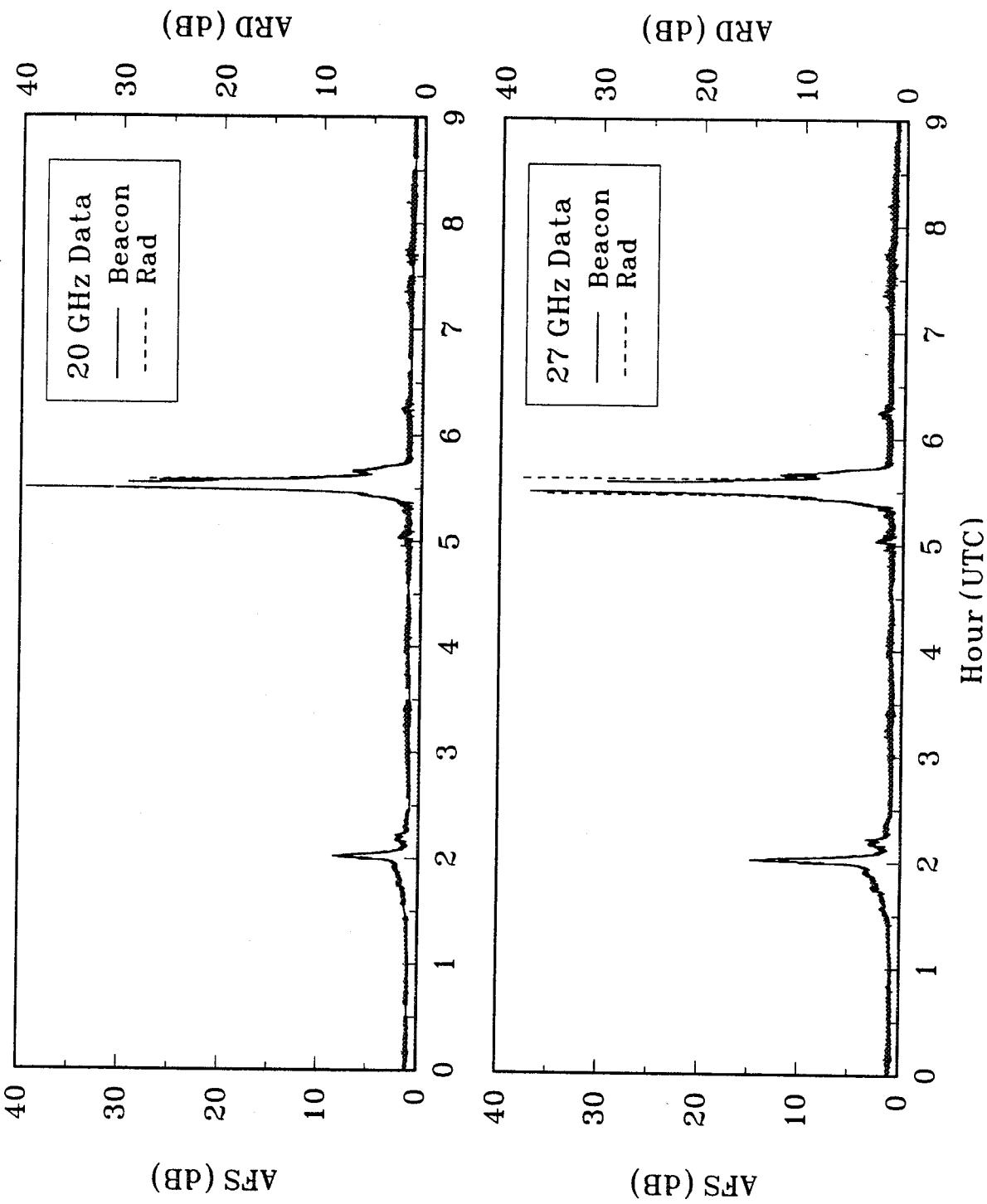


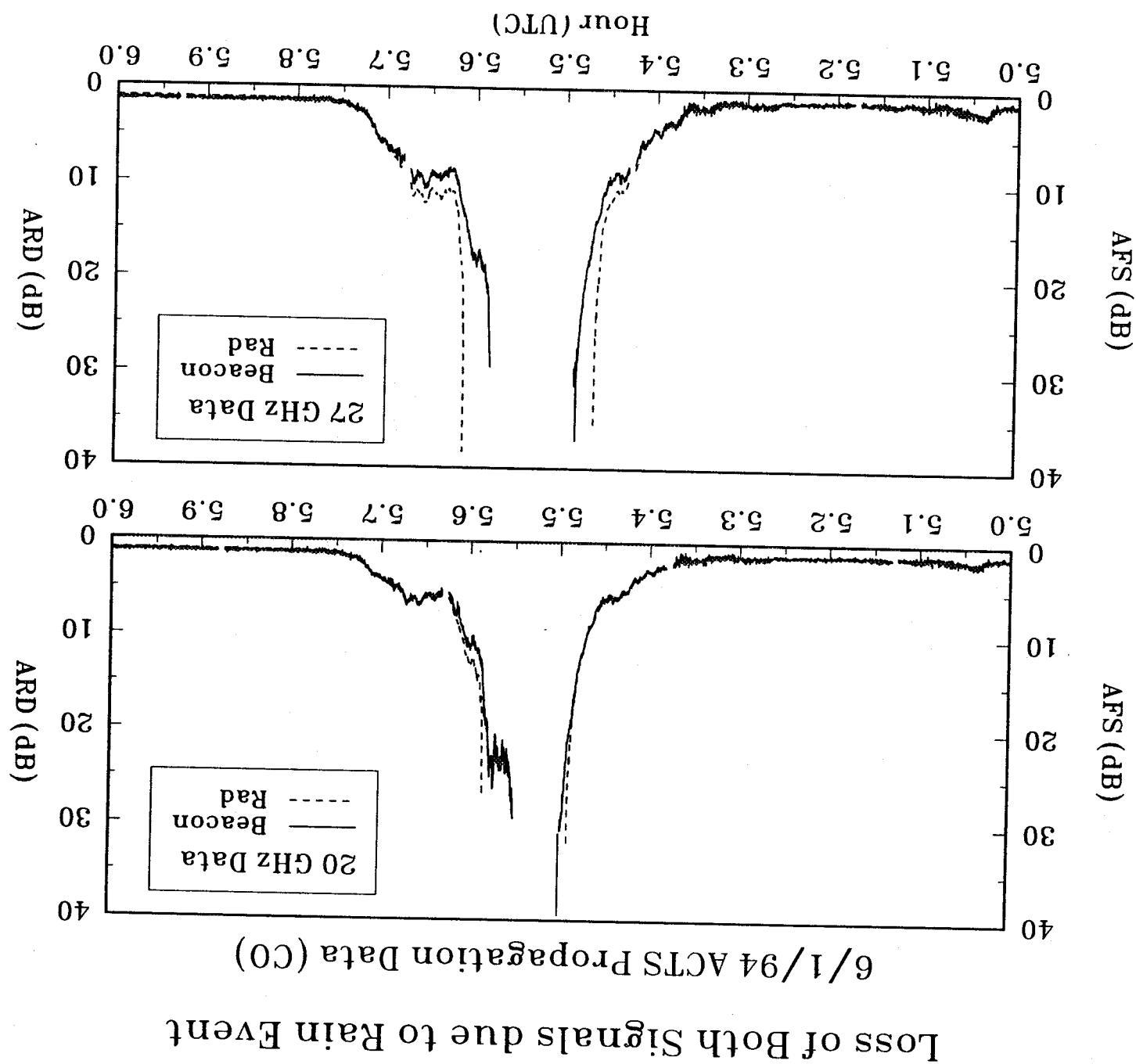




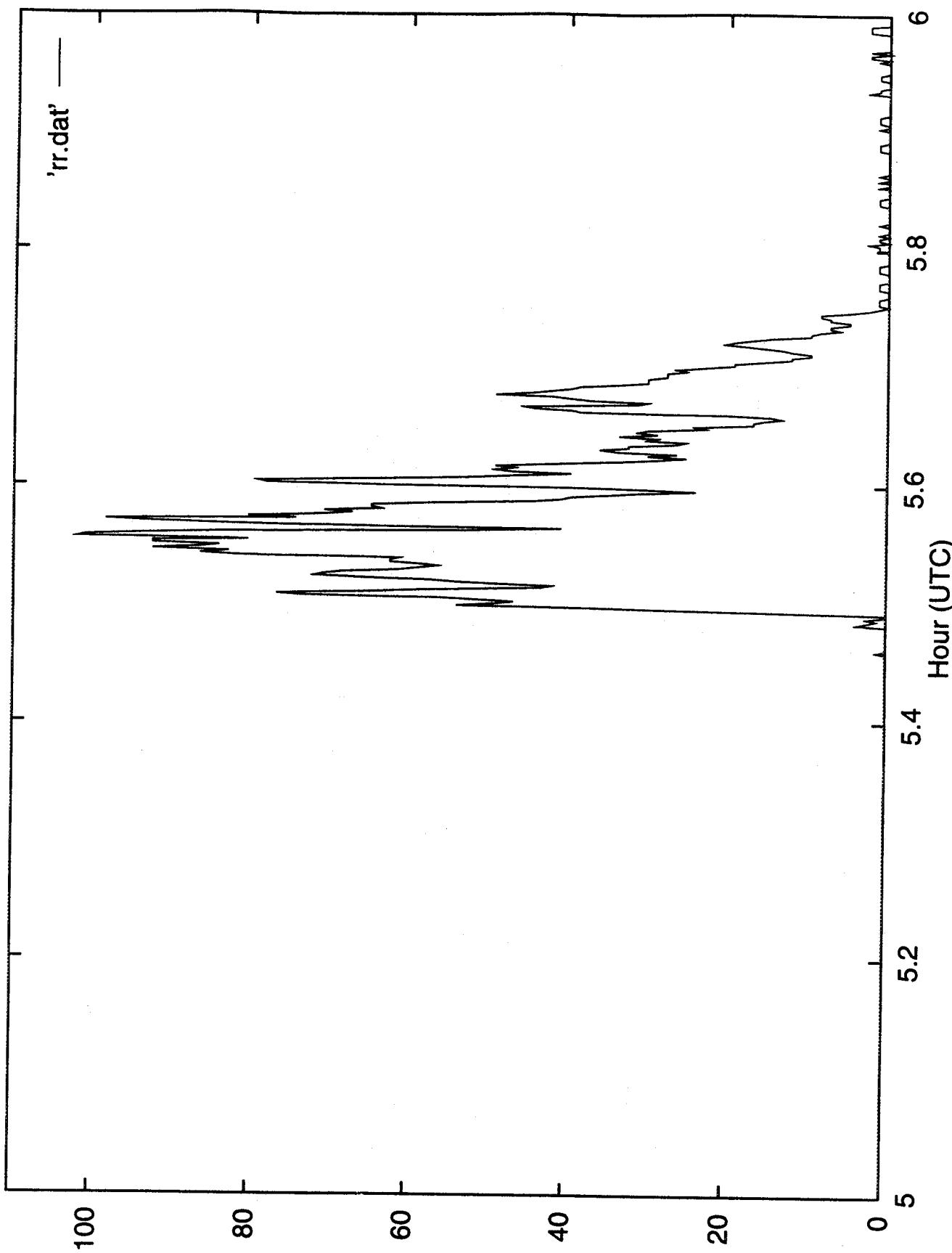
# Loss of Both Signals due to Rain Event

## 6/1/94 ACTS Propagation Data (CO)





Rain Rates for 6/1/94 data



377  
P. G.

## Propagation Models

- Mueller Propagation Model (Wayne Adams, NCAR)
  - The variation of the electric field along the propagation path is given by

$$\frac{dE_v}{ds} = (ik + M_{vv})E_v + M_{vh}E_h$$

$$\frac{dE_h}{ds} = M_{hv}E_v + (ik + M_{hh})E_h$$

where

$$M_{ij} = \sum_p n_p \frac{2\pi i}{k} f_{ij}(\hat{k})$$

- $f_{ij}$  are the forward scattering amplitudes
- $n_p$  is the number concentration

## Propagation Models

- The equations for the variation of the electric field along the propagation path can be used to obtain differential equations in terms of the modified Stokes parameters

$$\frac{dI_v}{ds} = 2Re(M_{vv})I_v + Re(M_{vh})U + Im(M_{vh})V$$

$$\frac{dI_h}{ds} = 2Re(M_{hh})I_h + Re(M_{hv})U - Im(M_{hv})V$$

$$\begin{aligned}\frac{dU}{ds} = & 2Re(M_{hv})I_v + 2Re(M_{vh})I_h + [Re(M_{vv}) \\ & + Re(M_{hh})]U - [Im(M_{vv}) - Im(M_{hh})]V\end{aligned}$$

$$\begin{aligned}\frac{dV}{ds} = & -2Im(M_{hv})I_v + 2Im(M_{vh})I_h + [Im(M_{vv}) \\ & - Im(M_{hh})]U + [Re(M_{vv}) + Re(M_{hh})]V\end{aligned}$$

where

$$I_v = \frac{|E_v|^2}{\eta}$$

$$I_h = \frac{|E_h|^2}{\eta}$$

$$U = \frac{2Re(E_v E_h^*)}{\eta}$$

$$V = \frac{2Im(E_v E_h^*)}{\eta}$$

## Propagation Models

- Solutions of the four differential equations yield four eigenvalues and eigenvectors

$$\beta(\hat{s}) = \begin{bmatrix} \beta_1(\theta, \phi) \\ \beta_2(\theta, \phi) \\ \beta_3(\theta, \phi) \\ \beta_4(\theta, \phi) \end{bmatrix} = \begin{bmatrix} 2ImK_1 \\ iK_2^* - iK_1 \\ iK_1^* - iK_2 \\ 2ImK_2 \end{bmatrix}$$

where

$$K_1 = k - \frac{i}{2} [M_{vv} + M_{hh} + r]$$
$$K_2 = k - \frac{i}{2} [M_{vv} + M_{hh} - r]$$

and

$$r = [(M_{vv} - M_{hh})^2 + 4M_{hv}M_{vh}]^{\frac{1}{2}}$$

## Propagation Models

The eigenmatrix is given by

$$\mathbf{H} = \begin{bmatrix} 1 & |b_2|^2 & b_2 & b_2^* \\ |b_1|^2 & 1 & b_1^* & b_1 \\ 2\operatorname{Re}(b_1) & 2\operatorname{Re}(b_2) & 1 + b_1^*b_2 & 1 + b_1b_2^* \\ -2\operatorname{Im}(b_1) & 2\operatorname{Im}(b_2) & i(1 - b_1^*b_2) & -i(1 - b_1b_2^*) \end{bmatrix}$$

where

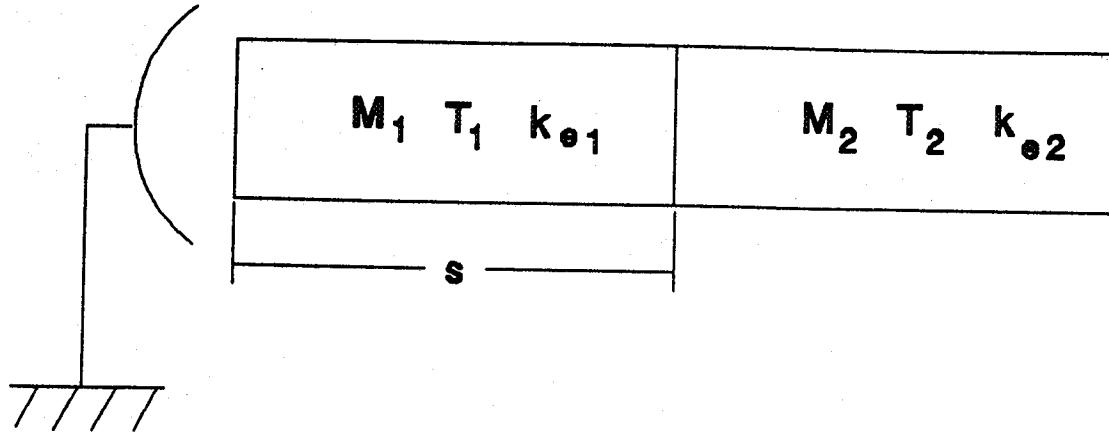
$$b_1 = \frac{2M_{hv}}{M_{vv} - M_{hh} + r}$$

$$b_2 = \frac{2M_{vh}}{-M_{vv} + M_{hh} + r}$$

The extinction matrix is defined as

$$\kappa_e = \begin{bmatrix} -2\operatorname{Re}(M_{vv}) & 0 \\ 0 & -2\operatorname{Re}(M_{hh}) \\ -2\operatorname{Re}(M_{hv}) & -2\operatorname{Re}(M_{vh}) \\ 2\operatorname{Im}(M_{hv}) & -2\operatorname{Im}(M_{vh}) \\ -\operatorname{Re}(M_{vh}) & -\operatorname{Im}(M_{vh}) \\ -\operatorname{Re}(M_{hv}) & \operatorname{Im}(M_{hv}) \\ -(R\operatorname{e}M_{vv} + R\operatorname{e}M_{hh}) & (I\operatorname{m}M_{vv} - I\operatorname{m}M_{hh}) \\ -(I\operatorname{m}M_{vv} - I\operatorname{m}M_{hh}) & -(R\operatorname{e}M_{vv} + R\operatorname{e}M_{hh}) \end{bmatrix}$$

## Propagation Models



The transmission matrix  $\mathbf{T}_1$  is given by

$$\mathbf{T}_1 = \mathbf{H} \mathbf{P} \mathbf{H}^{-1}$$

where

$$\mathbf{P} = \begin{bmatrix} e^{-\beta_1 s} & 0 & 0 & 0 \\ 0 & e^{-\beta_2 s} & 0 & 0 \\ 0 & 0 & e^{-\beta_3 s} & 0 \\ 0 & 0 & 0 & e^{-\beta_4 s} \end{bmatrix}$$

## **Propagation Models**

- The Mueller matrix in resolution volume 2 is then modified to take into account the propagation effects of resolution volume 1.

$$\mathbf{M}'_2 = \mathbf{T}_1^t \mathbf{M}_2 \mathbf{T}_1$$

- Radar parameters that are normally computed using the Mueller matrix, can now be computed with the new Mueller matrix ( $\mathbf{M}'_2$ ).

# **ACTS Up-link Power Control Experiment**

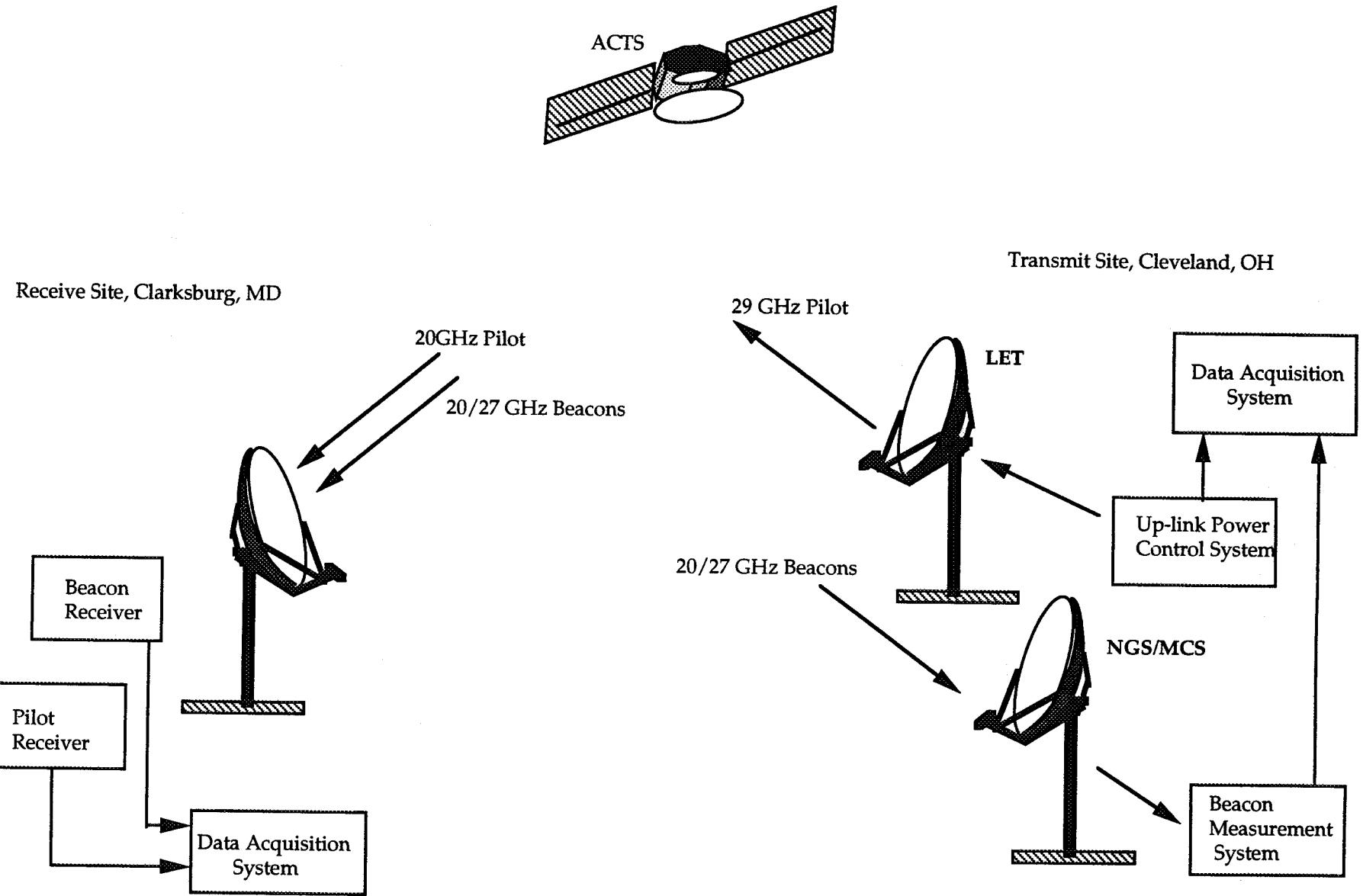
385

**A. Dissanayake**

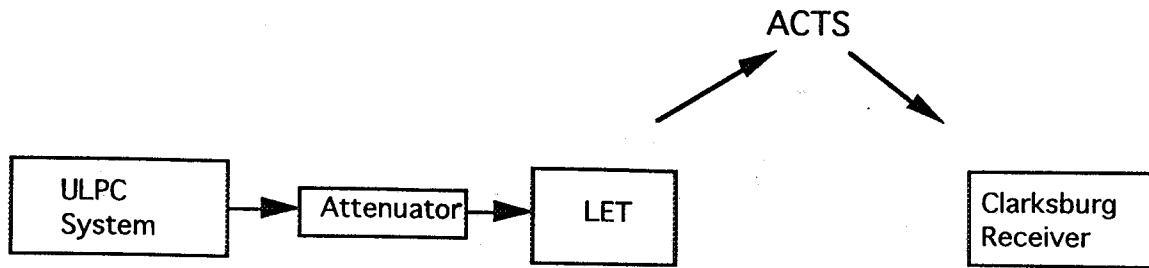
June 16, 1994

## Ka-band Up-link Power Control

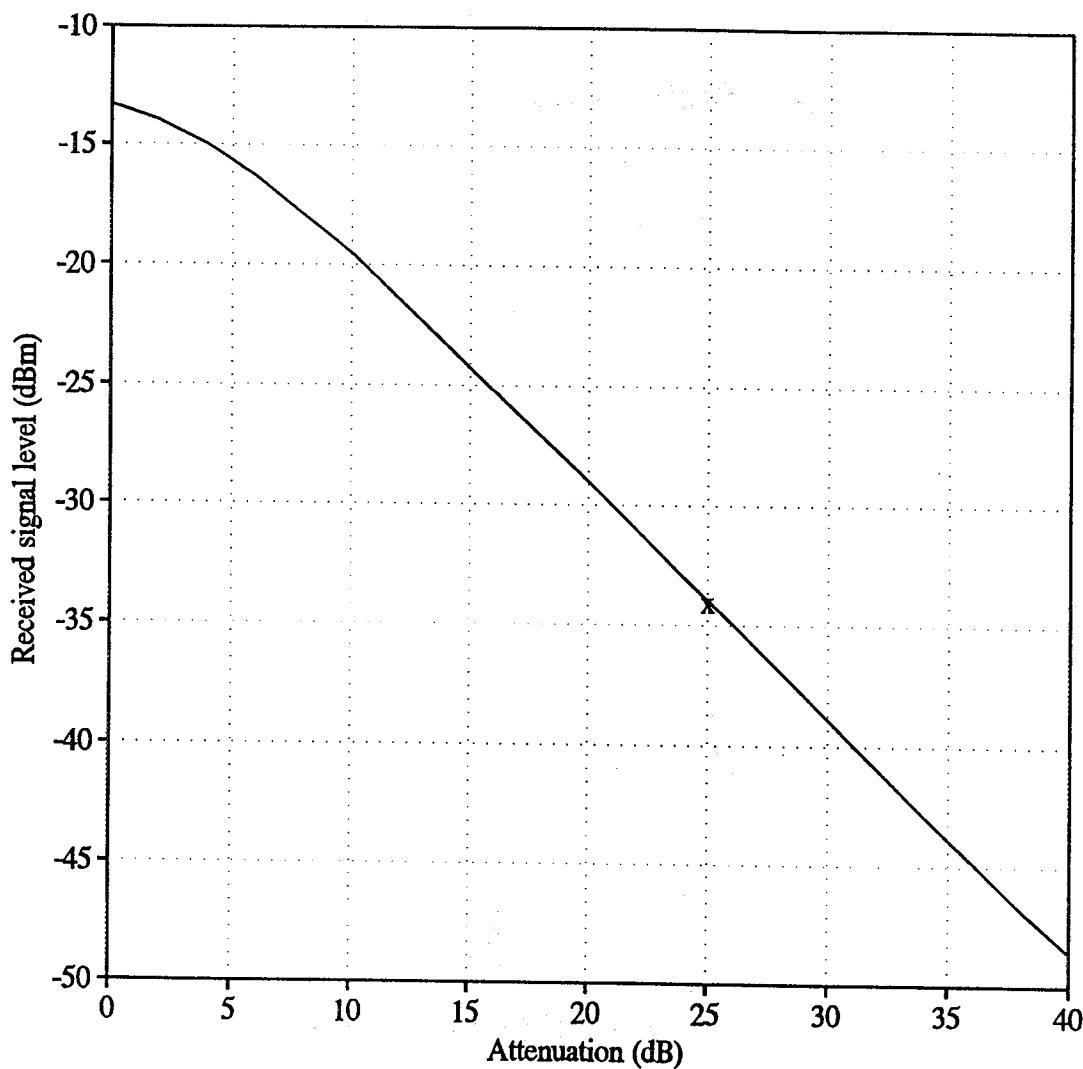
- \* Power control carried out using a 27 GHz pilot carrier transmitted from the LET at Lewis Center in Cleveland; transponded carrier received at Clarksburg.
- \* Power control based on down-link attenuation measurements at 20 GHz
- \* Beacon reception and pilot transmission are done on separate antennas; antenna separation ~ 15 ft.
- \* Control applied at IF; power control resolution: 0.2 dB; update rate 5 Hz
- \* Maximum power control range: 25 dB; however, investigation will be limited to a control range of 15 dB.
- \* Several safety features incorporated into the power controller design to protect space segment



ACTS Up-link Power Control Experiment Configuration



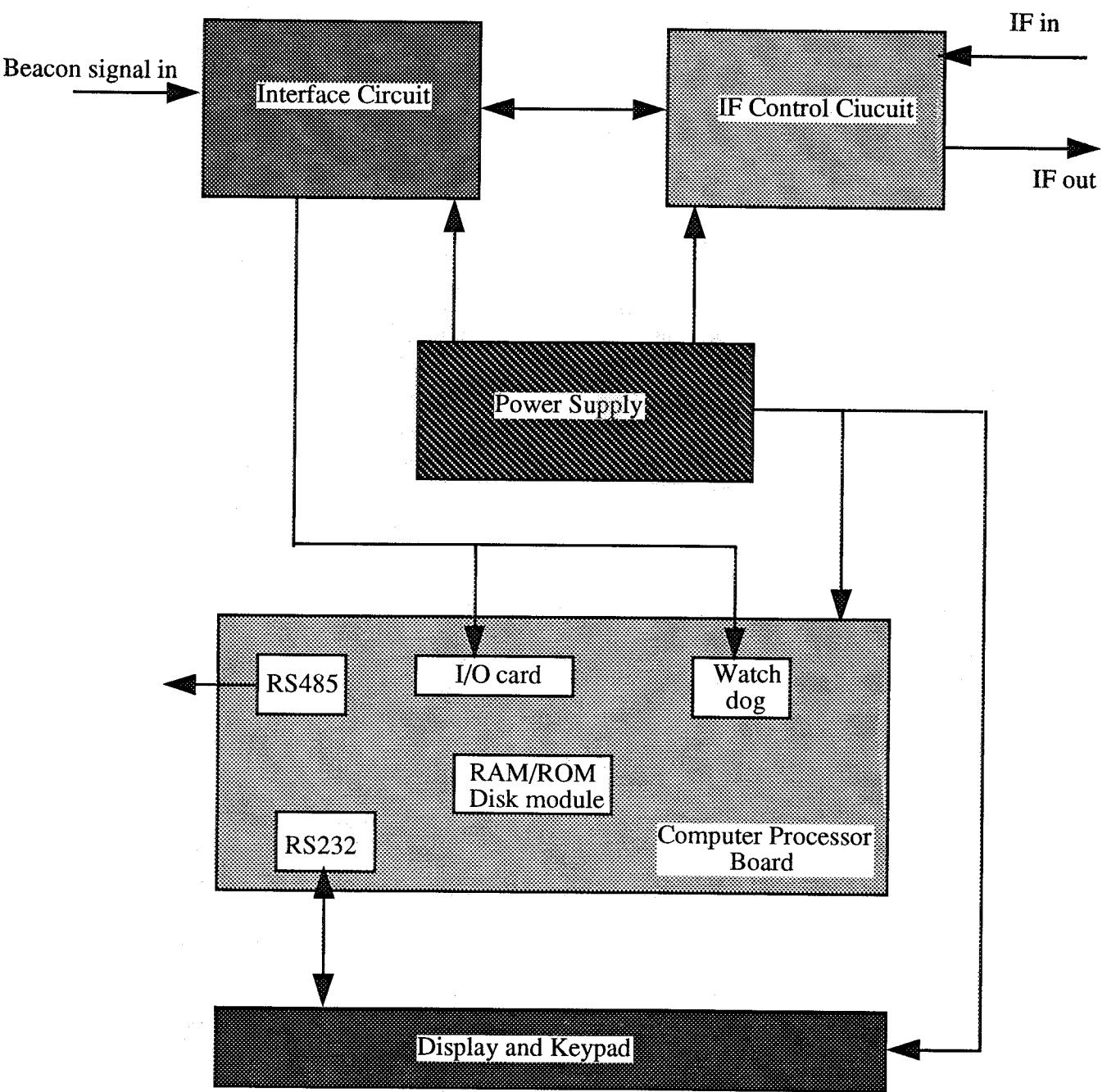
Measurement Configuration



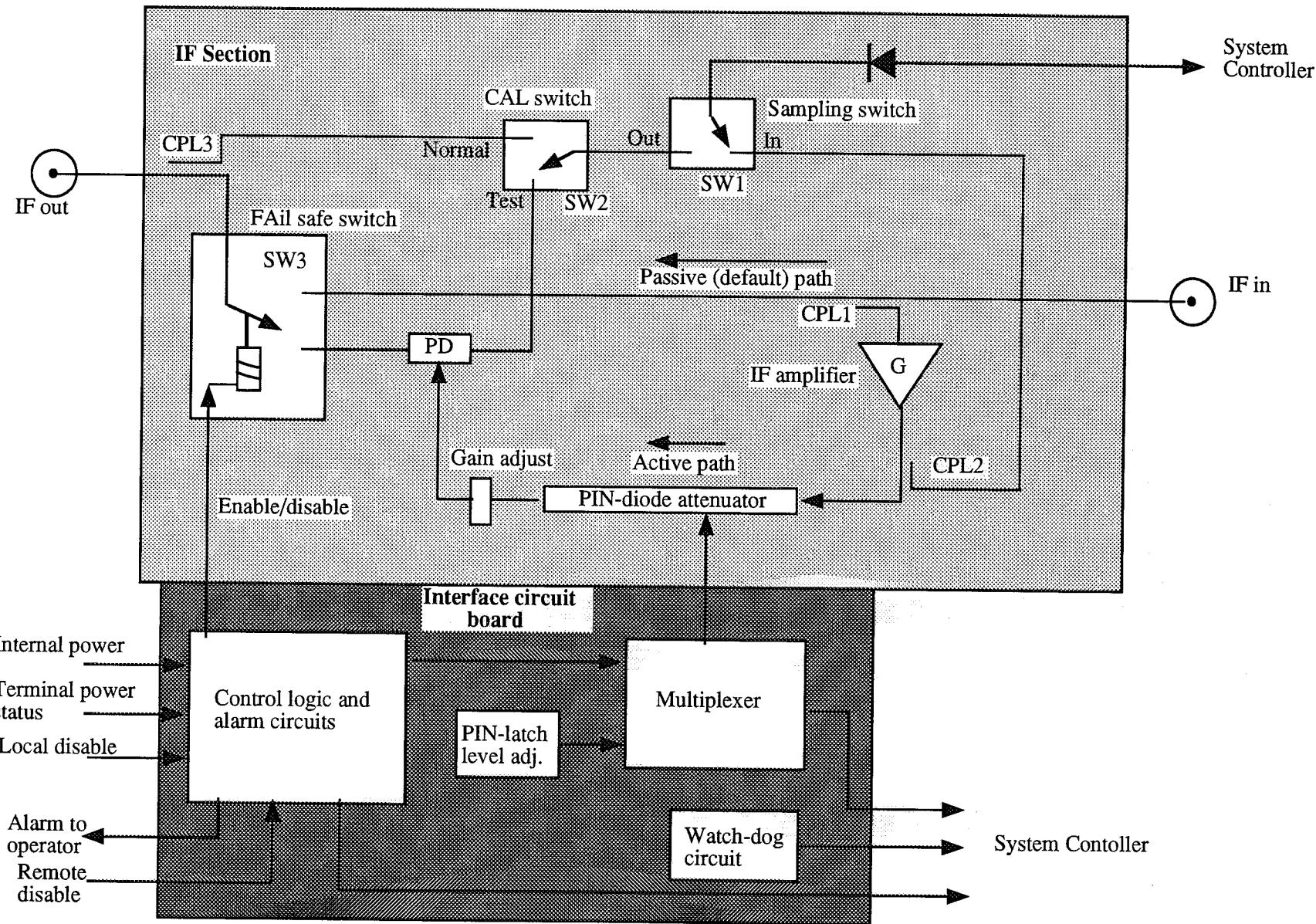
*Transponder/LET linearity test; attenuator setting  
vs. signal strength received at Clarksburg  
x - nominal operating point*

## Power Control System

- \* Power control applied via a linearized PIN attenuator
- \* A default path without power control available in case of a system failure; this path is also activated under exceptional conditions (beacon failure, beacon level jump or unacceptable drift)
- \* Intel 386 based PC used as the system controller; system controller and control circuitry housed in a standard rack unit.
- \* Controller parameters programmed through a front panel keypad and display.



Functional Block Diagram of the Up-link Power Controller



Control and Interface Circuits

# Power Control Algorithm

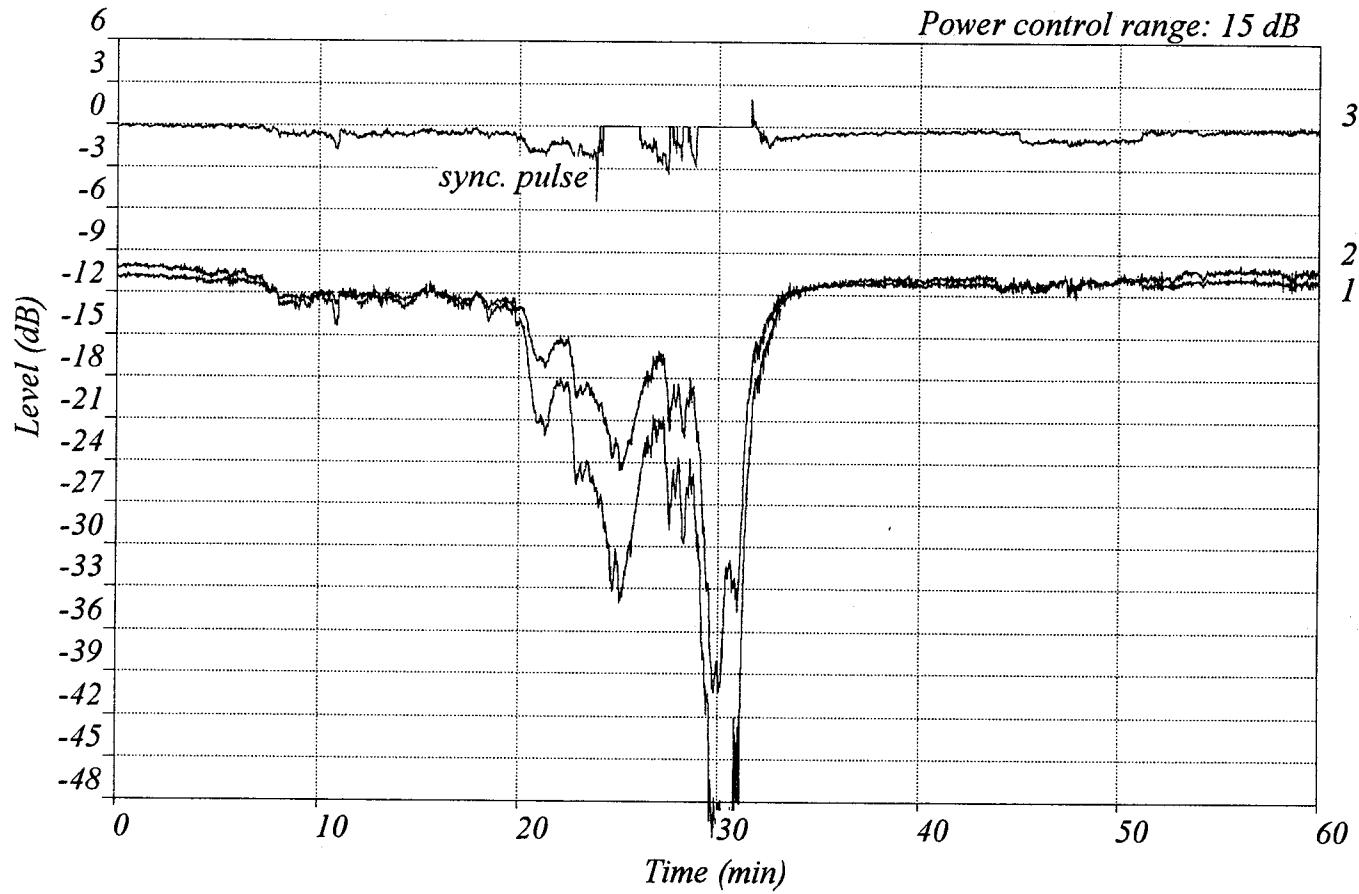
392

- \* Detect down-link fade after establishing the reference level; reference level based on long-term observations using an adaptive filter with a time constant of the order of 1 hour
- \* Down-link fade separated in to rain fade and scintillation components; n averaging time of 20 sec. used in estimating the rain fade.
- \* Current level of rain fade predicted using an adaptive filter
- \* Frequency scaling of rain and scintillation fades to 27 GHz

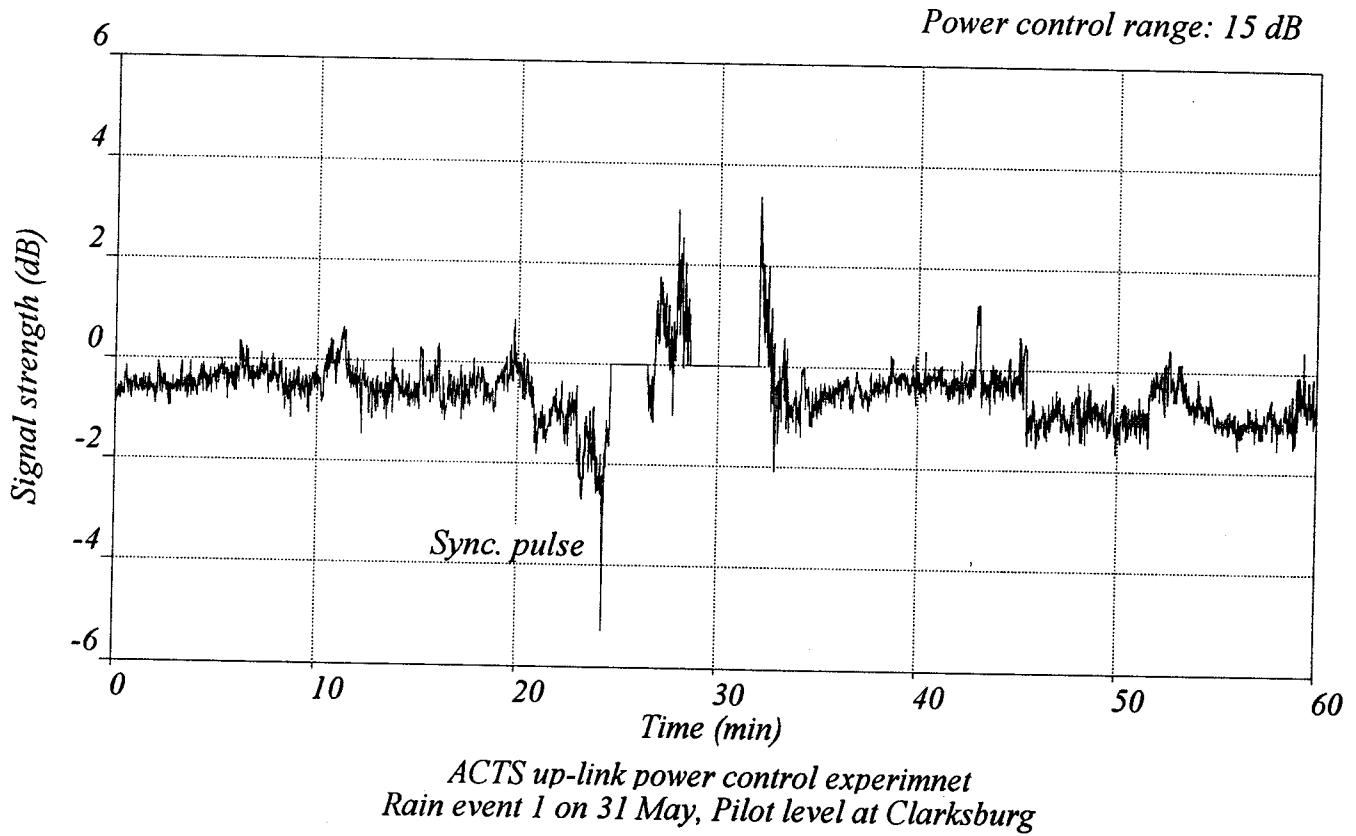
## Initial Results

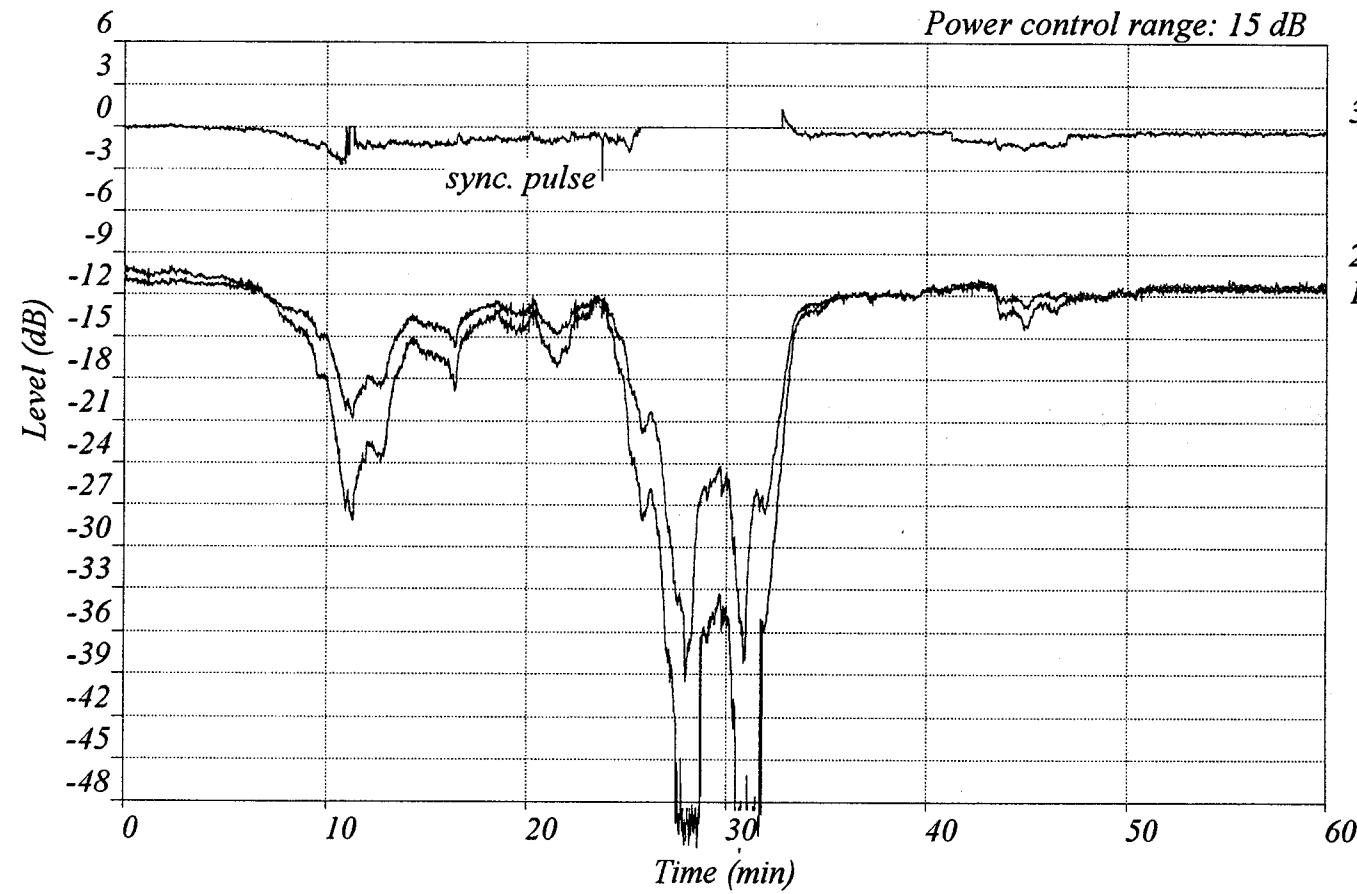
393

- \* Separate transmit and receive antennas do not allow meaningful investigation of scintillation compensation.
- \* Approximately 24 hours of pilot transmissions completed; three severe rainstorms encountered during this period.
- \* Algorithm appears to underestimate the up-link fade.
- \* When restricted to a power control range of 15 dB, the control accuracy can be maintained within  $\pm 3$  dB.



ACTS up-link power control experiment  
Rain event 1 on 31 May, 1994; 1: 20GHz, 2: 30GHz, 3: control error





ACTS up-link power control experiment  
Rain event 2 on 31 May, 1994; 1: 20GHz, 2: 30GHz, 3: control error

